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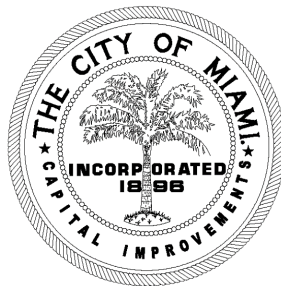
# **DRAINAGE REPORT**

## **Mary Brickell Village Drainage and Roadway Improvements Phases I and II City of Miami Project B-30637**

Miami-Dade County, Florida

*Prepared for*

**CITY OF MIAMI**



**DEPARTMENT OF CAPITAL IMPROVEMENTS**

***July 2011***

*Prepared by*

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**TABLE OF CONTENTS**

**SECTION 1 INTRODUCTION.....4**

1.1 PURPOSE.....4

1.2 PROJECT LOCATION.....4

1.3 NEED FOR IMPROVEMENT.....4

**SECTION 2 EXISTING CONDITIONS .....7**

2.1 DRAINAGE WATERSHED .....7

2.2 TOPOGRAPHY.....7

2.3 GROUND WATER TABLE/BOUNDARY CONDITION ELEVATION.....9

2.4 LAND USE .....9

2.5 SOILS.....11

2.6 FLOOD PLAIN INFORMATION .....11

2.7 EXISTING DRAINAGE SYSTEM CHARACTERISTICS .....12

2.8 CONTRIBUTING FACTORS.....15

2.9 EXISTING FLOODING CONDITIONS.....16

**SECTION 3 DESIGN AND EVALUATION CRITERIA..... 16**

3.1 DESIGN CRITERIA .....16

3.2 WATER QUALITY.....17

3.3 WATER QUANTITY .....17

3.4 ALLOWABLE FLOOD LEVELS .....18

3.5 PERMITTING REQUIREMENTS AND ENVIRONMENTAL AGENCY COORDINATION .....18

**SECTION 4 MODEL METHODOLOGY ..... 19**

4.1 APPROACH.....19

4.2 GENERAL MODEL INFORMATION .....19

4.3 HYDROLOGIC MODELING.....19

4.3.1 Curve Number.....20

4.3.2 Rainfall Precipitation.....20

4.3.3 Rainfall Distribution.....21

4.3.4 Time of Concentration (TOC).....21

4.4 HYDRAULIC DATA .....21

4.4.1 Node Data.....22

4.4.2 Boundary Conditions.....22

4.4.3 Link Data.....22

4.5 MODEL CALIBRATION.....23

**SECTION 5 ANALYSIS OF PRE-DEVELOPMENT CONDITIONS..... 23**

**SECTION 6 ANALYSIS OF POST-DEVELOPMENT CONDITIONS..... 26**

6.1 OBJECTIVES .....26

6.2 ANALYSIS OF PROPOSED IMPROVEMENTS – ALTERNATIVE 1 .....26

6.3 ANALYSIS OF PROPOSED IMPROVEMENTS – FINAL DESIGN .....29

6.4 OTHER DESIGN CONSIDERATIONS .....34

6.5 WATER QUALITY.....34

**SECTION 7 ROADWAY IMPROVEMENTS ..... 35**

**SECTION 8 CONCLUSIONS..... 36**



**APPENDICES**

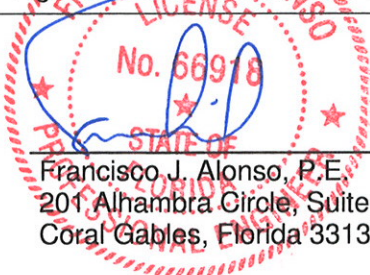
Appendix A – Report Back-Up Documentation.....A  
 Appendix B – Roadway Typical Sections .....B  
 Appendix C – Miscellaneous calculations ..... C  
 Appendix D – Water Quality Calculations..... D  
 Appendix E – Existing Flooding Conditions Documentation .....E  
 Appendix F – ICPR Pre-Development Model .....F  
 Appendix G – ICPR Post-Development Model ..... G  
 Appendix H – Geotechnical Engineering Reports ..... H  
 Appendix I – Cost Estimates ..... I  
 Appendix J – Correspondence ..... J

**LIST OF TABLES**

Table 1 Design Rainfall Depths, inches 21  
 Table 2 Pre-Development Conditions Flood Stage Summary 24  
 Table 3 Post-Development Alternative 1 Flood Stage Summary 28  
 Table 4 Post-Development Final Flood Stage Summary 30

**LIST OF FIGURES**

Figure 1 Project Location Map 6  
 Figure 2 Survey Topography 8  
 Figure 3 Mary Brickell Village Project Area Land Use Map 10  
 Figure 4 NRCS Soils Survey Map 11  
 Figure 5 FEMA FIRM 12  
 Figure 6 Flooding at the intersection of SE 9<sup>th</sup> Street and 1<sup>st</sup> Avenue 13  
 Figure 7 Drainage Basin Map and Existing Drainage System 14  
 Figure 8 Pre-Development Node-Link Diagram 25  
 Figure 9 Possible Pump Station Location 27  
 Figure 10 Post-Development Node-Link Diagram 32  
 Figure 11 Time vs. Stage of B-21 - Pre vs. Post 33  
 Figure 12 Current State of SW 1<sup>st</sup> Court Outfall 34



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## Abbreviations

Some of the abbreviations used in this report are defined here for convenience.

BMP	Best Management Practices
CIT	City of Miami Department of Capital Improvements and Transportation
cfs	Cubic Feet Per Second
CR	County Road
DCIA	Directly Connected Impervious Area
DERM	Miami-Dade Department of Environmental Resources Management
DHW	Design High Water
EPA	United States Environmental Protection Agency
ERP	Environmental Resource Permit
FDOT	Florida Department of Transportation
FEMA	Federal Emergency Management Agency
FIRM	Flood Insurance Rate Map
FIS	Flood Insurance Study
FLUCCS	Florida Land Use, Cover and Forms Classification System
fps	Feet Per Second
GDP	General Development Plan
GIS	Geographical Information System
HSG	Hydrologic Soil Group
MDWASD	Miami-Dade Water and Sewer Department
NET	Neighborhood Enhancement Team
NGVD	National Geodetic Vertical Datum of 1929
NRCS	Natural Resources Conservation Service
NW	North West
NWL	Normal Water Level
SFWMD	South Florida Water Management District
SPT	Standard Penetration Test Borings
SR	State Road
SW	South West
SWMM	Storm Water Management Model
SWMMP	Storm Water Management Master Plan
USACE	United States Army Corps of Engineers
USGS	United States Geological Survey

## SECTION 1 INTRODUCTION

The City of Miami Department of Capital Improvements Program (CIP) retained the services of T.Y. Lin International | H.J. Ross (TYLI) to prepare the design documents for the Mary Brickell Village Area of the City in order to provide drainage improvements and roadway restoration based on the findings of the accepted Technical Memorandum. **Figure 1** shows the Project Location Map.

### 1.1 PURPOSE

The purpose of this Drainage Report is to provide a basis for proposed drainage improvements within the above City of Miami community that will address flooding problems. This report will serve as the basis for the design to improve the drainage system and reduce flooding in this community. This report will also identify contributing factors to the flooding conditions, establish drainage requirements, and present the proposed measures to reduce flood stages within the project limits. Drainage improvements presented in this report do not guarantee complete elimination of potential drainage problems. By design, flood levels and the duration of standing water will be reduced, but the potential for flooding cannot be completely eliminated.

### 1.2 PROJECT LOCATION

The Mary Brickell Drainage Improvement project is located within Section 12, Township 54S, Range 41E, within the City of Miami limits. The project area, as defined by the CIP department, is bounded by and includes SW 9<sup>th</sup> Street to the north, SE 1<sup>st</sup> Ave. to the east, SW 12<sup>th</sup> Street to the south, and SW 1<sup>st</sup> Avenue to the west. In addition the area along SW 1<sup>st</sup> Court West of the MDT corridor between SW 9<sup>th</sup> Street and SW 8<sup>th</sup> Street will be used for the proposed location of the pump station and possible drainage wells. **Figure 1** shows an Aerial Plan depicting the limits of the Mary Brickell Village project.

This project is located in the heart of Miami's Financial District and is home to many recent development projects such as the shops at Mary Brickell Village and several condominium towers. The area is one of the City's more unique attractions with dozens of restaurants, stores, and night clubs.

Through the center of the project area runs the South Miami Avenue corridor. This corridor is part of the Miami-Dade County right-of-way and is maintained by the County. Currently there are two projects in the works for the South Miami Avenue corridor that are of interest to CIP. The County is initiating a drainage project along South Miami Avenue that will address drainage from SW 10<sup>th</sup> Street south to SW 13<sup>th</sup> Street along the corridor. As part of this study, it will be assumed that the contributing basin in this area is captured by the future County system. In addition the City of Miami's Downtown Development Agency (DDA) is currently holding workshops for conceptual designs on aesthetic and vehicular improvements for the corridor. No conflicts between this proposed project and the two ongoing City and County projects are anticipated, but coordination will remain a primary objective.

### 1.3 NEED FOR IMPROVEMENT

Within the Mary Brickell Village project area there are extreme low-lying areas that frequently experience flooding from routine rainstorm events. The extent and duration of the flooding

problems vary from event to event, however, the nature of standing water within the City streets and adjacent properties is often predictable. During the summer months, short, intense storm events are a daily occurrence and city streets routinely flood followed by a slow subsidence when the storm are combined with high tide. Storm events such as Hurricane Irene in October of 1999, Hurricane Leslie in October of 2000, and the storms of 2005 produced water levels of several feet in the streets. In addition several private shops located adjacent to the lowest areas along SE 9<sup>th</sup> Street and SW 10<sup>th</sup> Street have experienced flooding and water damage as a result.

The effects of these intense storms and the resulting physical damage to properties and public facilities caused by high water levels are experienced throughout the community. Damages include City roadways that are in need of repair, reduced traffic flows during routine storm events, and several properties that have recurring damages.

The need for improvement lies in three key components. First, the existing storm water management system was constructed in the 1950's when development first began in this area. The existing system is a gravity system with a tidal dependant outfall. The system has not been significantly upgraded over the years. The original box culvert trunk lines, 12" cross drains, and cast iron inlets are still in use. Secondly, High tide elevations are typically around 2.60' (CM Datum) and the lowest grade elevations in the major depressions of the project are below 3.50'. As such there is very little storage in the system, and when intense rainfalls arrive during high tide, extreme flooding occurs and does not subside until the tide recedes.

To exacerbate the situation the land use in the area has significantly changed to the point where the area is practically built out and the percent impervious has reached nearly 100%. Although the developments have been required to address drainage on their sites, the impact of high-rise structures and reduced perviousness has inevitably increased runoff.

Engineered flood mitigation solutions and measures are desperately needed to provide this Miami community relief from the effects of flooding.



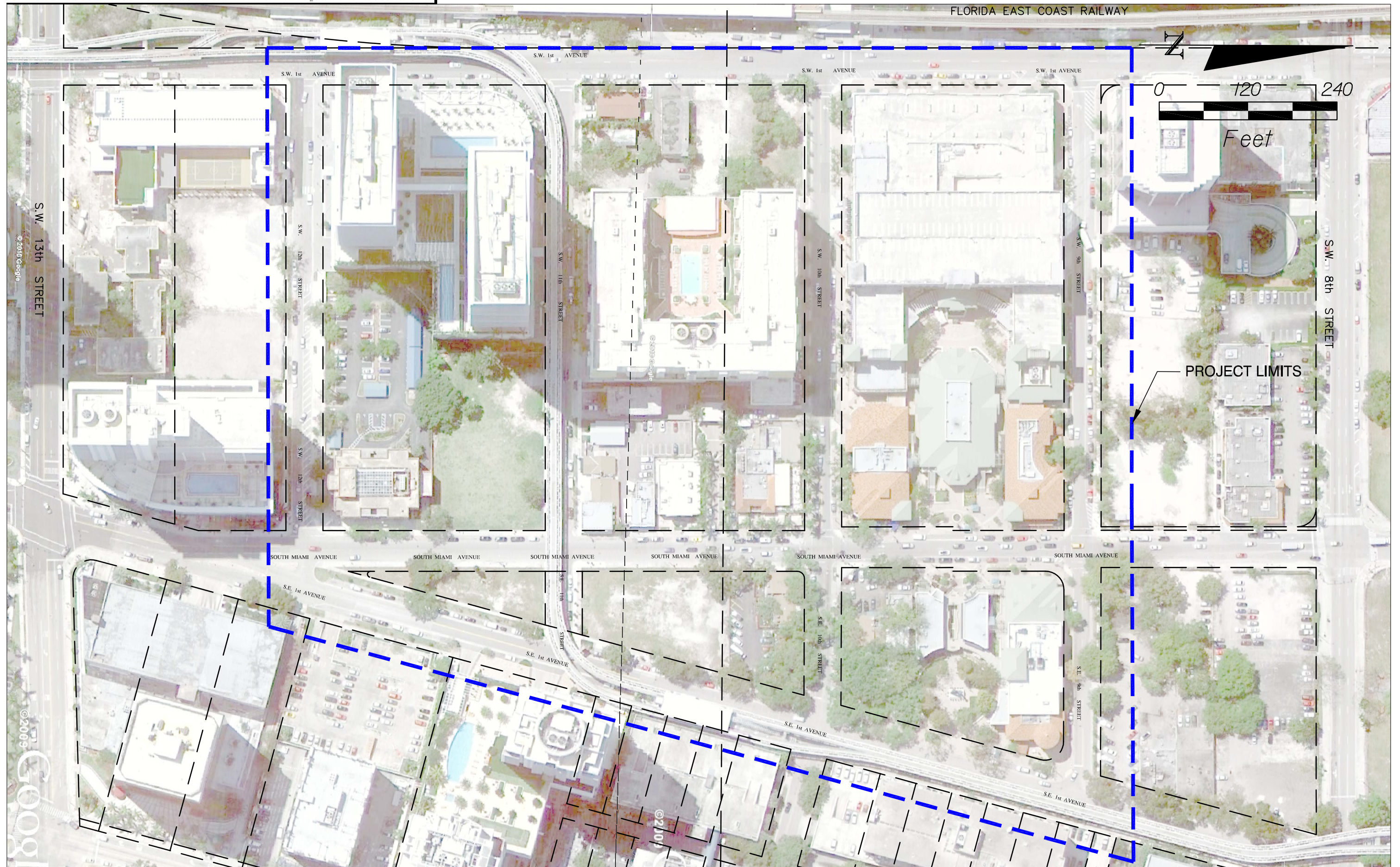


FIGURE 1: MARY BRICKELL VILLAGE PROJECT LOCATION MAP



## SECTION 2 EXISTING CONDITIONS

### 2.1 DRAINAGE WATERSHED

The Mary Brickell Village Drainage Improvements Project is located at the downstream end of the Miami River Watershed (C-5 basin). The project lies downstream of the last South Florida Water Management District (SFWMD) control structures (S-25 and S-25B and S-26) and is subject to tidal conditions. Because of its proximity to the Bay, tidal conditions have a greater influence on the functioning of the drainage system.

Both the SFWMD and the Miami-Dade County Department of Environmental Resources Management (DERM) are conducting hydrologic-hydraulic models of the C-3, C-4, C-5 and the C-6 Canal systems.

### 2.2 TOPOGRAPHY

The Mary Brickell Village Drainage Improvements Project is in eastern Miami-Dade County in an area of relatively flat or slightly rolling topographic relief. The topography is such that the land surface undulates between extreme low spots and slightly higher ground. The undulating topographic characteristics combined with inadequate existing drainage systems leaves scattered areas vulnerable to recurring flooding conditions.

The existing ground elevations vary from a low of approximately 3.50-feet\* in the depressions at SE 9<sup>th</sup> Street/1<sup>st</sup> Avenue and SW 10<sup>th</sup> Street east of 1<sup>st</sup> Avenue to a high of approximately 10.30-feet at SW 12<sup>th</sup> Street. The area was topographically surveyed by J. Bonfill and Associates specifically for this project. **Figure 2** depicts the actual surveyed elevation contours throughout the project area.

The project area is extremely low relative to the neighboring arterial roads and properties. SW 8<sup>th</sup> Street to the North, the Brickell Avenue developments to the east and SW 13<sup>th</sup> Street to the south are on average 2'-3' higher than the residential roads in the project area. This topography causes a "soup bowl" effect in this area of the City. With no overland relief the area requires a robust internal drainage system to manage storm water runoff. This report will serve to evaluate the deficiencies of this internal drainage system and propose improvements based on the findings of the technical memorandum.

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\* City of Miami Datum unless otherwise noted.

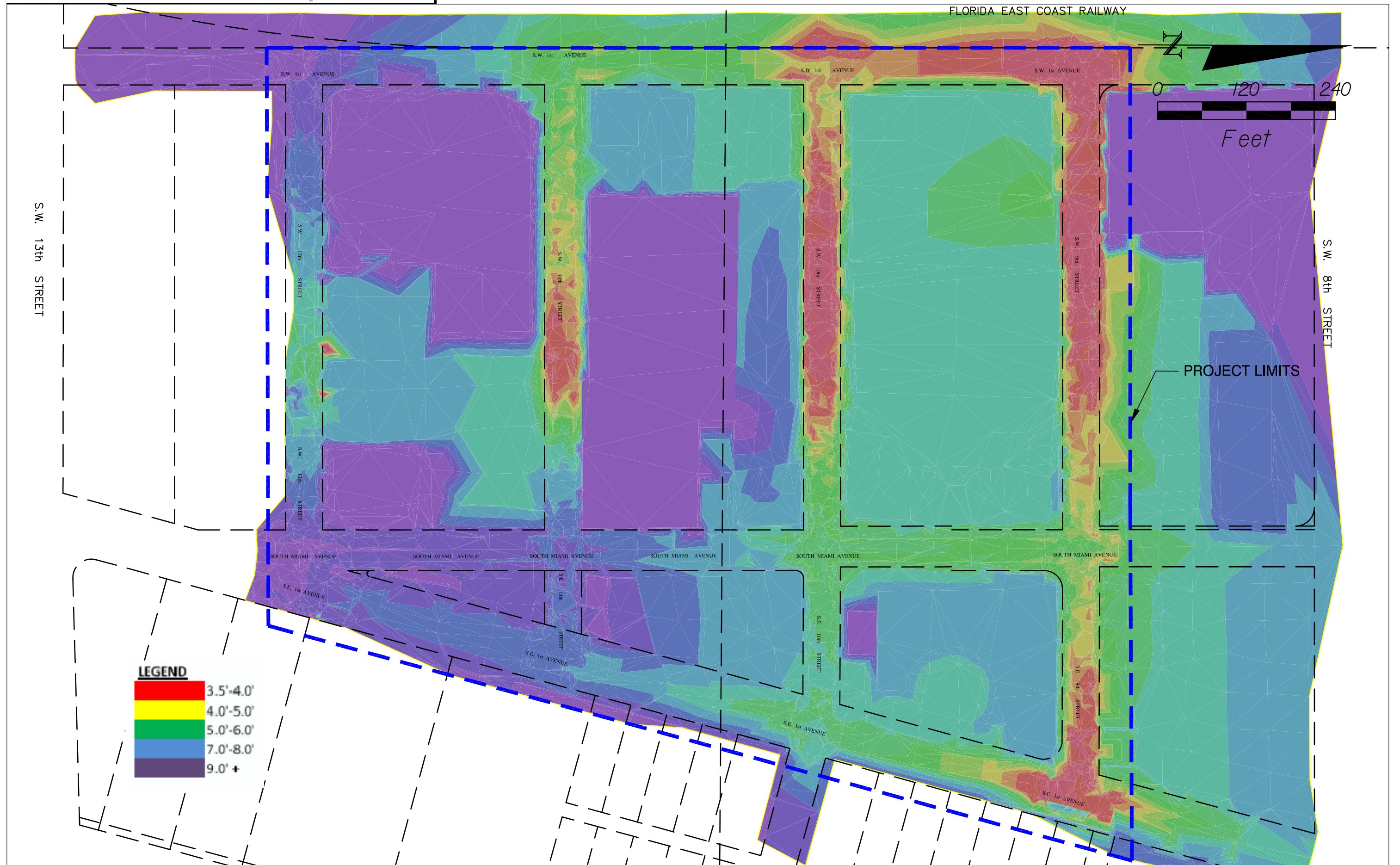


FIGURE 2: MARY BRICKELL VILLAGE PROJECT TOPOGRAPHY

### 2.3 GROUND WATER TABLE/BOUNDARY CONDITION ELEVATION

The ground water table elevation was obtained from the Miami-Dade County Public Works Department Design Standards Figure W.C. 2.1, Average Yearly Highest Ground Water Level (GWL) 1960-1975, and figure W.C. 2.2, Average October Ground Water Level (GWL) 1960-1975. The average yearly highest GWL is approximately 3.00-feet above mean sea level or 3.25-feet City of Miami Datum (CMD). The average October GWL is 2.00-feet above mean sea level (MSL) or 2.25-feet City of Miami Datum (CMD). See Appendix A for Miami-Dade County Public Works Department Design Standards GWL Figures.

The high tide water level was derived from the nearest NOAA tidal station (id# 8723165) at the Miami Marina near Bayside Marketplace. The elevation was calculated from tidal datum information to correspond to 2.10' City of Miami Datum. The highest observed elevation at this station was found to 3.32' City of Miami Datum. See Appendix C for the NOAA tide station information and datum calculations.

For modeling purposes, field observations of the static water levels were used as the observed levels were higher than the 2.10' derived from the NOAA tide station. This may be due to the fact that the point of discharge at the River is further inland than the NOAA station and may be subject to some head loss through the river section, raising the tailwater elevation. On October 14, 2010, a field survey was taken at high tide (approx. 3:04PM) and the water level was measured to be approximately 2.60' City of Miami Datum. This was used as the design tailwater and water table starting elevation. For the 25 year and 100 year storm events a tailwater elevation equivalent to the highest observed elevation was implemented in the model. Since our observed elevation for the MHHW was approximately 0.5' above the recorded level at the NOAA station, it was deduced that the same incremental elevation could be added to the highest observed elevation of 3.32' yielding a tailwater elevation of approximately 3.80' City of Miami Datum.

### 2.4 LAND USE

All on-site and adjacent land use types were classified according to the Florida Department of Transportation Florida Land Use, Cover and Forms Classification System (FLUCCS). Land use types were delineated utilizing ArcView, a Geographical Information System software package.

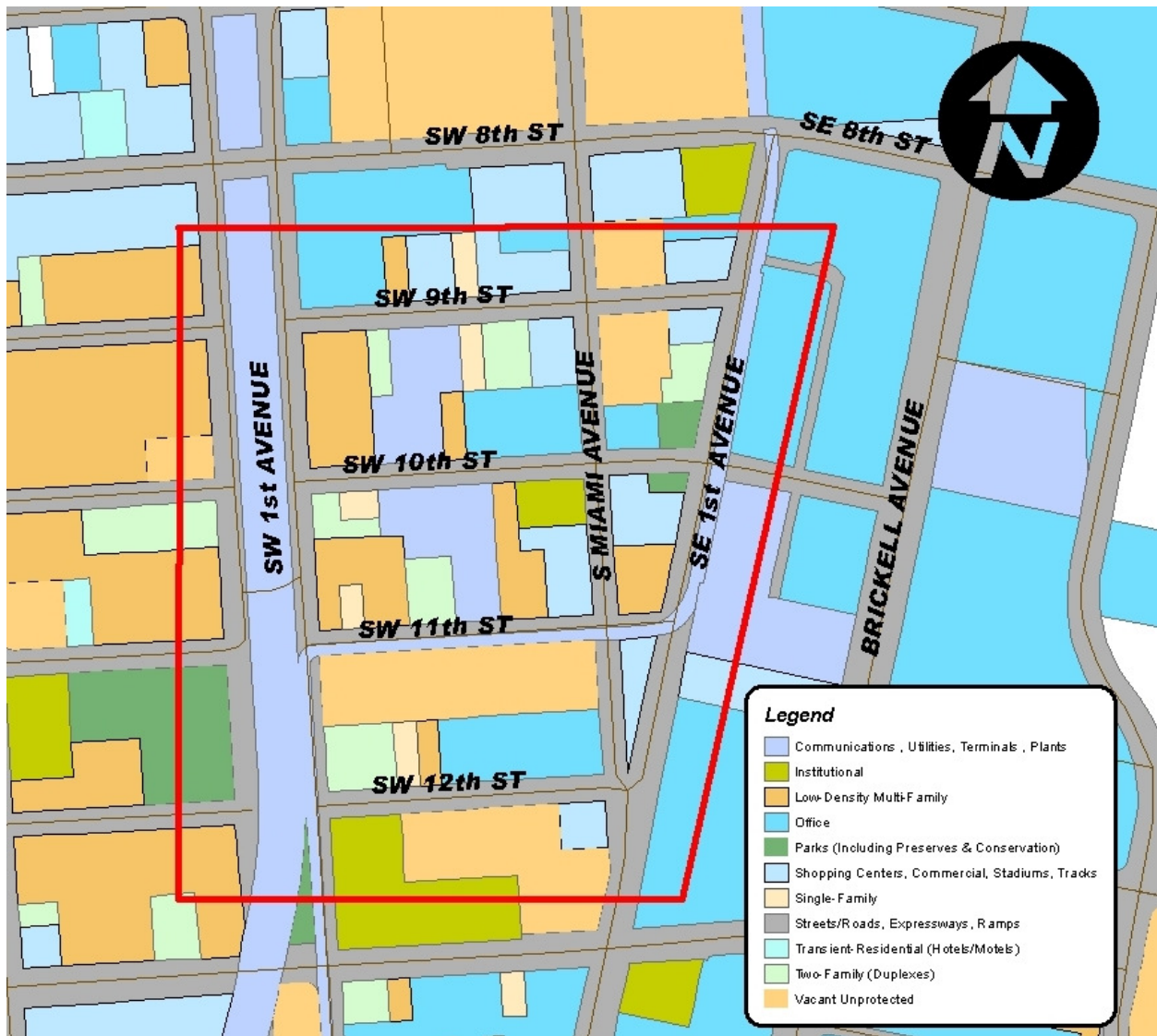
The Mary Brickell Village project area is highly diverse and consists of the following different land use categories:

- Communications, Utilities, Terminals, Plants
- Institutional
- Low-Density Multi-Family
- Office
- Parks (including preserves and conservation)
- Shopping Centers, Commercial, Stadiums, Tracks
- Single Family



- Transient Residential (Hotels/Motels)
- Two-Family (Duplexes)
- Vacant Unprotected

The primary uses are commercial (storefronts and restaurants) and residential condominiums. **Figure 3** shows the existing Land Use Maps for the Mary Brickell Village Area. This map is based on current land use which has been modified within the last ten years. Future land uses within the project areas are expected to remain the same.



**FIGURE 3 MARY BRICKELL VILLAGE PROJECT AREA LAND USE MAP**

## 2.5 SOILS

Soil properties in Miami-Dade County are highly variable. MacTec Engineering and Consulting, Inc. prepared geotechnical reports for the project area. Appendix G includes the geotechnical report.

Because of the extremely low ground elevations and high water table, the use of exfiltration trenches has been dismissed for the lowest elevation basins. As such the geotechnical exploration did not include percolation testing. However SPT borings to determine the condition and type of earth were taken as well as various pavement cores to determine the extent of pavement restoration.

The “Soil Survey of Miami-Dade County, Florida,” (1984) published by the Natural Resources Conservation Service (NRCS) was reviewed for near surface and subsurface soil information for the project area. Due to the urban nature of the area the dominant soil type is Urban Land, defined as land covered by more than 70-percent impervious urban development. These soils do not have a hydrologic soil group (HSG) classification.

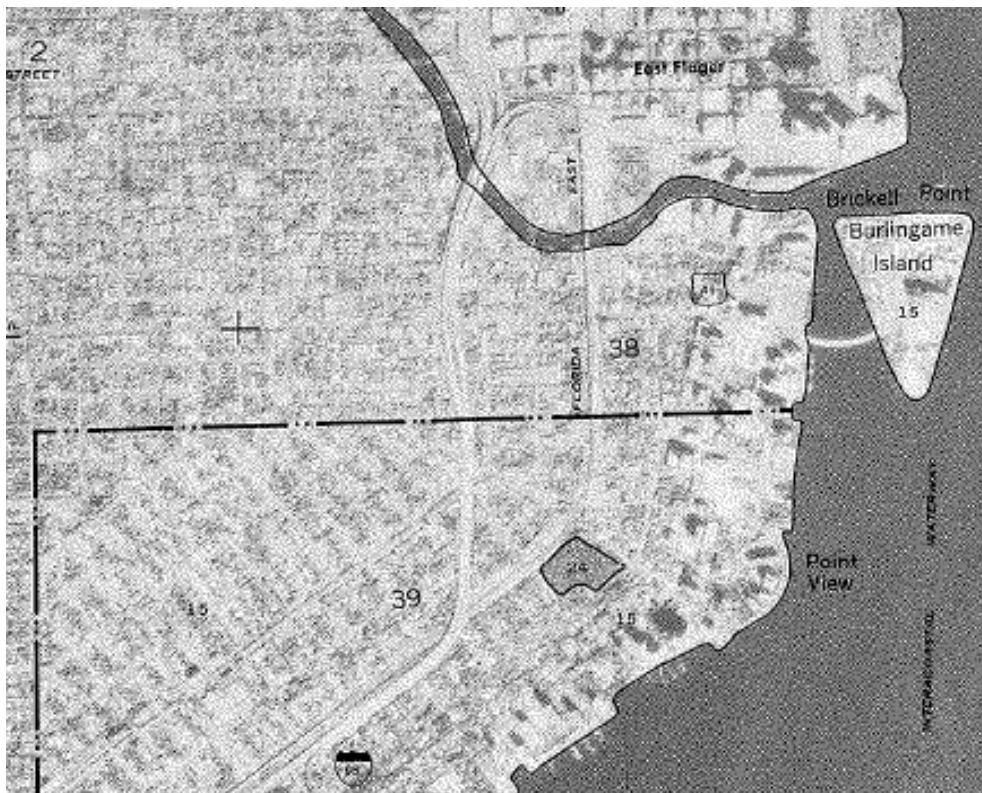


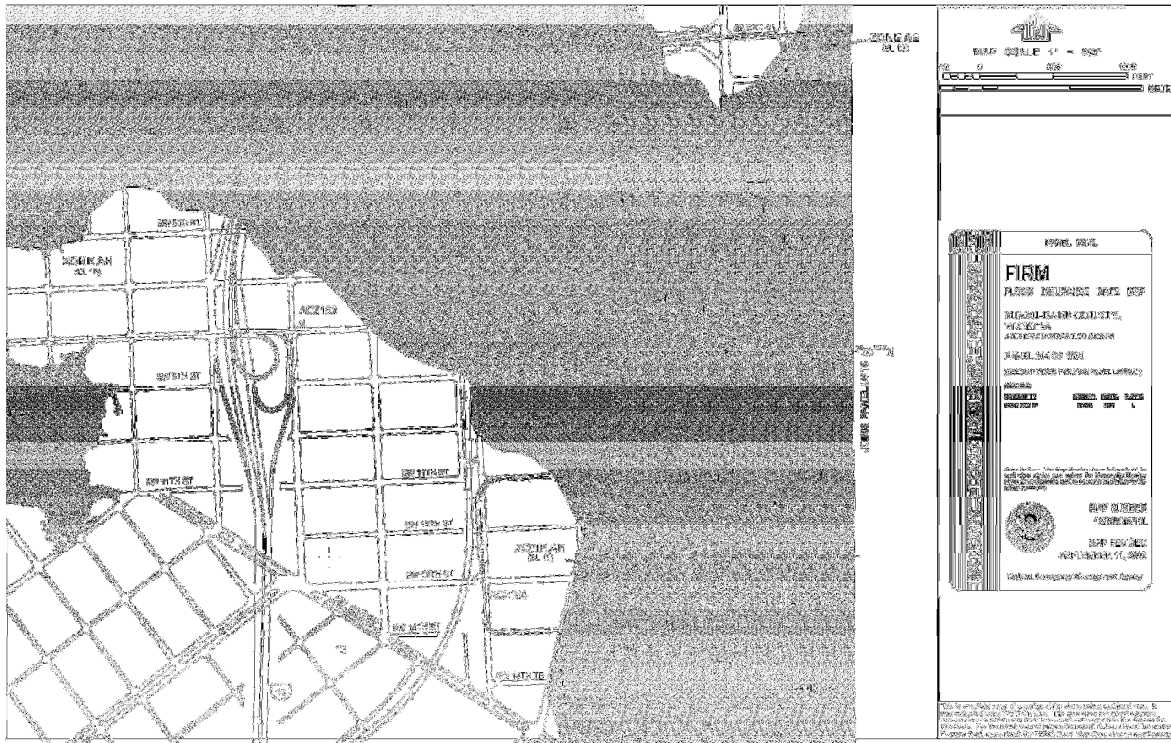
FIGURE 4 NRCS SOILS SURVEY MAP

## 2.6 FLOOD PLAIN INFORMATION

A review of the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Maps (FIRM) indicates that the project area is primarily located within zone AE with a base flood elevation of 10 as depicted in FIRM Community Panel No. 12086C0314L, dated September 11,



2009. The higher elevation areas around SW 12<sup>th</sup> Street and 1<sup>st</sup> Avenue lie within zone X, outside of the 100 yr floodplain. **Figure 5** depicts the FEMA FIRM map for the project area.



**FIGURE 5 FEMA FIRM**

## 2.7 EXISTING DRAINAGE SYSTEM CHARACTERISTICS

The existing storm water management system the Durham Terrace project area consists primarily of curb and gutter street sections with curb inlets, and an interconnected gravity sewer system with direct discharge to the Miami River at SW 1<sup>st</sup> Court. The curb inlets are primarily cast-iron type F-3 curb inlets with limited capacity. In some locations where valley gutters are present, valley grates are used.

The following is a description of the system beginning downstream at the outfall. The outfall consists of a sand-cement rip-rap reinforced endwall with a 60"x36" concrete box culvert main trunk line. This line proceeds down SW 1<sup>st</sup> Court where it picks up a small off-site system to the west from SW 9<sup>th</sup> Street. The main trunk line then crosses the MDT corridor onto SW 1<sup>st</sup> Avenue and decreases in size to a 54"x30" concrete box culvert. The main trunk line proceeds south along SW 1<sup>st</sup> Avenue decreasing in size after each street block from 42"x30" to 36"x30" to 21" circular. Per the as-built drawings all culverts are described as concrete. The first Branch to the trunk line extends along SW 10<sup>th</sup> Street where a 24"x15" culvert collects the major depression just east of SW 1<sup>st</sup> Avenue. Two other branches extend into SW 11<sup>th</sup> Street and SW 12<sup>th</sup> Street collecting the mid-block depressions just east of SW 1<sup>st</sup> Avenue.

A secondary trunk line branches from the main trunk line at the intersection of SW 1<sup>st</sup> Avenue and 9<sup>th</sup> Street and extends down 9<sup>th</sup> Street to the East. This line begins as a 36"x24" box culvert

all along SW/SE 9<sup>th</sup> Street collecting from the mid-block depression just east of SW 1<sup>st</sup> Avenue, 4 inlets at South Miami Avenue, and the major depression at SE 1<sup>st</sup> Avenue. This secondary trunk line continues along SE 1<sup>st</sup> Avenue and ranges in size from 30"x19" to 23"x14" to 15" circular and collects the inlets at the 10<sup>th</sup> Street and 11<sup>th</sup> Street intersections. Throughout the entire system, the trunk and branch lines run within the pavement and are connected to the curb inlets through 12" concrete cross drains. Some cross drains terminate at manhole structures and others are cored directly into the box culverts. **Figure 7** depicts the Mary Brickell Village Project Basin Map and existing drainage system layout.

Currently it has been observed that the existing drainage system is not adequate for disposing of runoff in a reasonable amount of time and within reasonable flood limits. There are two major depressions within the area that the study will focus on in order to determine the efficiency of the proposed improvements when compared to the pre-mitigation or existing condition. The major depressions are at the intersection of SE 9<sup>th</sup> Street and 1<sup>st</sup> Avenue and along SW 10<sup>th</sup> Street just east of 1<sup>st</sup> Avenue. During a recent site visit in December of 2009, extreme flooding was experienced firsthand. **Figure 6** depicts a picture of the flooding experienced at the peak of this particular storm. Unfortunately rainfall data specific to this area is not readily available so a true calibration of the model was not possible, but data from nearby station recorded nearly 1.75" of rainfall in less than an hour. These depressions often experience this level of flooding and beyond, to the point where the adjacent shops have sustained water damage, particularly along SW 10<sup>th</sup> Street.



**FIGURE 6 FLOODING AT THE INTERSECTION OF SE 9<sup>TH</sup> STREET AND 1<sup>ST</sup> AVENUE**

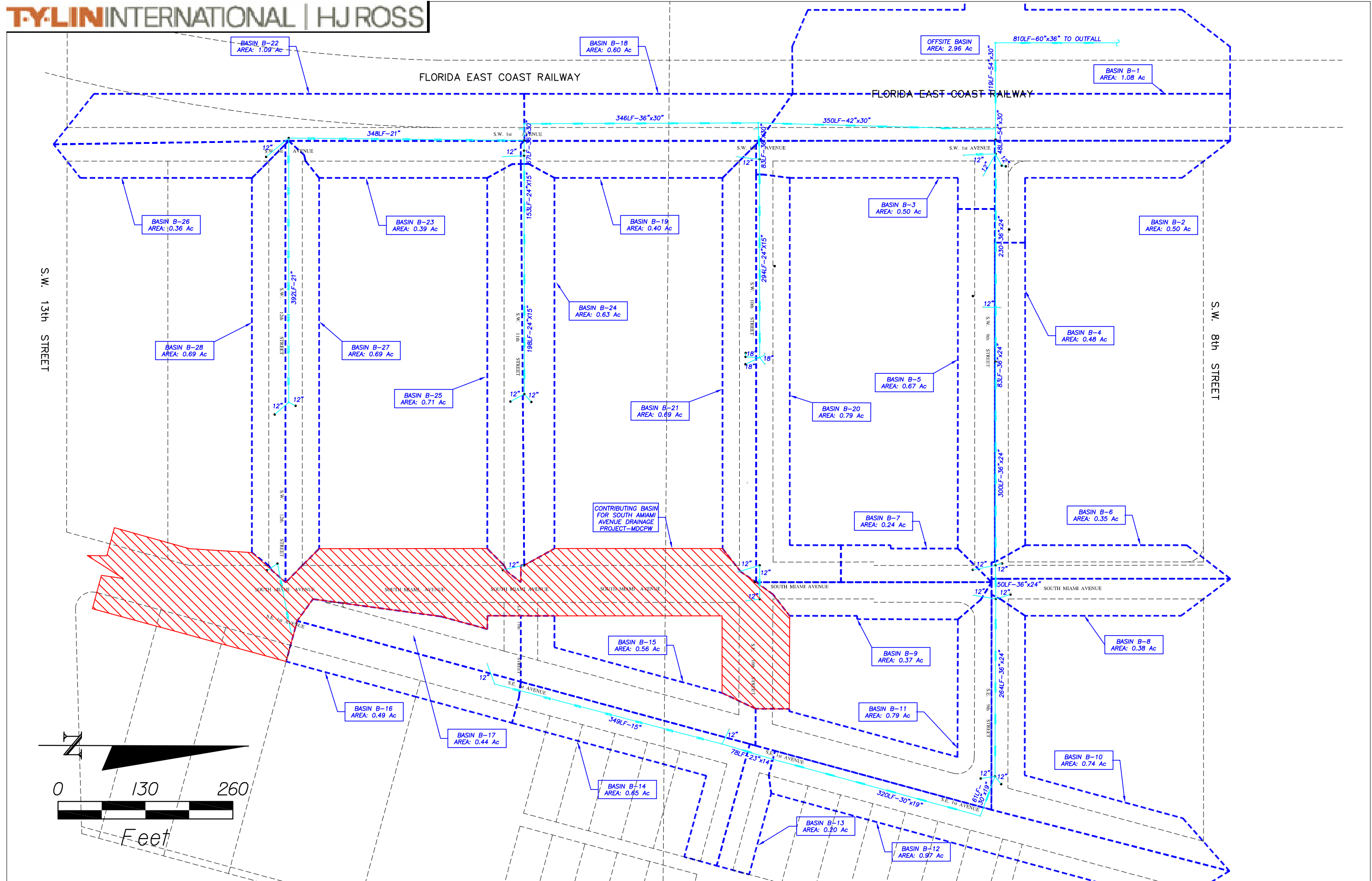


FIGURE 7: MARY BRICKELL VILLAGE PROJECT DRAINAGE MAP



## 2.8 CONTRIBUTING FACTORS

There are several major contributing factors to the frequent and intense flooding experienced within the project area. The following are some of those factors:

1. ***Outdated and Undersized System and the Impacts of Land Use Changes*** – The existing drainage system was constructed in the 1950's and was sized appropriately for the land uses of the day. In the past decade there has been a massive change in the zoning profile of this community. Where small restaurants and duplex condominiums once stood are now 40 story high rises and expansive shopping plazas. Although most of these developments have in some way mitigated for their impacts, the inevitable increase in runoff to the City streets as a results of the increased impervious area, and massive building faces (which add to the contributing basin areas) have been realized. Currently the system is not sufficiently sized to accommodate for this increase runoff. No major improvements to the original system have been made following the recent developments. The existing inlets, 12" cross drains, and concrete box culverts are still in use. As part of this report the upgrading of key system features will be explored.
2. ***Tidal Dependency*** – The existing drainage is a simple gravity sewer with discharge directly to the Miami River. As with any gravity system, its performance is fully dependant on the tailwater condition which in this case is the water level at the River. The discharge point at the River lies downstream of the final SFWMD control structures and as such is fully susceptible to tidal fluctuations. High tide elevations are on the order of 2.60'. When combined with the low ground elevations at the major depressions and the head losses through the system, there is less than 1' of vertical storage available in the system at these key areas. The results are extreme flooding when rain events coincide with high tide. Flooding typically does not subside until the high tide has passed. To correct this deficiency, a controlled tailwater condition that can be manipulated is required to maintain a functioning gravity system. The method by which this can be accomplished is through the use of a pump station. All of the proposed alternative designs will include a pump station as the primary drainage component.
3. ***High Water Table*** – The October-high water table in this area is above 2.25'. There is very little vertical storage available between this level and that of the low surface elevations.
4. ***Limited Vertical Relief and Extremely Low Surface Grades*** - Existing project area is subjected to the bowl effect. There are two major depressions where adjacent surface elevations are substantially higher isolating runoff to these depressions and not allowing discharge by overland relief. Under some circumstances, runoff may actually flow into, rather than out of these depressions since the head differentials are not present to move water out. The major depressions at SE 9<sup>th</sup> Street and 1<sup>st</sup> Avenue, and SW 10<sup>th</sup> Street just east of 1<sup>st</sup> Avenue have lowest grade elevations on the order of 3.50' with some grates even lower. When combined with the higher adjacent grades, high boundary condition, and high water table, the extreme flooding witnessed occurs.
5. ***Poor Subsurface Percolation*** – Due to the extremely high water table and low surface elevations, exfiltration trenches are inadequate for primary drainage in this area. They may be useful in some of the basins where higher surface elevations are

present such as along SW 12<sup>th</sup> Street and the southern portion of SE 1<sup>st</sup> Avenue, and may be utilized to provide water quality treatment. However, because the primary source of drainage that will be proposed is a pump station, exfiltration trenches will not be widely proposed in order to avoid pumping of ground water.

6. **Limited Maintenance** – The project area is a highly developed urban landscape with a high volume of vehicular and pedestrian traffic. As such there is a much larger volume of pollutants, including large waste debris, being introduced into the catch basins than would be introduced in a typical residential street. During several site visits, it has been observed that many of the inlets are full of debris or heavily silted. This can greatly diminish the efficiency of the system and certainly cause spot flooding in locations where the catch basins or pipes are clogged with debris. As part of the memorandum, we would recommend that the City increase its maintenance activities in the area to account for the increased use of the City right-of-way.
7. **No Water Quality Considerations** - A major deficiency that the existing stormwater management system for the area has is a complete lack of water quality treatment. The system currently has direct discharge to the Miami River with no provisions for retaining the “first-flush” of runoff. As part of this memorandum several options will be explored and recommended for addressing water quality as part of the final design.

## 2.9 EXISTING FLOODING CONDITIONS

To ascertain the extent and level of flooding within the Mary Brickell Village project area, information from several sources was compiled.

- Site visits were conducted during rainfall events and photographs were taken to document the levels of flooding.
- Photographs were collected from the City for flooding conditions during extreme events.
- Meetings were held with DDA representatives in order to assess the complaints of the residents and business owners in the areas.

It was concluded that major areas of concern are along SW 10<sup>th</sup> Street midblock between SW 1<sup>st</sup> Avenue and S. Miami Avenue and the intersection of SE 9<sup>th</sup> Street and SE 1<sup>st</sup> Avenue. Extreme flooding was reported and witnessed in these areas and will be the focus of the design evaluation.

## SECTION 3 DESIGN AND EVALUATION CRITERIA

### 3.1 DESIGN CRITERIA

The City of Miami Public Works Department establishes design criteria related to their storm water management systems. The project also falls under the jurisdiction of DERM and SFWMD. Design criteria for these projects should follow the most stringent of these agencies requirements.

### 3.2 WATER QUALITY

The Department of Environmental Resources (DERM) and South Florida Water Management District (SFWMD) have jurisdiction over the stormwater quality criteria for this project. In many instances, geological conditions do not permit full onsite retention of the design runoff due to poor soil infiltration, and in such instances, Miami-Dade County encourages the retention of at least the first inch of runoff. Because most contaminants are considered to be contained in the first inch of runoff, this rule is intended to at least meet the water-quality objectives of stormwater-management systems, even if the water-quantity objectives cannot be met. Supplementary systems, such as emergency overflow pipes that allow excess water to be discharged into off-site surface-water bodies, are used to provide flood protection.

The following are the accepted water quality criteria for the project area per the environmental agencies:

*SFWMD:*

- The first one inch of runoff times the total project (basin) area.
- The total runoff from 2.5 inches times the impervious area.

*DERM:*

- Retain one inch of storm water runoff on-site from the farthest point of the drainage basin to the point prior to discharging offsite (DERM criteria).

Of the three criteria, for the project parameters, the DERM criterion is most stringent and will be used to assess water quality.

The primary method of complying with storm water treatment requirements in South Florida is through the use of exfiltration trenches. Due to the low ground elevation and high water table, this method may not be utilized exclusively. If the improvements incorporate a storm water lift station, additional methods such as structural BMP's (vortex separators) and/or injection wells will be utilized as part of the proposed solutions to the flooding problems.

### 3.3 WATER QUANTITY

Another important aspect of storm water management systems in Florida is water quantity. The South Florida Water Management District (SFWMD) water-quantity requirements for stormwater-management systems must be met in addition to any other local municipal requirements. The SFWMD water-quantity requirements are as follows:

- **Off-site discharge**—The off-site discharge rate is limited to rates that do not cause adverse effects to existing off-site properties, historic-discharge rates, rates determined in previous District permit actions, or other rates specified by the District.
- **Design storm**—Unless otherwise specified by previous District permits or criteria, a storm event having a 25-year / 3-day duration return frequency must be used in computing off-site discharge rates. In instances where there is no off-site discharge, adequate aboveground onsite storage must be available to accommodate the 25-year / 3-day storm.
- **Flood protection of building floors**—Building floors must be at or above the 100-year flood elevations as determined from the most appropriate information, including Federal



Flood Insurance Rate Maps. Both tidal flooding and the 100-year 3-day storm event are considered in determining elevations.

- **Flood protection of roads and parking lots**—In instances where criteria are not specified by local government with jurisdiction, the design criteria used for drainage and flood protection are: 5-year 1-day storm for road centerlines, and 5-year / 1-hour storm for parking lots served by exfiltration systems.
- **Floodplain encroachment**—No net encroachment is allowed into the floodplain between the average wet-season water table and that encompassed by the 100-year event, which will adversely affect the existing rights of others.
- **Historic basin storage**—Provision must be made to replace or otherwise mitigate the loss of historic basin storage provided by the project site.

### 3.4 ALLOWABLE FLOOD LEVELS

The following are some of the flood level criteria as established by Miami-Dade County:

- All structures (commercial, residential) shall be flood-free during the 100-year storm event.
- Major evacuation routes, shall be passable during the 100-year storm event.
- Minor arterial (4-lane roads) shall be passable during the 10-year storm event.
- Collector and local residential streets shall be passable during the 5-year storm event.

The roadways being addressed as part of this project are considered local residential streets and will be designed to the 5-year storm event criteria. Flood stages cannot encroach upon the crown of the roadway to be defined as passable. Ponding will be defined as stages above the grate elevations and will also be documented as part this report.

### 3.5 PERMITTING REQUIREMENTS AND ENVIRONMENTAL AGENCY COORDINATION

The following are the required permits for this project depending on the final proposed solutions:

- Environmental Resource Permit (ERP).
- DERM Class II Permits
- USACE permits and DERM Class I Permits will be required if outfall reconstruction is proposed in the final design.

Permit applications have to be submitted to DERM. In addition to this a permit from the Florida Department of Environmental Protection (FDEP) will be required for drainage wells, if ultimately proposed. A permit from the City of Miami Public Works Department will also be required to construct within the right-of-way.

A pre-application meeting will be conducted with DERM and SFWMD staff to further define the project goals. Documentation of the meetings and conversations will be included under separate covers.

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## SECTION 4 MODEL METHODOLOGY

### 4.1 APPROACH

A detailed hydrologic/hydraulic analysis was performed to develop flood discharges and stages for the Mary Brickell Village project. The following sections describe the methodology and results of the hydrologic/hydraulic analysis completed for the existing project conditions described in Section 2. To conduct the analysis, a review of the following information was performed:

- Topographic survey of the existing conditions
- Record plans for the existing storm water management systems in the area
- Field reviews and site visits

The initial phase of the model construction was to create an AutoCAD Civil 3D drawing of all known drainage structures including catch basins, storm sewers, and exfiltration trenches from the field surveys and as-built records. In addition the surveyed elevations were used to develop the site topography and create a three dimensional model of the project area in order to identify basins and develop stage-storage relationships. Upon completion, a Drainage Map was produced that identified the drainage basins and drainage patterns and incorporated them into the hydrologic/hydraulic model network.

The model network is constructed of nodes and links where the hydrologic and hydraulic data of the model is stored. The nodes are typically storage nodes, junctions and outfalls whereas the links are the storm pipes and overland flow representations. The model was run for the following four design storm events: 5-year/24-hour, 10-year/24-hour, 25-year/72-hour, and 100-year/72-hour.

### 4.2 GENERAL MODEL INFORMATION

ICPR is a stormwater management analysis and design tool developed by Streamline Technologies, Inc. ICPR is a hydrodynamic model that simulates hydrologic and hydraulic conditions using conveyance features such as basins, nodes, and links.

The Interconnected Pond Routing (ICPR) computer model (Version 3.10) was used to analyze existing and proposed drainage conditions, and to verify that the required stormwater quantity criteria outlined in Section 3 is in compliance. The ICPR computer model simulated hydrologic and hydraulic conditions by generating runoff hydrographs and dynamically routing these hydrographs through diverging, looped, and/or bifurcated stormwater management systems.

In ICPR, the stormwater management system is divided into networks of nodes or junctions and links or reaches. A node is a discrete location in the drainage system where runoff enters the system and conservation of mass or continuity is maintained. Links represent connections between nodes and are used to transfer or convey stormwater runoff through the system. The links are used to model the hydraulic response of the system for a defined hydrologic condition.

### 4.3 HYDROLOGIC MODELING

ICPR uses three methods for generating stormwater runoff hydrographs: the Soil Conservation Service (SCS) unit hydrograph method, Santa Barbara Urban Hydrograph (SBUH) method and

kinematic overland flow method. For this project, the method selected for hydrograph generation is the Soil Conservation Service (SCS) Unit Hydrograph procedure as outlined in the USDA, SCS, "National Engineering Handbook, Section 4, Hydrology." This is one of the recommended SFWMD procedures found in the Environmental Resource Permit (ERP) Basis of Review (BOR) Manual and is the most appropriate method for the size of the drainage areas, land use, soil condition and regional location.

A dimensionless unit hydrograph with a peak factor of 256 was used for analysis, as is typical in South Florida.

The SCS unit hydrograph procedure requires input data describing the physical features of each drainage sub-basin in the system and generates runoff hydrographs using the following hydrologic parameters:

1. Basin areas (acres);
2. Curve numbers (CN);
3. Rainfall precipitation;
4. Rainfall distribution;
5. Storm Duration;
6. Time of Concentration (TOC).

Basin areas are calculated by analyzing the DTM generated by Civil 3D and is based on the surveyed elevations. Also taken into account when determining basin limits, is the interconnectivity of the storm sewer system. Finally, based on the recommendations of MD-DERM, The City of Miami Public Works Department, and other local agencies, basin areas are limited to the right-of-way area plus 25 feet on either side. In addition to the surface basin areas,  $\frac{1}{2}$  of the total high-rise building (over 3 stories) face area was added to the contributing area of the basins. This was done in order to simulate the capturing affect of the building faces when heavy rain falls at an angle. See **Figure 7** for the basis of calculations drainage basin map.

#### **4.3.1 CURVE NUMBER**

The Curve Number is dependent on land use, soils and topography.

Existing land use information for project is found in section 2.4.

Soil types for the study area were determined from Miami-Dade County NRCS Soil Survey and the subsurface soil exploration. Soil types were assigned a hydrologic soil group in accordance with *Guidelines for Determining Hydrologic Soils Groups*, see section 2.5.

The information used for relating land use and soil types to curve numbers was based on the imperviousness of the land use using the NRCS publication TR-55, latest edition. The percent impervious was obtained from the aerial shown on **Figure 1**. Due to the built out nature of the project area a curve number of 98 was used for all basins.

#### **4.3.2 RAINFALL PRECIPITATION**

Rainfall data is the single most important group of hydrological data required by ICPR. A hyetograph of rainfall intensities versus time is required for the period of the simulation. For single event simulation, the data is usually entered directly as a synthetic design storm.

The following design storm events were simulated in ICPR:

- 5 year – 24 hour
- 10 year – 24 hour
- 25 year – 72 hour
- 100 year – 72 hour

Table 6 depicts the design rainfall precipitation depths as obtained from the South Florida Water Management District Environmental Resource Permit (ERP) Basis of Review (BOR) Manual rainfall maps. See appendix A for the SFWMD rainfall maps.

Table 1 Design Rainfall Depths, inches

Return Period	24-Hour	72-Hour
5-year	6.30	--
10-year	7.90	--
25-year	--	12.00
100-year	--	14.00

### 4.3.3 RAINFALL DISTRIBUTION

The unit hydrograph was distributed over time using the Florida Modified Type II 24-hour Distribution and the South Florida Water Management District 72-hour Distribution with an antecedent moisture condition (AMC) of II.

The design rainfall distribution defines how the mass rainfall is distributed throughout the storm event. The SFMWD 72-hour distribution was used for the 25-year / 72-hour and 100-year / 72 hour storm events. The SCS Type II Florida Mod distribution was used for the 5-year / 24-hour, and 10-year / 24-hour.

### 4.3.4 TIME OF CONCENTRATION (TOC)

The drainage basin TOC is the time for a drop of water to reach the basin discharge point from the most hydraulically remote point in the basin. It is typically computed utilizing the kinematic wave equation for overland flow as outlined in the NRCS publication TR-55. However the pre-development and post-development drainage basins of the project are relatively small and highly impervious. The drainage system also offers wide coverage in each of the sub-basins. Because of this the travel times from the most hydraulically remote point to a system catch basin is relatively low. For these reasons, all of the sub-basins are conservatively presumed to have TOC less than 10 minutes. Therefore, a TOC of 10 minutes was assumed for all basins where the majority of runoff occurs via overland flow.

## 4.4 HYDRAULIC DATA

Peak water-surface elevations for the design storm events were computed using the ICPR computer program. ICPR uses a link-node network to describe the physical model. Nodes are the storage elements and correspond to manholes and junctions. The conduit system is idealized as a series of links or conduits that are connected at nodes or junctions. Once ICPR generates the runoff hydrographs, the program then routes the hydrographs through the model network.

#### 4.4.1 NODE DATA

Node data is required for every node in the network including junction nodes, storage nodes, and outfall nodes. Appendices E and F list the Node Input data for both the pre-development (existing) and post-development models. Following are the node input parameters:

- **Node Name** - the node name is the same as the name of the sub-basin that contains it, and surface runoff from the sub-basin is directed to the node. Not every node in the model has surface runoff directed to it.
- **Node Type** – The project basin nodes with storage will be modeled as stage-volume nodes with stage-volume relationships derived from the Civil 3D generated DTM based on the surveyed topography. Below ground storage is calculated by taking into account the cross-sectional area of the particular drainage structure.
- **Base Flow** – there will be no base flows modeled in this project
- **Initial Stage** – this is the initial node depth or starting water surface elevation. The design boundary condition/river elevation was used for all of the nodes as the initial stage in order to begin with a stable model with no flow.
- **Warning Stage** – warning stages will be set at the lowest grate elevation to display when the inlets are surcharging.

#### 4.4.2 BOUNDARY CONDITIONS

The only boundary condition node for this project will be the surface tail-water elevation at the outfall along the Miami River. The high-high tide elevation will be used as both the boundary condition and starting ground water level. The design high tide was derived from field observations and corresponds to 2.60' City of Miami Datum. See section 2.3.

#### 4.4.3 LINK DATA

There are several different types of links in the hydraulic model. The main types utilized in this project are pipes, channels, weirs, and rating curves. It should be noted that it is being assumed that the system is clean and free of major debris and/or silt and is modeled as such.

Appendices E and F list the Link Input data for both the pre-development (existing) and post-development models. The size, shape, material, inverts and lengths for the existing culverts were obtained from the topographic survey prepared by J. Bonfill and Associates, Inc. or from the as-built drawings. Following is a description of some of the link input parameters:

- **Manning's Roughness** - Manning's Roughness is a standard indicator of the smoothness of the conduit. Roughness values for culverts and force mains are based on culvert material and condition. A value of 0.012 was used for reinforced concrete pipes and a value of 0.024 for corrugated metal pipes. A value of 0.011 was used for ductile iron pipe force mains. A roughness of 0.08 was estimated for natural overland flow channels. Entrance and exit losses were taken into account based on FDOT standards.
- **Natural Channels (Overland Weirs)** - Occasionally it is necessary to perform routing on the water that floods onto the ground. A Natural channel conduit is constructed for the overland flow paths to transport the flooded water from the ground elevation of the upstream junction to the ground elevation of the downstream junction or vice versa. The natural channel shape consists of coordinate pairs for the positions in feet (**X**) and elevations (**Stage**) at

each coordinate. If the left-most or right-most elevations are less than the maximum value, vertical sides are projected up to the high point as shown in the above figure. Data for the channel cross sections was obtained from the DTM.

#### 4.5 MODEL CALIBRATION

The model was calibrated by modeling the storm event witness on December 17, 2009. The nearest rain gauges recorded approximately 1.22" in an hour near the airport. It was estimated that nearly 2" fell in our area within the hour. This has based on the fact that the storm traveled in an east-west pattern that day and no other rain gauge data is readily available near the project area. The results of the model were within inches of the witnessed flood levels depicted in **Figure 6**. It was determined that the model is adequately calibrated as the model did not take into account the observed debris and silt found in many of the catch basins throughout the project. This reduced efficiency would have no doubt raised the modeled flood levels closer to the observed flood levels.

## SECTION 5 ANALYSIS OF PRE-DEVELOPMENT CONDITIONS

Once the ICPR model was completed and the calibration process conducted, the existing conditions system was simulated for the four design storm events. **Figure 9** shows the Existing Conditions Node-Link Diagram. Appendix E contains all the input and output data on the pre-development (existing) ICPR model. Table 2 shows the results of the analysis for the existing condition nodes.

There are several assumptions made during the modeling process. As stated in section 4.3, the drainage basin area taken into account were up to 25' beyond the right-of-way in either direction plus the high-rise building face area. In addition, the contributing basin along S. Miami Avenue that will be addressed by the Miami-Dade County Public Works drainage project that is currently under construction was disregarded as a contributing area to this model. This model assumes that said project is complete and functioning as designed. The final assumption is that the system is clean and free of debris. Taking these factors into account, the system is being modeled in its optimal state.

As is evident from the results, several of the existing basins have substandard flood conditions. Of the 28 basins, 12 were identified as having flooding conditions beyond the acceptable criteria. Of interest are the particular critical basin nodes which correspond to the major 9<sup>th</sup> Street and 10<sup>th</sup> Street depressions. The following basins correspond to the depression at SE 9<sup>th</sup> Street and SE 1<sup>st</sup> Avenue: **Basins B-10, B-11, B-12, and B-13**. The following basins correspond to the depression midblock along SW 10<sup>th</sup> Street east of SW 1<sup>st</sup> Avenue: **Basins B-21 and B-22**. These basins will serve as the barometer for determining the effectiveness of the proposed alternatives. It should also be mentioned that the maximum discharge rates to the canal for the 25yr-72hr storm event, which serves as the criteria for offsite discharge, was 59.94 CFS.

**TABLE 2 PRE-DEVELOPMENT CONDITIONS FLOOD STAGE SUMMARY**

Node	5yr-24hr	10yr-24hr	25yr-72hr	100yr-72hr	Warning Stage (Grate or Top Elev.)	Criterion Stage (Lowest Crown Elev.)	5yr Ponding Depth over Grate	5yr Criterion Flood Depth
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(in)	(in)
B-1	4.20	4.42	5.03	5.17	3.80	4.15	4.79	0.59
B-2	4.73	5.04	5.51	5.73	3.96	4.16	9.22	6.82
B-3	4.40	4.63	5.13	5.28	3.96	4.16	5.27	2.87
B-4	4.65	4.88	5.32	5.48	3.12	4.11	18.36	6.48
B-5	4.70	4.93	5.35	5.51	3.69	4.11	12.16	7.12
B-6	4.92	5.18	5.54	5.71	4.87	5.23	0.65	-
B-7	4.91	5.17	5.54	5.70	5.22	5.54	-	-
B-8	5.03	5.29	5.62	5.79	4.90	5.23	1.58	-
B-9	5.03	5.29	5.62	5.79	4.86	5.54	2.09	-
B-10	5.18	5.45	5.75	5.92	4.11	4.36	12.82	9.82
B-11	5.21	5.47	5.76	5.94	4.06	4.36	13.76	10.16
B-12	5.28	5.57	5.86	6.05	4.15	4.55	13.55	8.75
B-13	5.47	5.80	6.08	6.29	5.87	6.03	-	-
B-14	5.78	6.16	6.45	6.69	5.70	6.16	0.91	-
B-15	5.92	6.30	6.57	6.81	5.66	6.16	3.06	-
B-16	6.41	6.95	7.37	7.75	8.13	8.28	-	-
B-17	6.51	7.07	7.51	7.92	8.15	8.28	-	-
B-18	4.51	4.77	5.29	5.45	4.03	4.84	5.80	-
B-19	4.59	4.87	5.33	5.50	4.37	4.84	2.65	-
B-20	4.78	5.04	5.44	5.62	3.67	4.02	13.32	9.12
B-21	4.79	5.04	5.45	5.62	3.83	4.02	11.47	9.19
B-22	4.73	5.02	5.49	5.68	5.31	5.86	-	-
B-23	4.92	5.24	5.67	5.87	5.34	5.86	-	-
B-24	5.31	5.64	5.98	6.21	4.20	4.60	13.32	8.52
B-25	5.52	5.86	6.18	6.43	4.20	4.60	15.82	11.02
B-26	5.82	5.93	6.41	6.75	9.94	10.33	-	-
B-27	6.38	6.94	7.36	7.71	5.90	6.43	5.75	-
B-28	6.30	6.82	7.22	7.54	5.80	6.43	5.99	-
WATER WAY	2.60	2.60	3.80	3.80	N/A	N/A	N/A	N/A



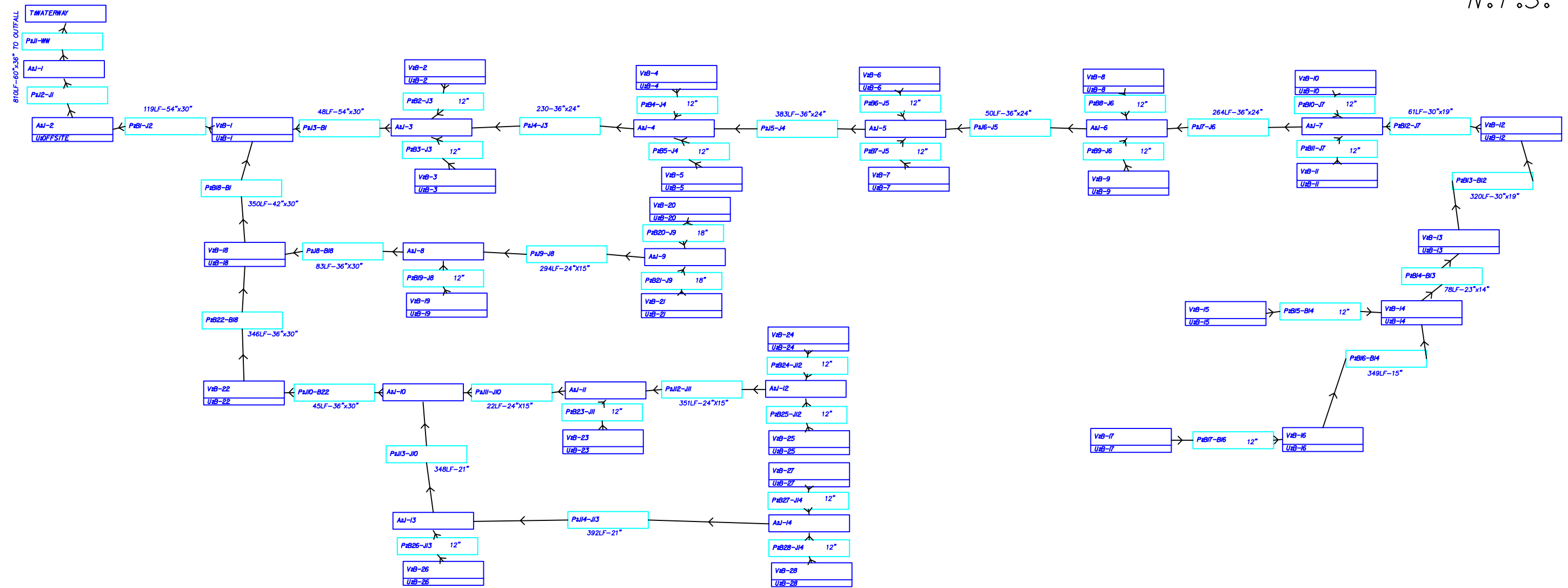
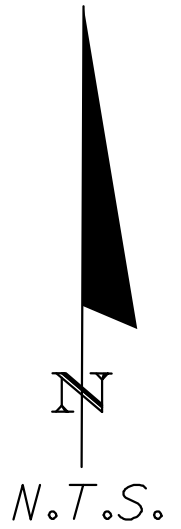


FIGURE 8: PRE-DEVELOPMENT NODE-LINK DIAGRAM



## SECTION 6 ANALYSIS OF POST-DEVELOPMENT CONDITIONS

### 6.1 OBJECTIVES

In order to minimize the cost and environmental impacts of the proposed project, several options for the proposed drainage improvements were analyzed as part of a technical memorandum finalized in February 2011. In all cases the options considered had to meet the objectives listed below:

- Maximize the utilization of existing drainage systems,
- Minimize the need for additional Right-of Way acquisition,
- Minimize environmental impacts, and
- Minimize project cost

In order to minimize project cost and to minimize environmental impacts it was decided to attempt to utilize as much of the existing trunk lines as possible. Furthermore it was decided that due to the restrictive nature of the existing topography and boundary conditions, any improvements proposed would require a pump station as the primary method of discharge.

The following section describes the proposed storm water management improvements that were selected as part of the technical memorandum. Appendix F lists the ICPR model input and output data, and Appendix H lists the Cost Estimates of the improvements.

### 6.2 ANALYSIS OF PROPOSED IMPROVEMENTS – ALTERNATIVE 1

The first alternative involves the addition of a new pump station to accommodate the runoff from the entire project basin. The pump station location is proposed within the City right-of-way along SW 1<sup>st</sup> Court west of the MDT Metrorail corridor just north of 9<sup>th</sup> Street along the existing parking lane. **Figure 9** shows pictures depicting the area where a pump station could be constructed. There are minimal utility conflicts and no encroachment into the MDT right-of-way. This proposed location will also be used for Alternative 2.

For Alternative 1 the entire existing storm sewer system was maintained intact in order to demonstrate the inefficiency of existing cross drains and branch lines to convey water from the depressions to the boundary node which in this case is now the wet well of the pump station. A bypass system was modeled using two additional junction nodes. The pump station itself was modeled with a 15'x25' wet well node depicting a stage vs. area storage relationship. The pumps were modeled utilizing a rating curve and an operating table defining a head vs. discharge where head is defined as the difference between the upstream and downstream stages. For the purposes of determining the optimum pump rate, a constant rate operating table was used where discharge was constant over the full range of possible head levels. Finally "dummy" nodes were introduced to represent the pump outlets, pipes with equivalent lengths were used to model the pump discharge pipes and valves, and a "dummy" node was used to represent the connection of the discharge pipes to the force main. The advantage of the pump station system is that the tail-water elevation can be manipulated to allow for increased flows. For this model the tail-water elevation corresponds to the pump start elevations which were set at 0.00' and 1.50' for lead and lag pumps respectively.

For modeling purposes the pump station was set-up as a duplex station with constant rate pumps. In reality a triplex station may be required depending on the horsepower requirements



**FIGURE 9 POSSIBLE PUMP STATION LOCATION SW 1<sup>ST</sup> COURT NORTH OF 9<sup>TH</sup> STREET**

of the specific pumps. Different pump rates were modeled for the design criteria storm (ranging from 40 CFS to 60 CFS pumps). Peak stage elevations in the critical nodes (see section 5) were compared for the various pumping rates, and through the utilization of a “point of diminishing returns” method, an optimal pump rate was chosen.

For purposes of comparison, nodes B-12 and B-22 were chosen as critical nodes and peak stages were compared for various pump rates for the criteria event (5yr). For two 20 CFS pumps the peak stages were 5.00’ and 4.51’ respectively. For two 30 CFS pumps the peak stages were 4.91’ and 4.37’ respectively. And for two 40 CFS and even 50 CFS pumps the peak stages were 4.91’ and 4.37’ respectively. As is evident from the results, extreme variations in the pump rates had no affect on the peak stages at the critical depressions of the project once the total outflow surpassed 60 CFS. This finding demonstrates that the existing drainage system is hydraulically maxed out at between 40CFS and 60CFS of total flow, pumping any more will not yield any gains as the pipes will be controlling or “choking” the flow. In addition although the results demonstrate much reduced peak stages, several nodes including the critical basins continue to show peak stages beyond the criteria. The subsequent alternatives will determine what improvements that must be made to the conveyance system, branch lines, and cross drains in order to take advantage of the controlled tailwater condition created by the use of the pump station and meet the flood criteria. Table 3 shows the results of the analysis of the proposed improvements – Alternative 1 utilizing two 40 CFS pumps (80 CFS total).

**TABLE 3 POST-DEVELOPMENT ALTERNATIVE 1 FLOOD STAGE SUMMARY**

Node	5yr-24hr	10yr-24hr	25yr-72hr	100yr-72hr	Warning Stage (Grate or Top Elev.)	Criterion Stage (Lowest Crown Elev.)	5yr Ponding Depth over Grate	5yr Criterion Flood Depth
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(in)	(in)
B-1	3.37	3.76	3.99	4.20	3.80	4.15	-	-
B-2	4.19	4.66	4.90	5.18	3.96	4.16	2.70	0.30
B-3	3.75	4.18	4.38	4.58	3.96	4.16	-	-
B-4	4.12	4.50	4.66	4.86	3.12	4.11	12.04	0.16
B-5	4.25	4.60	4.76	4.96	3.69	4.11	6.74	1.70
B-6	4.45	4.85	5.04	5.25	4.87	5.23	-	-
B-7	4.44	4.83	5.01	5.23	5.22	5.54	-	-
B-8	4.60	5.01	5.19	5.40	4.90	5.23	-	-
B-9	4.61	5.01	5.18	5.39	4.86	5.54	-	-
B-10	4.83	5.20	5.37	5.59	4.11	4.36	8.58	5.58
B-11	4.88	5.24	5.41	5.62	4.06	4.36	9.83	6.23
B-12	4.91	5.33	5.52	5.75	4.15	4.55	9.06	4.26
B-13	5.09	5.57	5.78	6.03	5.87	6.03	-	-
B-14	5.38	5.92	6.18	6.46	5.70	6.16	-	-
B-15	5.53	6.08	6.34	6.61	5.66	6.16	-	-
B-16	5.88	6.58	6.95	7.39	8.13	8.28	-	-
B-17	5.95	6.68	7.07	7.53	8.15	8.28	-	-
B-18	3.81	4.24	4.50	4.74	4.03	4.84	-	-
B-19	3.93	4.41	4.70	4.93	4.37	4.84	-	-
B-20	4.35	4.73	4.91	5.13	3.67	4.02	8.17	3.97
B-21	4.37	4.74	4.92	5.14	3.83	4.02	6.42	4.14
B-22	4.08	4.54	4.84	5.11	5.31	5.86	-	-
B-23	4.34	4.82	5.13	5.42	5.34	5.86	-	-
B-24	5.00	5.38	5.58	5.86	4.20	4.60	9.55	4.75
B-25	5.26	5.66	5.87	6.16	4.20	4.60	12.76	7.96
B-26	5.82	5.93	6.00	6.31	9.94	10.33	-	-
B-27	5.90	6.56	6.91	7.37	5.90	6.43	-	-
B-28	5.84	6.51	6.87	7.26	5.80	6.43	0.43	-
WATER WAY	2.60	2.60	3.80	3.80	N/A	N/A	N/A	N/A

### 6.3 ANALYSIS OF PROPOSED IMPROVEMENTS – FINAL DESIGN

The intent of final design was to determine what improvements needed to be made to the existing drainage system in order to allow the pump station to function efficiently. The initial iterations of this alternative included major improvements to the main outfall along SW 1<sup>st</sup> Court. However upon several modeling runs, it was determined that peak stages within the criteria could be achieved through improvements of the branch and secondary systems only. Through a method of trial and error, the model was run repeatedly in order to identify links that were “choking” the system. This was done by comparing upstream and downstream stages, or the head losses, for each link and identifying links with significant head losses. Subsequent model runs with larger pipe sizes were run until optimal sizes were obtained. The following is a list of the improvements proposed to the existing drainage system in addition to the pump station at SW 1<sup>st</sup> Court and 9<sup>th</sup> Street as described in section 6.2:

- All cross drains connecting the curb inlets with branch lines within the affected project area will be upgraded to a minimum diameter of 18”. The existing system has pipe diameters typically of 12”.
- The secondary trunk line along SW/SE 9<sup>th</sup> Street will be increased in diameter accordingly: 48” from node B-1 to J-4, 42” from node J-4 to J-5 with an intermediate manhole (not modeled) reducing the size to 36”. The remainder of the trunk lines will remain the existing sizes.
- The branch line along SW 10<sup>th</sup> Street will be increased in size from 24”x15” box culvert to a 30” diameter pipe.
- The branch line along SW 11<sup>th</sup> Street will be increased in size from 24”x15” box culvert to a 30” diameter pipe.
- The system along SW 12<sup>th</sup> Street will be effectively disconnected from the pump station system. This roadway is at a higher elevation where the use of exfiltration trenches is feasible. An isolated exfiltration trench system will be used here with a control structure installed between it and the pump station system. The control structure will be comprised of an overflow weir. The purpose of this action is to minimize the contributing area to the pump station and was required to meet the flood criteria requirement and also maintain the use of the existing primary trunk lines. See appendix B for the miscellaneous calculations sizing the exfiltration trench for this basin.
- The system at the intersection SE 11<sup>th</sup> Street and SE 1<sup>st</sup> Court will also be effectively disconnected from the pump station system. This intersection is at a much higher elevation where the use of exfiltration trenches is feasible. An isolated exfiltration trench system will be used here with a control structure installed between it and the pump station system. The control structure will be comprised of an overflow weir. The purpose of this action is to minimize the contributing area to the pump station and was required to meet the flood criteria requirement and also maintain the use of the existing primary trunk lines. See appendix B for the miscellaneous calculations sizing the exfiltration trench for this basin.
- Finally, although this feature is specifically not modeled, all catch basins and curb inlets within the affected project area will be upgraded from the existing type F-3 curb inlets to FDOT type 3 or 4 style inlets tops in order to increase the throat capacity.

As with Alternative 1, different individual pump rates were modeled for the design criteria storm (ranging from 0 CFS to 40 CFS pumps). Peak stage elevations in the critical nodes (see Appendix C) were compared for the various pumping rates, and through the implementation of a “point of diminishing returns” method, an optimal pump rate was chosen.

Based on the model findings, individual pumping rates beyond 30 CFS did not yield any appreciable reductions in the peak stages. This finding suggests that the conveyance system has reached its hydraulic potential and this is optimal pumping rate. A pumping rate of two 32 CFS pumps was utilized to account for a factor of safety.

As part of the water quantity criteria that will be required of DERM, the proposed system would have to mitigate for the additional flow discharged during the 25yr-72hr storm event. Due to the limited space found in this project area, the only feasible method to dissipate excess flow is the though the use of injection wells. Since the project area is located east of the current salt-water intrusion line, it can be permitted for the use of injection drainage wells with discharge into the G-III aquifer.

From recent projects in the area, it is estimated a conservative rate of 600 gpm/ft of head is available for a given well. It is also known that in this area approximately 1.5 ft of head required to overcome salinity mounding. Per FDEP standards, the maximum permitted peak stage upstream of an injection well is 8.0’ NGVD. Taking these factors into account, along with a water table elevation of approximately 2.0’ NGVD, a well in this area would have an available head of 4.5’. This would yield a rate of 2700gpm or 6 CFS. It is estimated then that 5 wells will be required to meet the 25 year storm event requirement. In other similar projects with discharge to the bay, the local agencies have been permitted to maintain a certain discharge velocity in lieu of adding wells to mitigate for additional flow. This is due to the excessive cost and space requirements associated with so many injection wells. In said projects DERM usually requested maintaining a discharge velocity of under 5 ft/sec. In this project we are proposing 2 wells to maintain a discharge velocity of **3.51 ft/sec** for the 25yr/72hr event.

Table 4 shows the results of the analysis of the final proposed improvements – utilizing two 32 CFS pumps. Figure 11 compares a time vs. stage graph of the critical node B-21 in the pre-mitigation condition and the proposed post-mitigation condition. This comparison serves to demonstrate the effectiveness of the pump station system in not only reducing the peak stages but also the flooding duration.

**TABLE 4 POST-DEVELOPMENT FINAL DESIGN FLOOD STAGE SUMMARY**

Node	5yr-24hr	10yr-24hr	25yr-72hr	100yr-72hr	Warning Stage (Grate or Top Elev.)	Criterion Stage (Lowest Crown Elev.)	5yr Ponding Depth over Grate	5yr Criterion Flood Depth
	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(in)	(in)
B-1	3.36	4.04	4.24	4.53	3.80	4.15	-	-
B-2	3.56	4.25	4.49	4.82	3.96	4.16	-	-
B-3	3.46	4.13	4.37	4.68	3.96	4.16	-	-
B-4	3.53	4.17	4.41	4.73	3.12	4.11	4.92	-
B-5	3.61	4.24	4.46	4.78	3.69	4.11	-	-
B-6	3.72	4.38	4.63	4.95	4.87	5.23	-	-
B-7	3.70	4.35	4.61	4.92	5.22	5.54	-	-



B-8	3.94	4.58	4.84	5.13	4.90	5.23	-	-
B-9	3.95	4.59	4.86	5.13	4.86	5.54	-	-
B-10	4.18	4.78	5.01	5.30	4.11	4.36	0.84	-
B-11	4.20	4.80	5.03	5.31	4.06	4.36	1.68	-
B-12	4.26	4.88	5.15	5.42	4.15	4.55	1.32	-
B-13	4.37	5.00	5.32	5.60	5.87	6.03	-	-
B-14	4.51	5.20	5.58	5.88	5.70	6.16	-	-
B-15	4.70	5.51	5.92	6.22	5.66	6.16	-	-
B-16	Isolated Exfiltration Trench System - See Water Quality Calculations							
B-17	Isolated Exfiltration Trench System - See Water Quality Calculations							
B-18	3.79	4.42	4.63	4.91	4.03	4.84	-	-
B-19	3.84	4.47	4.68	4.95	4.37	4.84	-	-
B-20	4.03	4.62	4.81	5.07	3.67	4.02	4.32	0.12
B-21	4.06	4.63	4.82	5.08	3.83	4.02	2.76	0.48
B-22	4.01	4.62	4.85	5.14	5.31	5.86	-	-
B-23	4.19	4.79	5.04	5.34	5.34	5.86	-	-
B-24	4.40	5.00	5.23	5.53	4.20	4.60	2.40	-
B-25	4.55	5.13	5.37	5.67	4.20	4.60	4.20	-
B-26	5.82	5.93	6.00	6.09	9.94	10.33	-	-
B-27	Isolated Exfiltration Trench System - See Water Quality Calculations							
B-28	Isolated Exfiltration Trench System - See Water Quality Calculations							
W-1	7.19	7.19	8.00	8.00	8.00	8.00	N/A	N/A
W-2	7.19	7.19	8.00	8.00	8.00	8.00	N/A	N/A
WATER WAY	2.60	2.60	3.80	3.80	N/A	N/A	N/A	N/A
WETWELL	2.10	2.47	2.77	3.15	N/A	N/A	N/A	N/A

Notes:

1. Junction nodes, identified as J-# in the model, are not depicted in this table. These nodes are representations of manholes and do not exhibit ponding.
2. Nodes W-1 and W-2 represent the upstream point of the drainage wells. These elevations are shown to depict compliance with FDEP's maximum allowable head over an injection well which is an elevation of 8.00'.

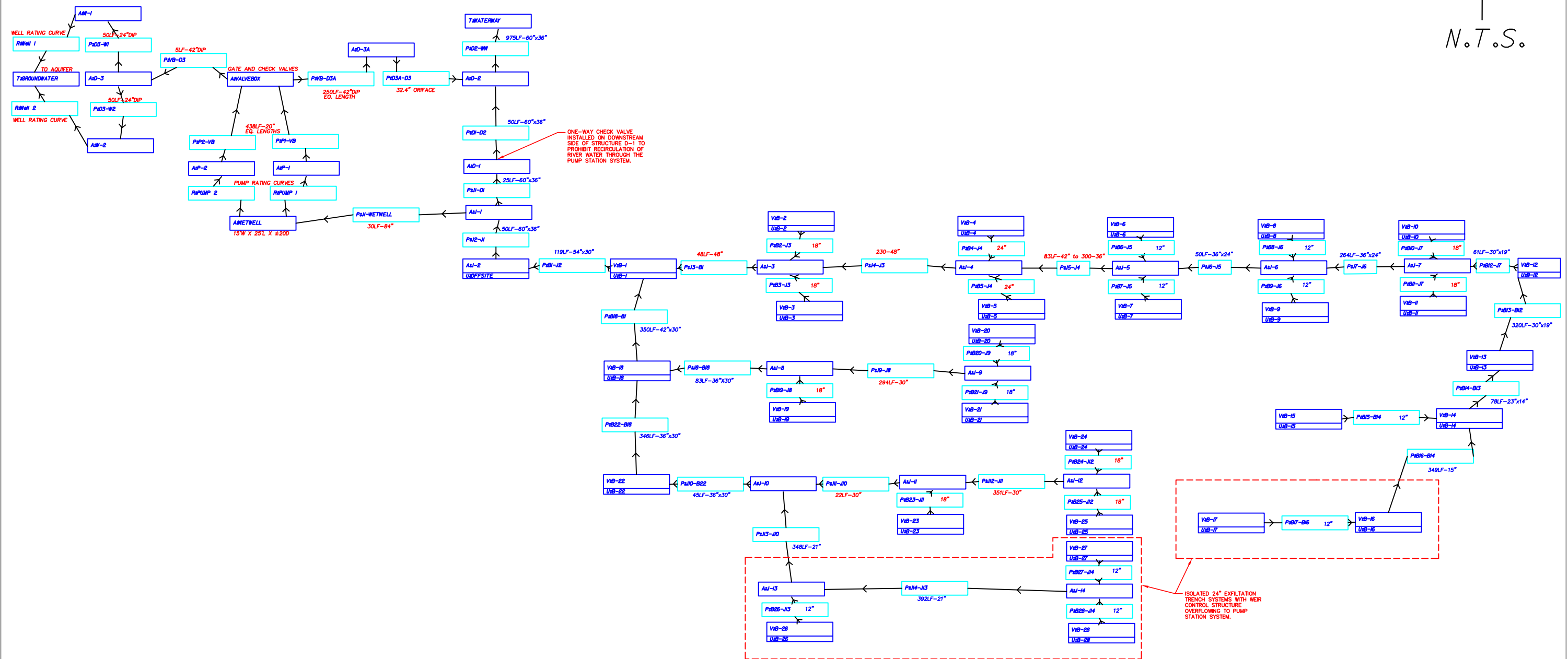
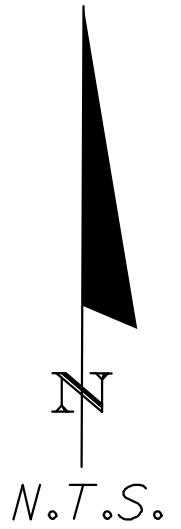
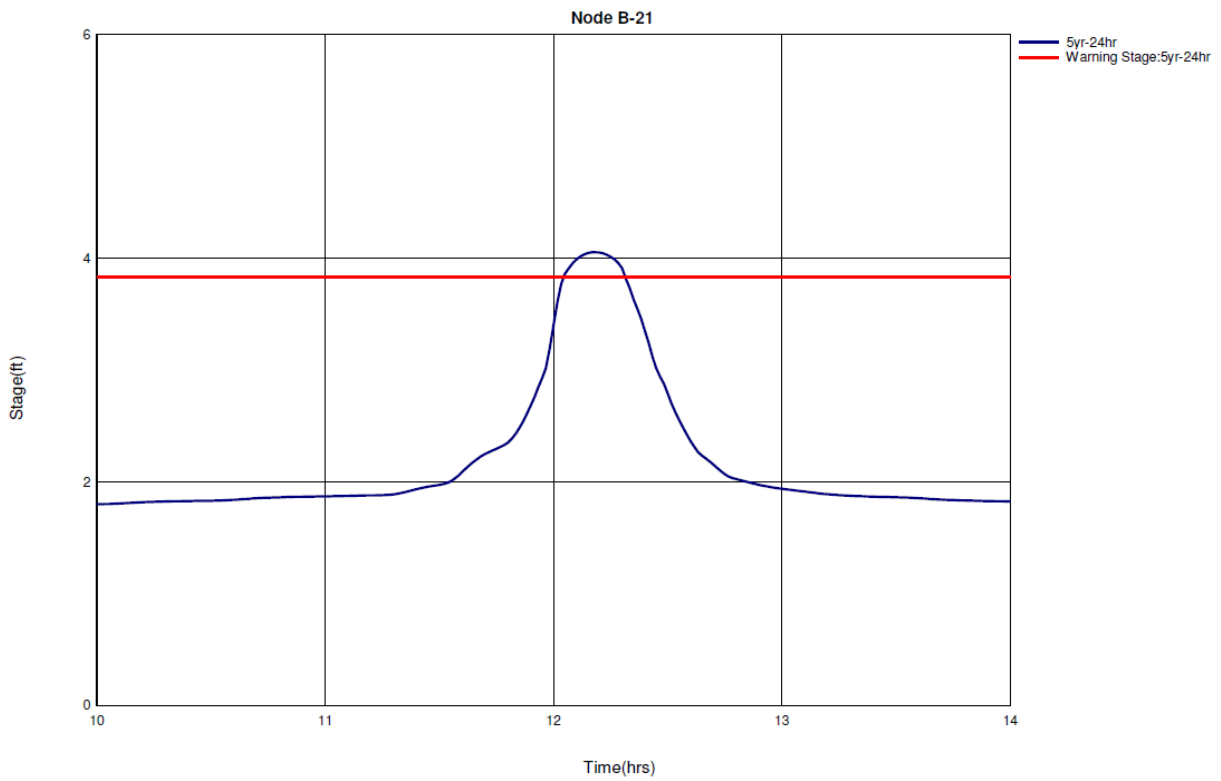
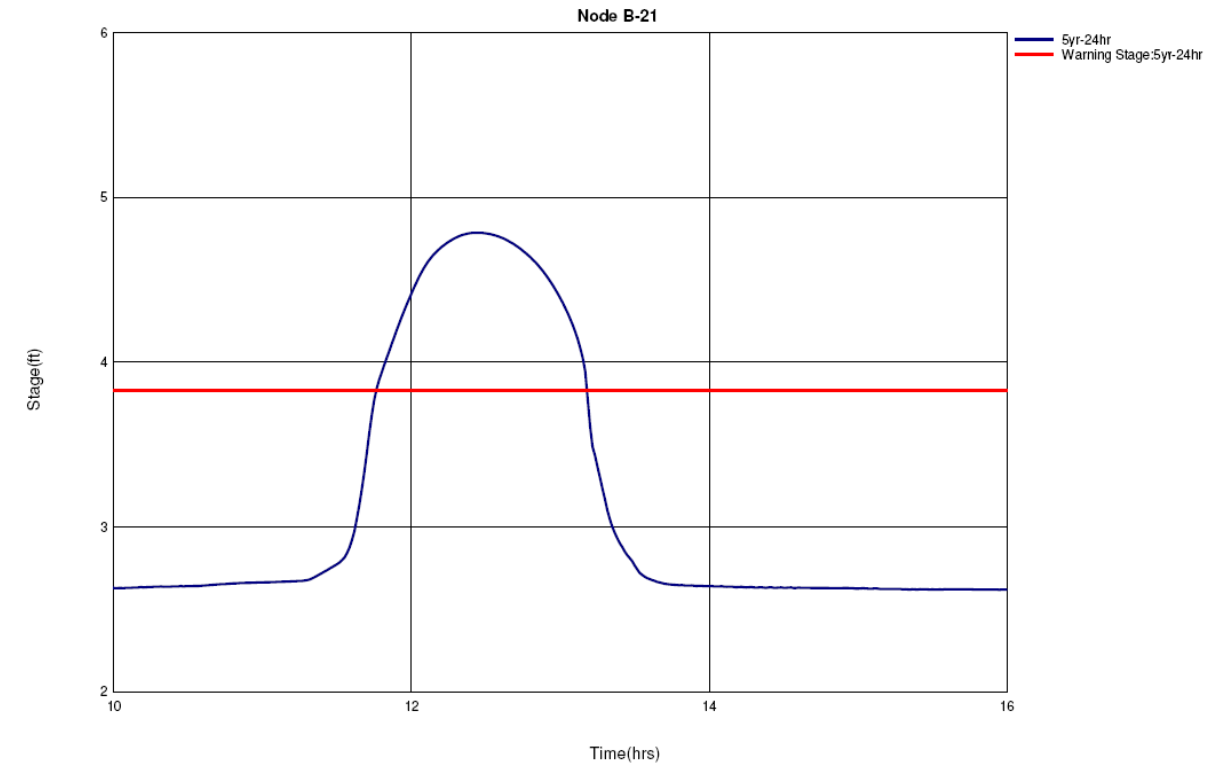


FIGURE 10: POST-DEVELOPMENT NODE-LINK DIAGRAM- FINAL DESIGN



**FIGURE 11 TIME VS. STAGE OF B-21 - PRE VS. POST**



## 6.4 OTHER DESIGN CONSIDERATIONS

An option that may be explored, if the budget permits, is “Cured in Place Pipe” (CIPP) liner for restoration of the existing box culverts. The existing lines, although hydraulically adequate, are extremely old (circa 1950’s) and CIPP could be used in lieu of full replacement. This procedure is very effective, preserves the integrity of the pipes, and does not require any impacts to the roadways for installation. In addition they will provide a water tight seal that is critical for the operation of a pump station where leaks can result in an overused and costly system.

The final design consideration should be the reconstruction of the existing outfall structure. As part of the scope of this project, the outfall reconstruction was removed due to funding shortfalls. However, this outfall is in an extreme state of disrepair. Upon recent inspections, the sand-cement rip rap bags that were installed a few years ago to reinforce the structure have collapsed (see figure 12). The County is currently underway on a project to address the outfall structure.



FIGURE 12 CURRENT STATE OF SW 1<sup>ST</sup> COURT OUTFALL

## 6.5 WATER QUALITY

In this project, due to the unavailability of space, a structural BMP or water quality structure is the preferred method of achieving the water quality criteria. The method for modeling this type of system begins with determining the volume of runoff requiring treatment. This is achieved through a method developed by Miami Dade DERM of calculating the time to generate 1” of runoff and subsequently calculating a runoff flow generated by the 1” runoff volume. This flow is the basis used to size the water quality structure.

In this project we have chosen Hydro International’s Downstream Defender as the basis for design due to their presence in the area as well as the availability of information. Other approved equal water quality structures may be substituted. The structure was sized based on the manufacture’s sizing criteria and the calculated flows. A weir was then sized to divert the 1” runoff flow to the water quality structure. The weir height was derived by calculating the head

losses through water quality system, taking into account the losses through the inflow and outflow pipes, as well the losses through the structure as provided in the manufacturer's literature (See Water Quality Calculations in Appendix D).

In addition to the water quality structure, baffles and a large screen can be incorporated in the pump station wet well to capture heavy debris, oil, and floatable that may bypass said structure.

As part of the proposed alternative the basins B-27, B-28, B-16, and B-17 will be effectively removed from the pump station's contributing area through the use of isolated exfiltration trenches with overflow weir control structures. Consequently, it will be required to size an appropriate exfiltration trench system for these basins. The current geotechnical exploration scope did not include percolation tests. A moderate hydraulic conductivity ("K") value was used;  $5 \times 10^{-4}$ . For the design phase two percolation tests are recommended in each area in order to determine an accurate hydraulic conductivity value (See Water Quality Calculations in Appendix D).

## SECTION 7 ROADWAY IMPROVEMENTS

As part of this project the City right-of-way along 9<sup>th</sup>, 10<sup>th</sup>, 11<sup>th</sup>, and 12<sup>th</sup> Street between SW 1<sup>st</sup> Avenue and SE 1<sup>st</sup> Avenue will be restored and improved. Improvements will include milling and resurfacing, installation of new curb and gutter where required, repair of damaged existing curbs and gutters, base restoration where required, sidewalk repairs, elimination of sod utility strips (request of public works and DDA), and the installation of new larger capacity curb inlets and catch basins. No improvements will be made to the South Miami Avenue right-of-way due to the ongoing drainage project between 10<sup>th</sup> and 13<sup>th</sup> Street and the future South Miami Avenue Streetscape project being designed for the DDA.

The following is an outline of the proposed right-of-way improvements for each street:

### SW/SE 9<sup>th</sup> Street:

- In general the roadway is in good condition and will be milled and resurfaced.
- A new curb and gutter will be construction along the north side of the existing roadway from approximately 300' east of SW 1<sup>st</sup> Avenue to South Miami Avenue. The new curb and gutter will slightly narrow the existing street and better define the northern edge of pavement which currently has no curb and meanders along the length of the road.
- As a result of the new curb and gutter, the existing sidewalk along the north side may require reconstruction in some sections to accommodate the higher grade elevations.
- From approximately 200' to 300' east of SW 1<sup>st</sup> Avenue the northern parking lane will have to be reconstructed to correct the existing cross slope which drastically exceeds 2%.
- The north side of 9<sup>th</sup> Street between South Miami Avenue and SE 1<sup>st</sup> Avenue will require repairs to the existing curb and gutter as well as sidewalk repairs and elimination of the utility strip.
- The south side of 9<sup>th</sup> Street is a new development with curb, gutters, and sidewalks in good condition. Only minor repairs to cracks and spalls will be proposed.
- The entire roadway will be restriped with two westbound lanes and parking lanes north and south. The roadway will remain one-way.

**SW/SE 10<sup>th</sup> Street:**

- In general the roadway is in good condition and will be milled and resurfaced.
- Most of the 10<sup>th</sup> Street right-of-way is new development with curb, gutters, and sidewalks in good condition. Only minor repairs to cracks and spalls will be proposed. There are several areas near South Miami Avenue on the south side where there is extensive curb and gutter damage, this will be repaired.
- The entire roadway will be restriped for two-way traffic and parking stalls on the north side west of South Miami Avenue, and on the south side east of South Miami Avenue (existing).
- Some of the older areas on the eastern and western ends of the street will have the existing sod utility strips eliminated.

**SW/SE 11<sup>th</sup> Street:**

- In general the roadway is in good condition. The recent development restored the pavement up to approximately 300' east of SW 1<sup>st</sup> Avenue. The remainder of the roadway from that point until SE 1<sup>st</sup> Avenue (excluding South Miami Avenue) will be milled and resurfaced.
- The western end (up to approximately 300' east of SW 1<sup>st</sup> Avenue) of the 11<sup>th</sup> Street right-of-way is mostly new development with curb, gutters, and sidewalks in good condition. Only minor repairs to cracks and spalls will be proposed and repair to some of the older curb and gutter on the northwest end.
- The entire area west of South Miami Avenue up to the recently restored area has extensive curb and gutter damage, this will be repaired. There are 6 curbed islands along the south side of the right-of-way adjacent to the MDT columns that are extensively damaged, these will be repaired.
- The entire roadway will be restriped for two lane one-way westbound traffic and parking stalls on the south side (existing).
- Most of the right-of-way is older development and will have the existing sod utility strips eliminated.

**SW 12<sup>th</sup> Street:**

- There is new hotel development being constructed mid-block along SW 12<sup>th</sup> Street. From recent site visits, it seems the developer is constructing major improvements within the right-of-way. No improvements to the 12<sup>th</sup> Street right-of-way are being proposed at this time pending a review of the new development permitted construction plans.

## SECTION 8 CONCLUSIONS

The proposed improvements will include a new pump station along SW 1<sup>st</sup> Court between SW 8<sup>th</sup> Street and SW 9<sup>th</sup> Street. In addition, improvements will be made to the existing drainage conveyance system. The secondary trunk line along SW/SE 9<sup>th</sup> Street will be improved by increasing the size of several pipe runs, and the branch line along SW 10<sup>th</sup> Street and 11<sup>th</sup> Street will also be upsized. Other improvements will include the replacement of sub-standard curb inlets, all cross drains will be improved to an 18" minimum diameter, and the higher elevation basins at SW 12<sup>th</sup> Street and SE 11<sup>th</sup> Street will be converted to isolated exfiltration trench systems to minimize the area of the pump station basin. Finally the implementation of a water quality BMP structure and 2 injection wells will be required to meet permitting requirements.

**APPENDIX A – REPORT BACK-UP DOCUMENTATION**

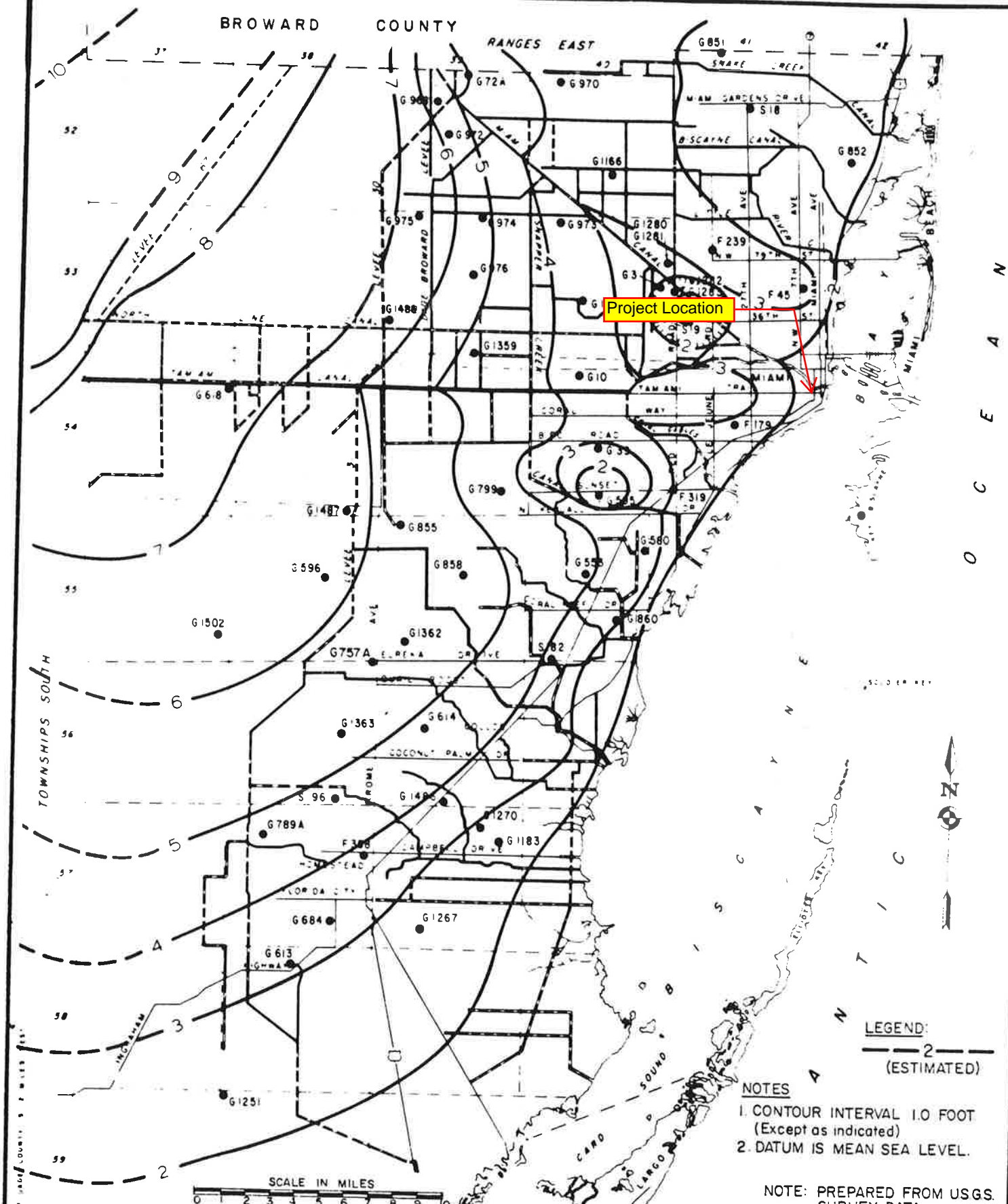
- MIAMI DADE COUNTY GROUND WATER LEVEL MAP WC 2.1 AND WC 2.2
  - SFWMD RAINFALL MAPS
  - CITY OF MIAMI DRAINAGE RECORD DRAWINGS





BROWARD COUNTY

RANGES EAST



Project Location

LEGEND:  
 2  
 (ESTIMATED)

NOTES  
 1. CONTOUR INTERVAL 1.0 FOOT  
 (Except as indicated)  
 2. DATUM IS MEAN SEA LEVEL.

NOTE: PREPARED FROM USGS SURVEY DATA

METROPOLITAN  
 DADE COUNTY  
 PUBLIC WORKS  
 DEPARTMENT

APPROVED	REVISED
4/5/72	2/19/75
	4/14/77

DESIGN STANDARDS  
 AVERAGE OCTOBER  
 GROUND WATER LEVEL  
 1960-75

W.C.  
 2.2  
 SHEET 1 OF 1

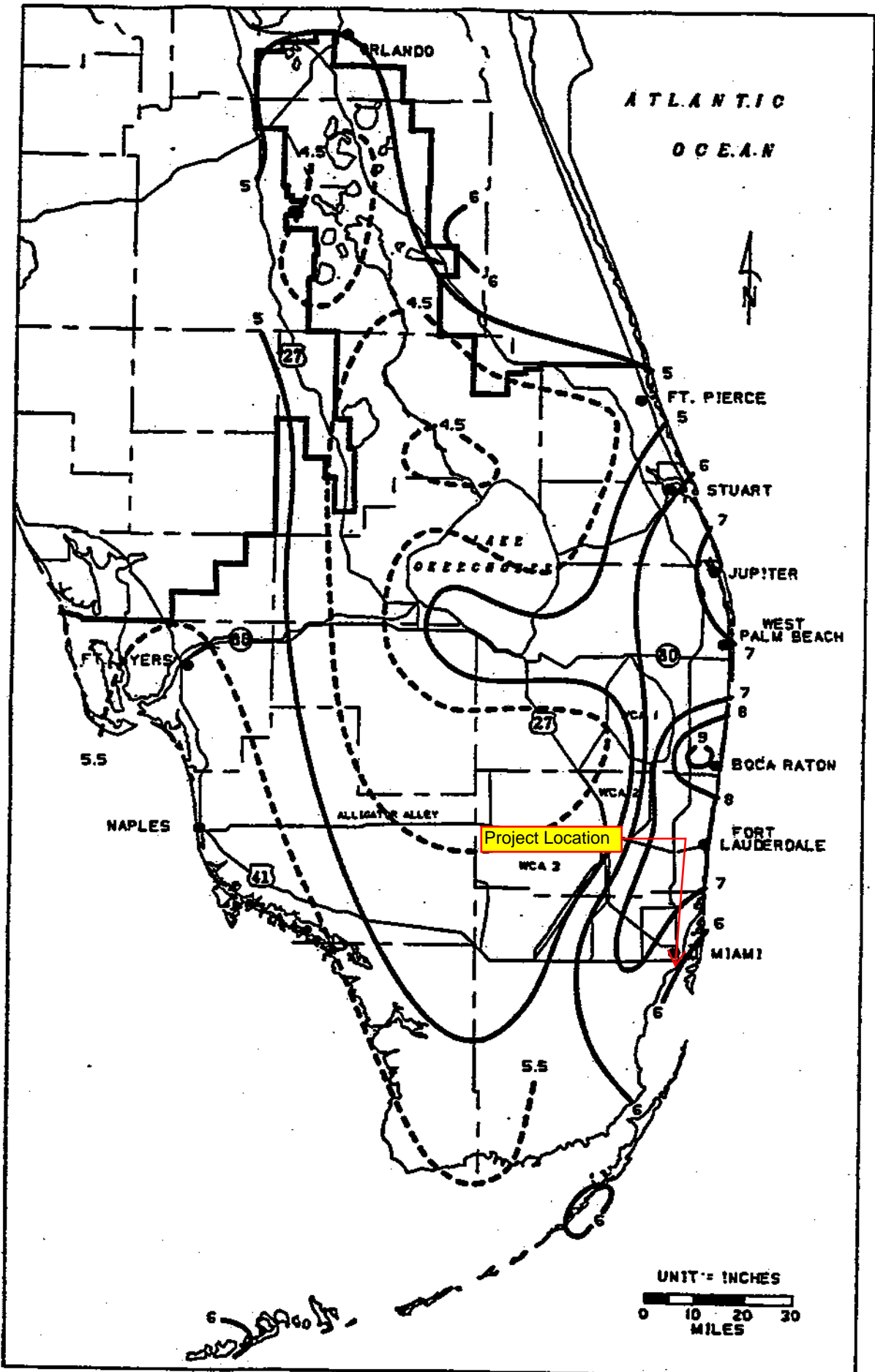


FIGURE C-3. 1-DAY RAINFALL: 5-YEAR RETURN PERIOD



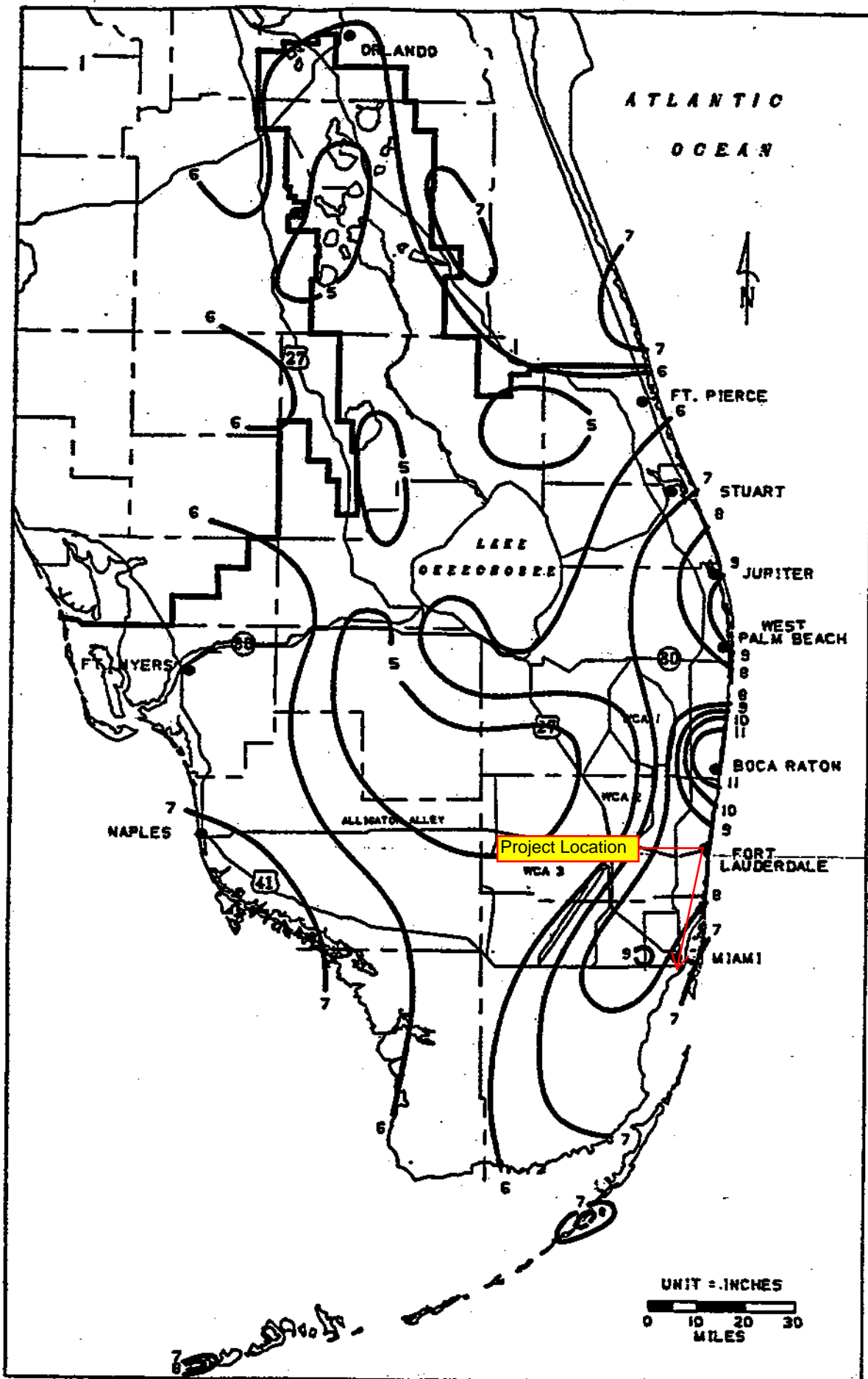


FIGURE C-4. 1-DAY RAINFALL: 10-YEAR RETURN PERIOD



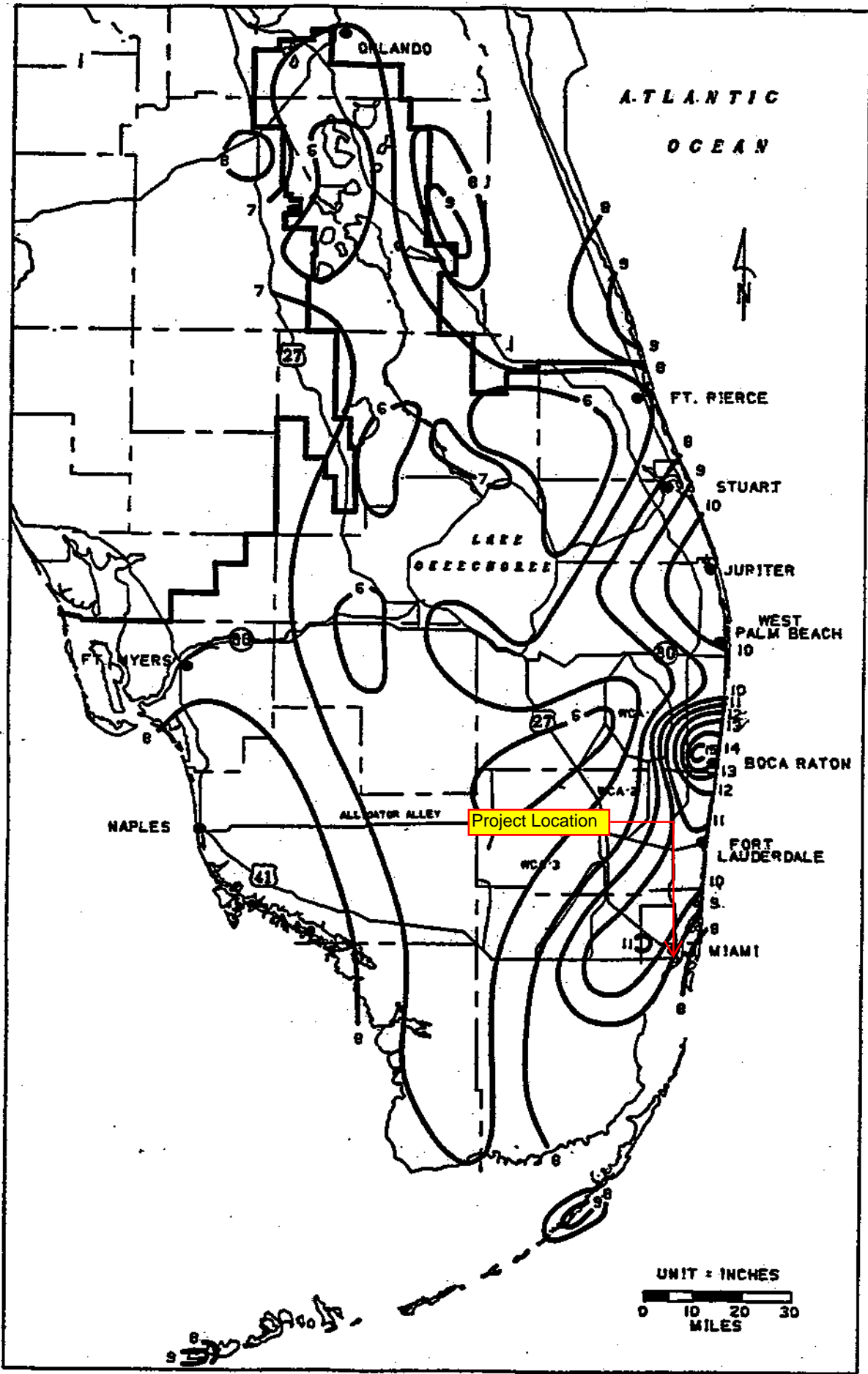


FIGURE C-5. 1-DAY RAINFALL: 25-YEAR RETURN PERIOD

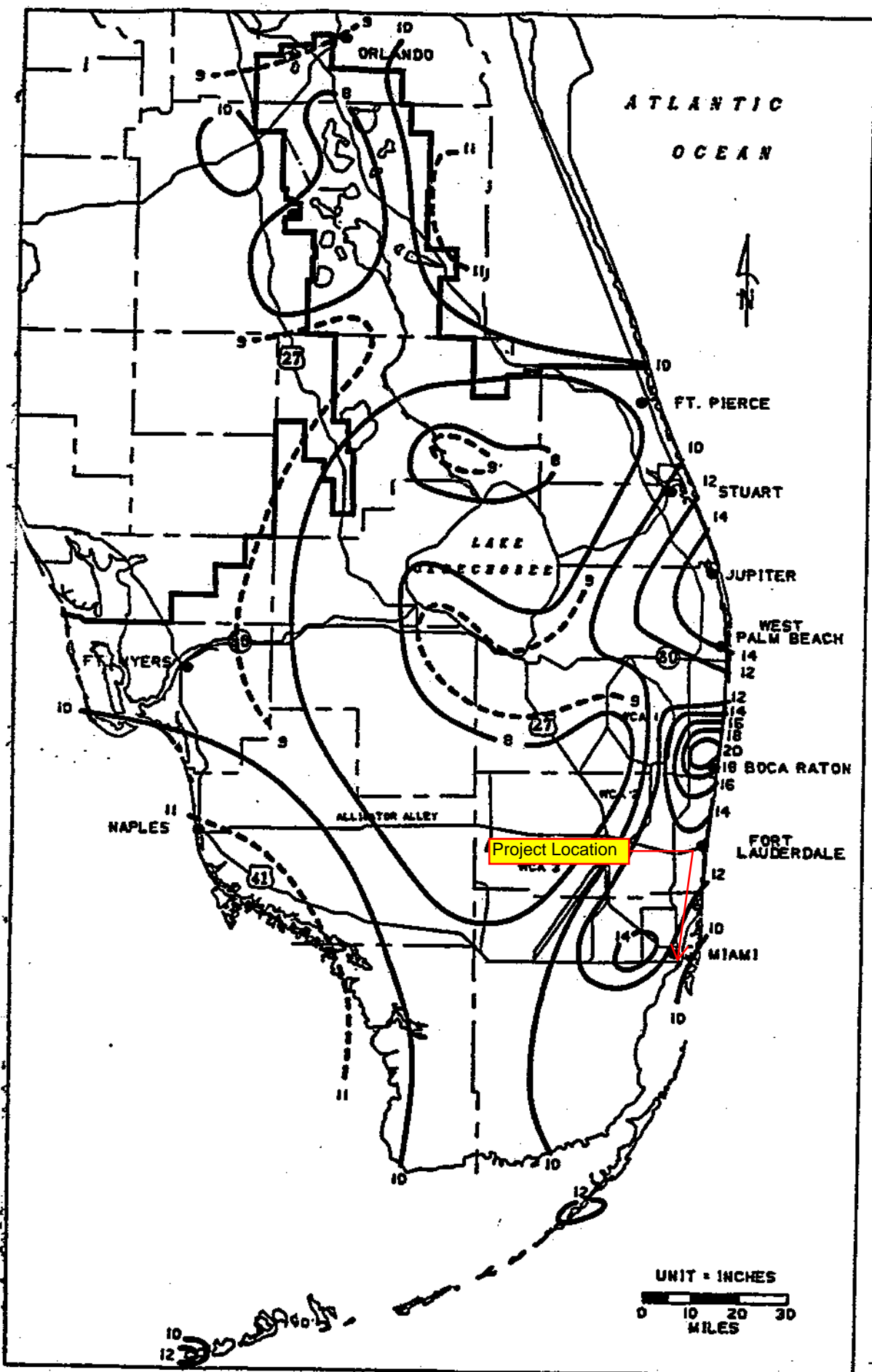


FIGURE C-6. 1-DAY RAINFALL: 100-YEAR RETURN PERIOD

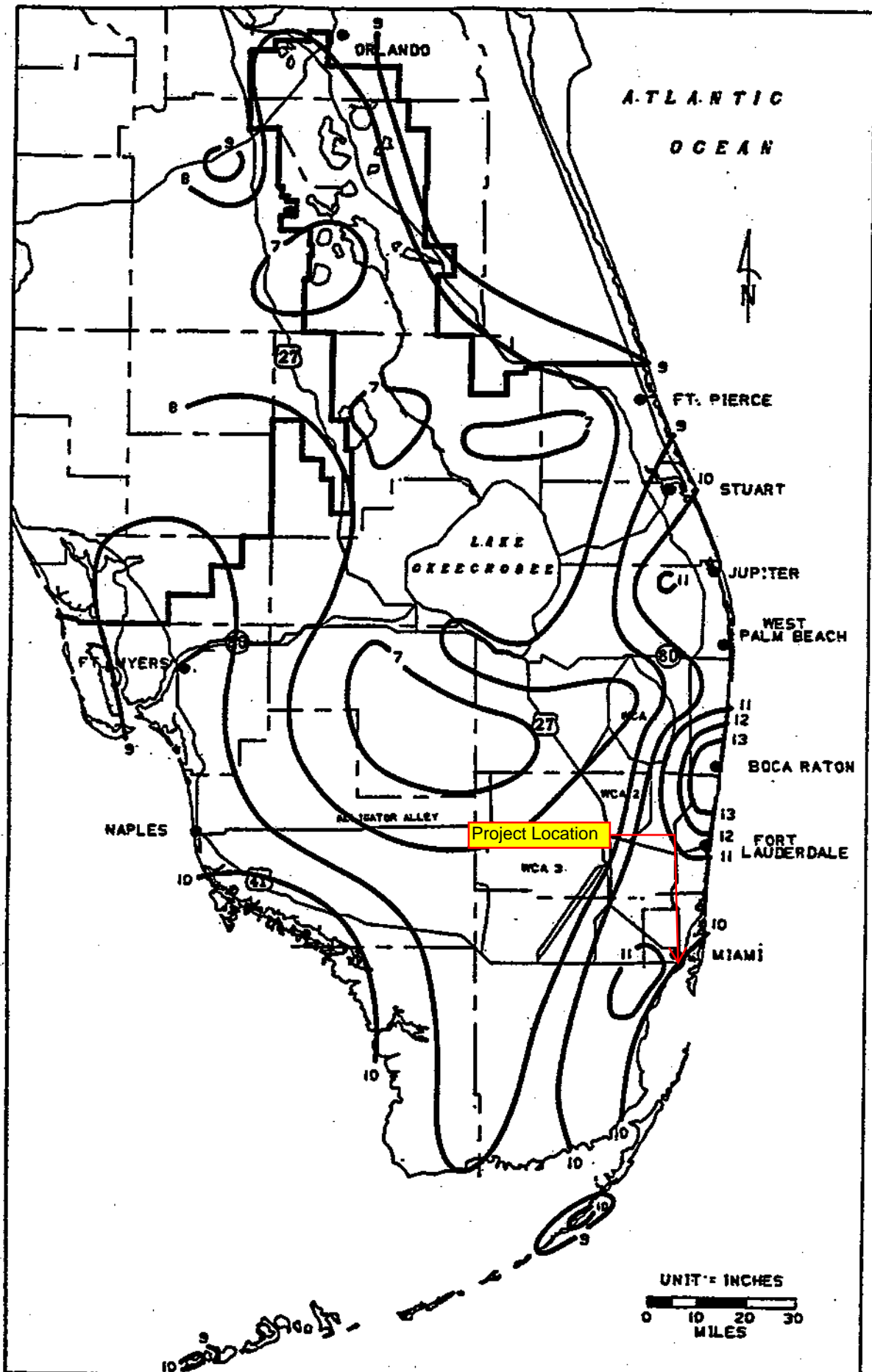


FIGURE C-7. 3-DAY RAINFALL: 10-YEAR RETURN PERIOD

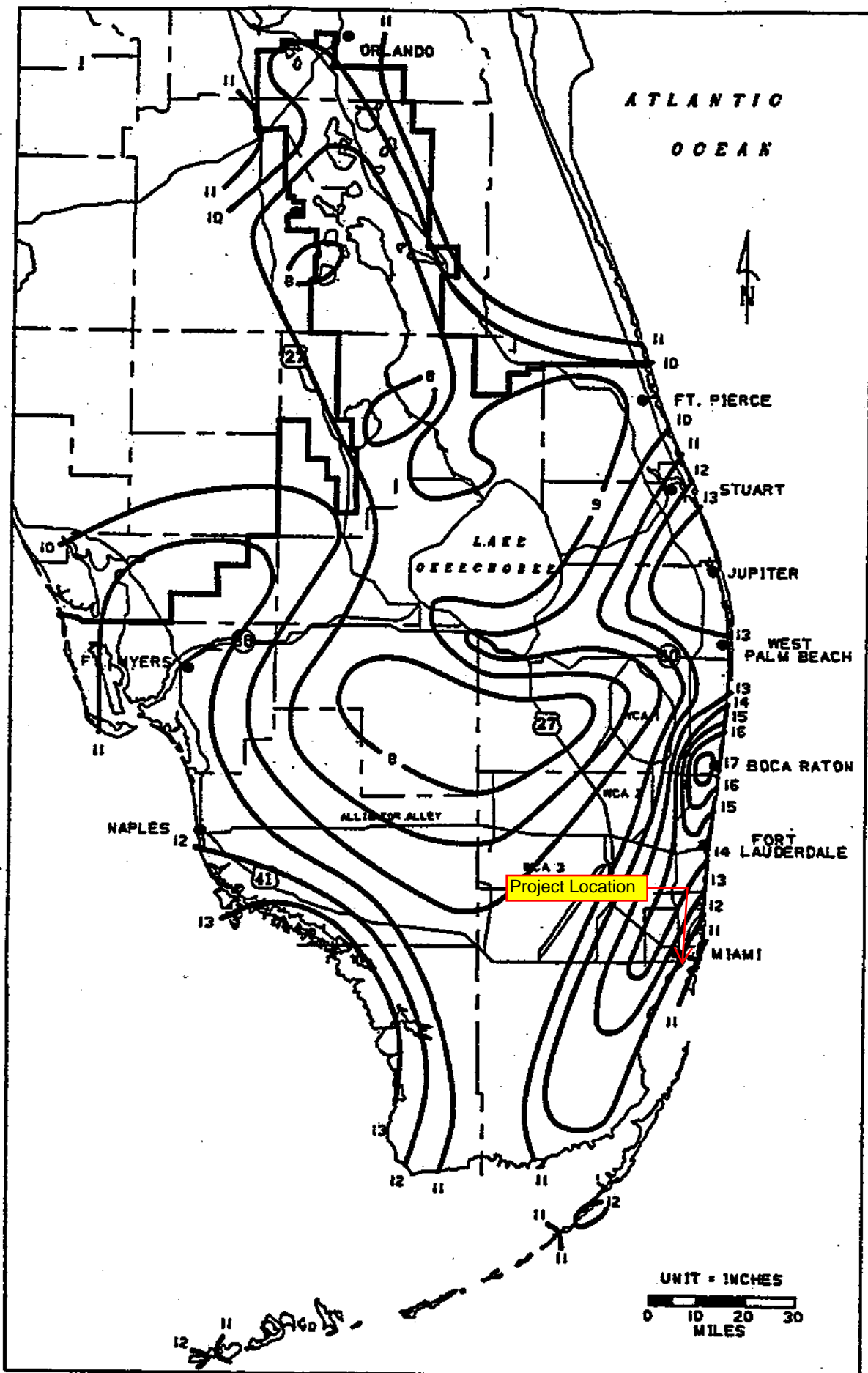


FIGURE C-8. 3-DAY RAINFALL: 25-YEAR RETURN PERIOD



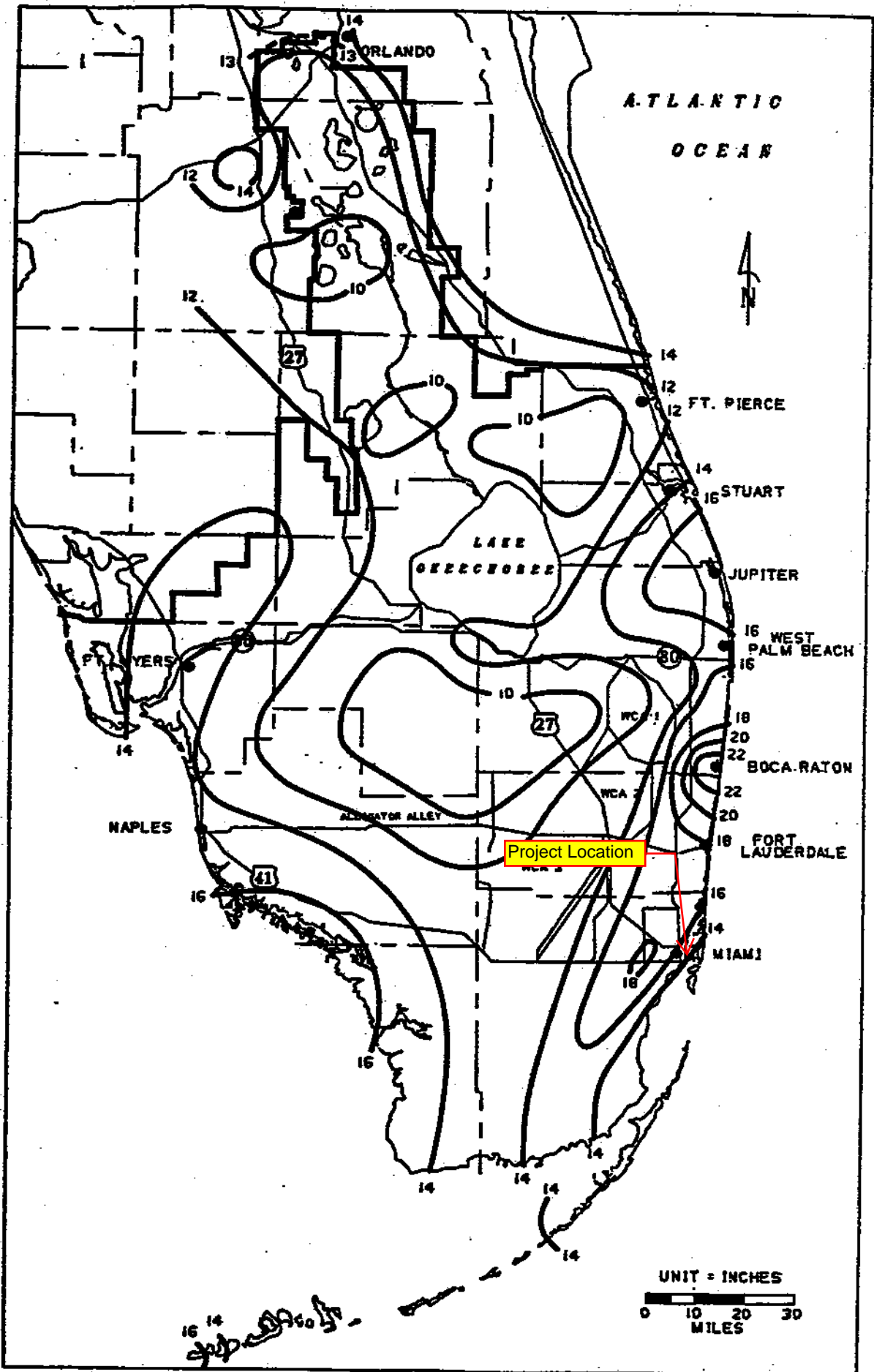
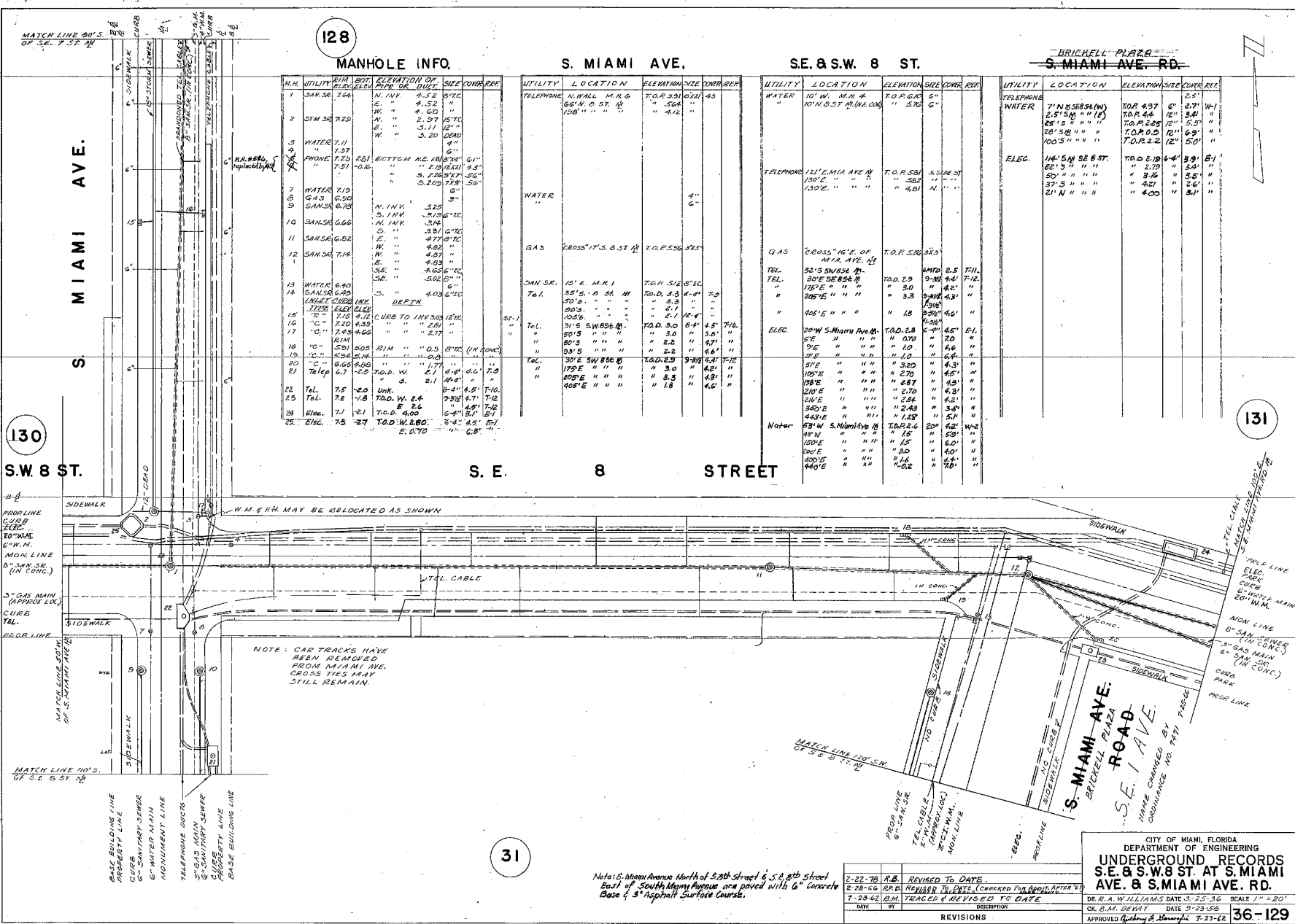


FIGURE C-9. 3-DAY RAINFALL: 100-YEAR RETURN PERIOD

- REFERENCES**  
 LAYOUT  
 T.O.P. 121 488  
 NOPIKINS  
 R/W SECTION  
 T.M. MAPS 3-1-36  
 AERIAL PHOTO  
 MISC. PLAT. B-27  
 SURVEY R.A. 1266-51
- SEWER**  
 SANITARY SEWER  
 U.G. BK. 53-42, 43  
 " " 13-57  
 " " 14-15  
 " " 120-34  
 " " 80-48, 49, 50  
 MISC. SR. 3-12  
 SAN. SR. MAP  
 CANTER BOOKS  
 COMPREHENSIVE
- STORM SEWER**  
 U.G. BK. 120-34  
 " " 80-48, 49  
 " " 50-51  
 STORM SR. MAP  
 COMPREHENSIVE
- TELEPHONE**  
 U.G. BK. 120-34  
 " " 80-48, 49  
 " " 50-51  
 " " 129-26  
 " " 170-60  
 " " 244-25  
 " " 243-28  
 " " 274-35  
 T.O.P. 121 488  
 D.I.L. P.C. 5-16-75  
 T.I.R. P.C. 3-28-18
- ELECTRIC**  
 E-11 P.C. 3-15-68  
 3" GAS MAIN (APPROX. LOC.)  
 6" WATER MAIN (IN CONC.)
- GAS**  
 3" GAS MAIN (APPROX. LOC.)  
 CURB TEL.
- WATER**  
 U.G. BK. 120-34  
 " " 215-47  
 " " 80-48, 49, 50, 51  
 OLD WATER BOOK  
 COMPREHENSIVE  
 W-1-E-8985  
 W-2-E-8530
- BASE BUILDING LINE**  
 PROPERTY LINE  
 3" GAS MAIN  
 6" SANITARY SEWER  
 6" WATER MAIN  
 MONUMENT LINE  
 TELEPHONE DUCT  
 3" GAS MAIN  
 6" SANITARY SEWER  
 6" WATER MAIN  
 PROPERTY LINE  
 BASE BUILDING LINE



MANHOLE INFO.				S. MIAMI AVE.				S.E. & S.W. 8 ST.				BRICKELL PLAZA S. MIAMI AVE. RD.						
M.H.	UTILITY	RIM BOT. ELEV.	ELEVATION OF CURB OR DUCT	SIZE	CORR.	REF.	UTILITY	LOCATION	ELEVATION	SIZE	CORR.	REF.	UTILITY	LOCATION	ELEVATION	SIZE	CORR.	REF.
1	SAN. SW	7.64	M. INV. 4.52	8" TC			TELEPHONE	N. WALL M.H. 6 80' W. S. ST. 12	T.O.P. 3.91	8" TC	23		WATER	10' W. M.H. 4 10' W. S.T. M.H. 606	T.O.P. 6.0	6"		
2	STW. SW	7.23	M. " 4.60	15" TC			"	"	" 3.94	"			"	"	" 5.76	6"		
3	WATER	7.11	M. " 2.97	15" TC			"	"	" 3.71	"			"	"	" 12" 6.9"	"		
4	PHONE	7.23	BOTTOM M.L. 1814.93	6"			"	"	" 3.20	"			"	"	" 12" 6.9"	"		
5	PHONE	7.51	" 2.19	6"			"	"	" 3.26	"			"	"	" 12" 6.9"	"		
6	PHONE	7.51	" 3.20	6"			"	"	" 3.20	"			"	"	" 12" 6.9"	"		
7	WATER	7.19	M. INV. 3.25	8" TC			WATER	"	" 2.97	4"			"	"	" 4.61	N.		
8	G.A.S.	6.95	S. INV. 3.19	6" TC			"	"	" 2.97	6"			"	"	" 4.61	N.		
9	G.A.S.	6.95	S. INV. 3.19	6" TC			"	"	" 2.97	6"			"	"	" 4.61	N.		
10	SAN. SW	6.66	M. INV. 3.94	8" TC			"	"	" 2.97	6"			"	"	" 4.61	N.		
11	SAN. SW	6.62	M. " 4.77	8" TC			"	"	" 2.97	6"			"	"	" 4.61	N.		
12	SAN. SW	7.14	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
13	WATER	6.40	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
14	SAN. SW	6.69	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
15	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
16	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
17	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
18	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
19	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
20	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
21	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
22	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
23	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
24	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		
25	"	"	M. " 4.82	"			"	"	" 2.97	6"			"	"	" 4.61	N.		

CITY OF MIAMI, FLORIDA  
 DEPARTMENT OF ENGINEERING  
**UNDERGROUND RECORDS**  
**S.E. & S.W. 8 ST. AT S. MIAMI**  
**AVE. & S. MIAMI AVE. RD.**  
 DR. R. A. WILLIAMS DATE 3-22-56 SCALE 1" = 20'  
 DR. R. M. DEWITT DATE 5-23-58  
 APPROVED *[Signature]* 7-23-62

NO.	BY	REVISIONS
1	R.B.	REVISED TO DATE.
2	R.B.	REVISED TO DATE. (CHECKED 1/3 REVISION AFTER 7/28-62)
3	B.M.	TRACED & REVISED TO DATE.

Note: S. Miami Avenue North of S.W. 8 Street & S.E. 8 Street  
 East of South Miami Avenue and paved with 6" Concrete  
 Base & 3" Asphalt Surface Course.

130  
 S.W. 8 ST.

131

31

**REFERENCES**

- LAYOUT**
- 31 OLD MANILA 36-130
  - 32 HOPKINS VOL. 1 76-12
  - 33 TAX MAPS 35(96)
  - 34 AERIAL PHOTOS 77(19)
  - 35 LG BOOK 48-10
  - 36 SURVEY BK. 557-34
  - 37 PAVING BK. 461-73
  - 38 " " 557-106
  - 39 SURVEY BK. 675-27
  - 40 " " 525-39
  - 41 " " 949-26-36
  - 42 " " 476-4,5
  - 43 SEWER ISS. CARDS
- MISCELLANEOUS**
- RIGHT OF WAY DEPT

- WATER**
- 41 OLD MANILA 36-130
  - 42 WATER SH. 219-1
  - 43 LG BOOK 12-28
  - 44 OLD MIAMI WATER 205
  - 45 SAN SR. COUNTER BOOK 38(1-18) (3)
  - 46 LG BOOK 124-22,25
  - 47 LG INSPECTION CARDS 233
  - 48 LG BOOK 262-54

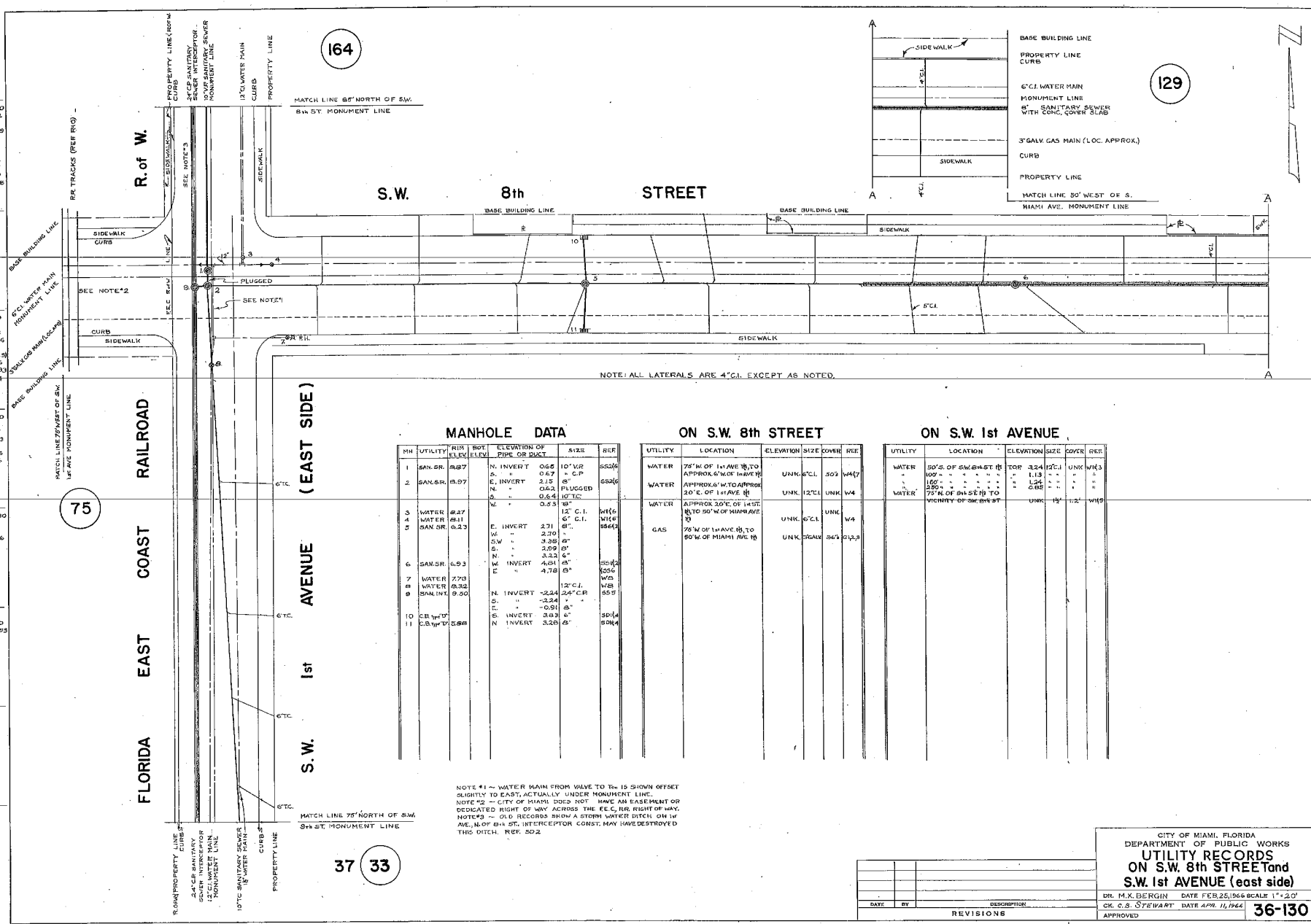
- SANITARY SEWER**
- 51 OLD MANILA 36-130
  - 52 COUNTER BKS. 158-39
  - 53 SEWER BK. 53(2,43)
  - 55 INTERCEPTOR AS QUALITY SH. 86
  - 56 LG BOOK 124-22,26

- STORM SEWER**
- 501 OLD MANILA 36-130
  - 502 LG BOOK 14-75
  - 503 STORM SR. CORR
  - 504 LG BOOK 124-22,26

- GAS**
- 91 CAD ATLAS 51(41)
  - 92 OLD MANILA 36-130
  - 93 LG INSPECTION CARDS 295

- ELECTRIC**

- TELEPHONE**



164

129

75

37 33

**MANHOLE DATA**

NO.	UTILITY	RIM ELEV.	SOFT ELEV.	ELEVATION OF PIPE OR DUCT	SIZE	REF.
1	SAN. SR.	8.97		N. INVERT 0.66 S. " 0.67	10" I/C 6" CP	55(3)
2	SAN. SR.	8.97		E. INVERT 2.15 N. " 0.62 S. " 0.64	6" I/C PLUGGED 10" I/C	55(3)
3	WATER	8.27		W. " 0.53	12" C.I.	51(6)
4	WATER	8.11		W. " 2.09	6" C.I.	51(6)
5	SAN. SR.	8.23		E. INVERT 2.71 W. " 3.38 S. " 3.09 N. " 3.32	8" I/C 6" C.I. 6" C.I. 6" C.I.	55(6)
6	SAN. SR.	6.93		E. INVERT 4.81 S. " 4.76	8" I/C 6" C.I.	55(2)
7	WATER	7.79			12" C.I.	55(6)
8	WATER	8.32			12" C.I.	55(6)
9	SAN. INT.	9.50		S. " -2.24 E. " -0.91	24" CP 8" S.	55(5)
10	C.B. 1/2" I/C			N. INVERT 5.83	8" S.	50(4)
11	C.B. 1/2" I/C			N. INVERT 3.26	8" S.	50(4)

**ON S.W. 8th STREET**

UTILITY	LOCATION	ELEVATION	SIZE	COVER	REF.
WATER	75' N. OF 1st AVE. TO APPROX. 6' W. OF INTERCEPTOR	UNK.	6" C.I.	30" W47	
WATER	APPROX. 6' W. TO APPROX. 20' E. OF 1st AVE. TO	UNK.	12" C.I.	UNK. W4	
WATER	APPROX. 20' E. OF 1st AVE. TO 50' W. OF 1st AVE. TO	UNK.	6" C.I.	UNK. W4	
GAS	75' N. OF 1st AVE. TO 50' W. OF MIAMI AVE. TO	UNK.	3" GALV.	30" S13.5	

**ON S.W. 1st AVENUE**

UTILITY	LOCATION	ELEVATION	SIZE	COVER	REF.
WATER	50' S. OF SW. 8th ST. TO 100' S. OF SW. 8th ST.	TOP 3.24 " 1.13	12" C.I.	UNK. W43	
WATER	100' S. OF SW. 8th ST. TO 150' S. OF SW. 8th ST.	" 1.24 " 0.68	" "	" "	
WATER	150' S. OF SW. 8th ST. TO VICINITY OF SW. 8th ST.	UNK.	12" C.I.	UNK. W43	

NOTE #1 - WATER MAIN FROM VALVE TO TR-15 SHOWN OFFSET SLIGHTLY TO EAST, ACTUALLY UNDER MONUMENT LINE.  
 NOTE #2 - CITY OF MIAMI DOES NOT HAVE AN EASEMENT OR DEDICATED RIGHT OF WAY ACROSS THE E.C.C. RR. RIGHT OF WAY.  
 NOTE #3 - OLD RECORDS SHOW A STORM WATER DITCH ON W. AVE. N. OF SW. 1st ST. INTERCEPTOR CONST. MAN HAS DESTROYED THIS DITCH. REF. 502

CITY OF MIAMI, FLORIDA  
 DEPARTMENT OF PUBLIC WORKS  
**UTILITY RECORDS**  
**ON S.W. 8th STREET and**  
**S.W. 1st AVENUE (east side)**

DR. M.X. BERGIN DATE FEB. 25, 1966 SCALE 1" = 20'  
 CK. C.B. STEWART DATE APR. 11, 1966

APPROVED **36-130**

DATE	BY	DESCRIPTION







ON SW 17th Ave. (W)

Utility	Location	Elevation	Size	Code
Electric	80' S of SW 8 St. N	T.O.D. 1.1'	66KV	55'
	17' N of SW 8 St.	1.8'		7.1'
	30' N of SW 8 St. N	2.5'		5.7'
	100'	2.6'		4.0'
	130'	2.4'		4.0'
	200'	2.9'		3.5'
	250'	2.1'		3.7'
	300'	2.8'		3.5'
Electric	201' N of SW 8 St. N	0.37' B.M.T.D.		4.9'
Storm Sr.	Along SW 1 Ave.		60" x 36"	4.1'

MM	Utility	Rm Elev.	Prop Elev.	Elevation of Pipe or Duct	Size	Code
1	Electric	3.2'	4.35'			
2	Electric					
3	San.Sr.	5.0'		W. Inv. 1.61'	12"	
				S. Inv. 1.70'	10"	
				N. Inv. 1.89'	8"	
				E. Inv.	8"	

ON SW 8th St.

Utility	Location	Elevation	Size	Code
Electric	14.1' W of SW 1 Ave. N	T.O.D. 7.41'	2-2"	
"	110.8' " " " " "	" 8.63 "	"	

**REFERENCES**

**ELECTRIC**

- UG. BK. 231-34
- MIAMI-DC. ORANGE PLANS
- UG. 111-32
- Permit # - 12-20-51

**San Sewer**

- SR. BK. F3-44
- COUNTER BK. SWP SW-8-1

**STORM SR.**

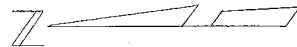
- SR. BK. 260-25

**SIDEWALK**

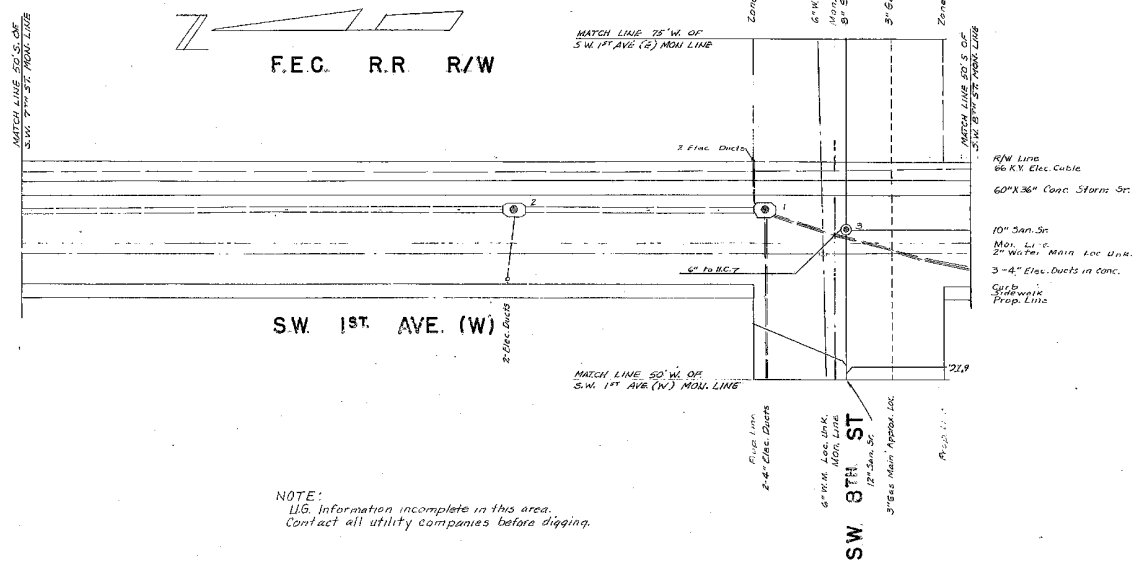
- SUR. BK. 897-93
- PAN. BK. 878-29

74

37-111



F.E.C. R.R. R/W



**NOTE:**  
 U.G. information incomplete in this area.  
 Contact all utility companies before digging.

130

157

CITY OF MIAMI, FLORIDA  
 DEPARTMENT OF ENGINEERING

**UNDERGROUND RECORDS**

DR. J. J. ... DATE 8-26-60 SCALE 1" = 20'  
 CK. F. E. ... DATE 8-25-60

APPROVED 36-75

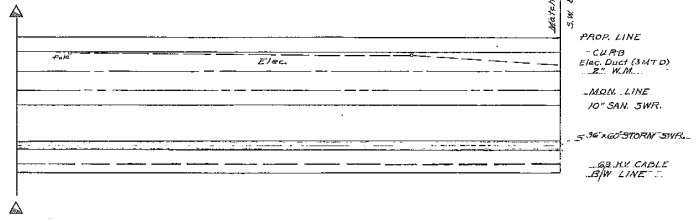
7-17-67 D.F. Allied interests

Dim	Dist	Elevation of	Utility	Location	Elevation	Size/Cover	
1	San	W Inv	2.26	8"	30"	Water	2" 15'
2	Storm	N Inv	0.85	3" x 5"		Elec.	At 10 St. Main Line TOP 116 08X4.5'
3		W Inv	7.53	18"			150' N of 10th St. = 0.82 4' 8.5'
4		S Inv	2.54				At 9 St. N. (Elev) = 20' 8" 11' 16.1'
5	Storm	TOV	0.64	42" x 30"	50"		250' N of 9 St. N. = 1.65 4'
6	Water			2"			
7	San	NSW Inv	1.88	8"		Elec.	2" 24'
8	San	S Inv	1.20	8"			
9	San	E Inv	0.21	8"		Water	At 10 St. = 1.08 188 6"
10	San	W Inv	1.70	8"		Gas	End of Main TOP 120 6"
A	Type F	NE Inv	2.01	18"			
B	Type F	SE Inv	1.85	18"			
C	Type D	NE Inv	1.61	18"			
D	Type D	SE Inv	1.43	18"			
E	Type F	W Inv	0.34	3" x 5"			
F	Type F	S Inv	0.33	3" x 5"			
G	Type D	N Inv	1.44	12"			
H	Water	S.W. Inv	2.25	12"			
I	Water	T.O.V.	2.79	6"	552"		

ON S.W. 1st AVE.						
Utility	Location	Elevation	Size/Cover			
Water			2" 15'			
Elec.	At 10 St. Main Line	TOP 116 08X4.5'				
	150' N of 10th St.		0.82 4' 8.5'			
	At 9 St. N. (Elev)		20' 8" 11' 16.1'			
	250' N of 9 St. N.		1.65 4'			

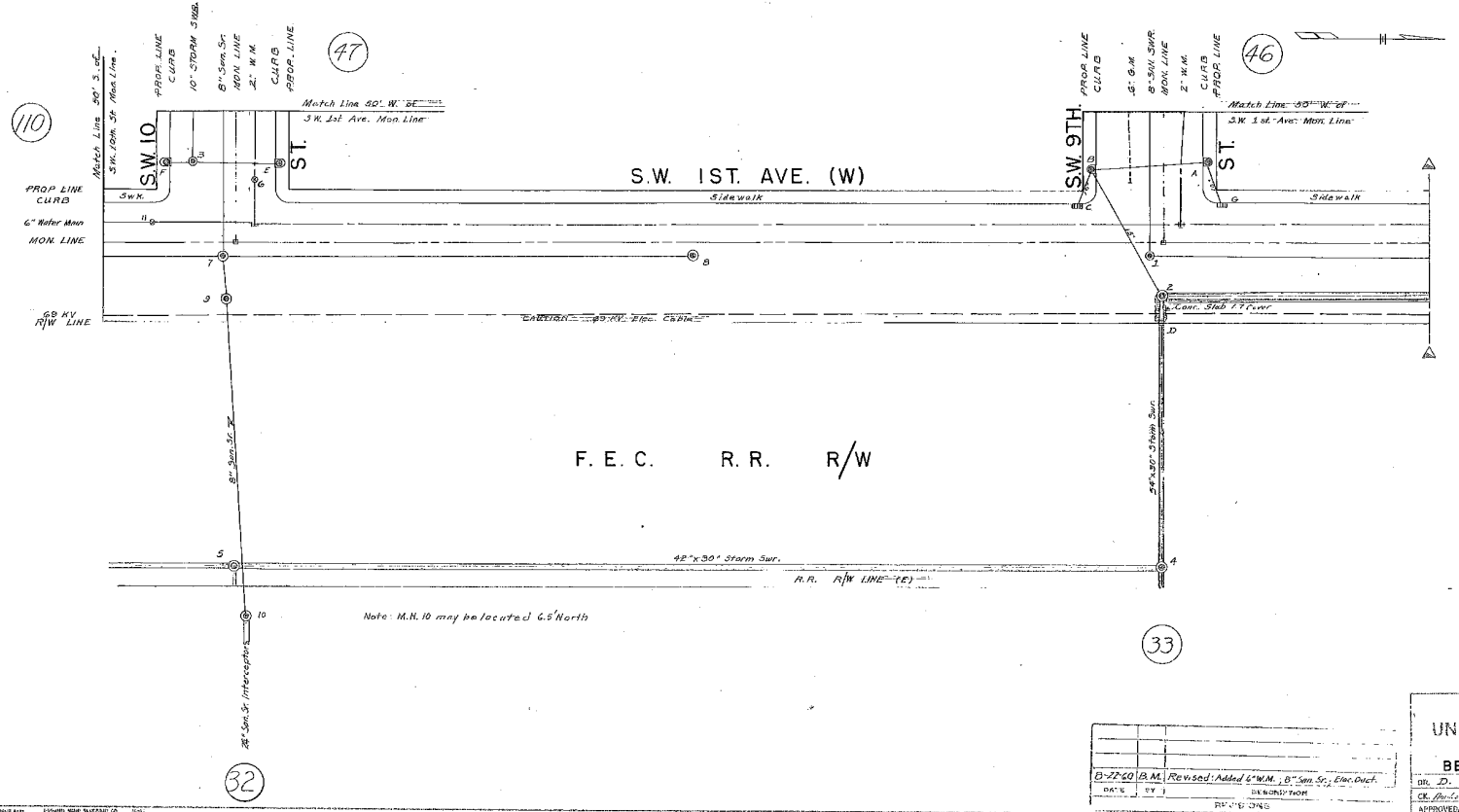
ON S.W. 9th ST.						
Utility	Location	Elevation	Size/Cover			
Water			2" 24'			
Gas	End of Main	TOP 120 6"				



(75)

REFERENCES

- LYONS
- Map 100
- Topographics Atlas A
- Sur. 590-57
- Sur. 602-38
- Plat 87B-37, 38, 45, 54
- Plat 88A-51-53
- Applied Plane Tables 19
- Sub. Insp. Plat. 121
- ELECTRIC
- UG. 231-A, 5
- UG. 111-42
- WATER
- Water 26: 162 (1)
- 2: 162 (2)
- Water Atlas 11-B
- E-7982
- SEWERS
- Counter Bks
- 340-25-97
- 341-1-1-9
- 342-54
- 343-10-11
- STORM SWR.
- 46-343-50, 51
- 34. Cont. 71 pg. 24
- GAS
- UG. 19-42, 46
- Atlas 42

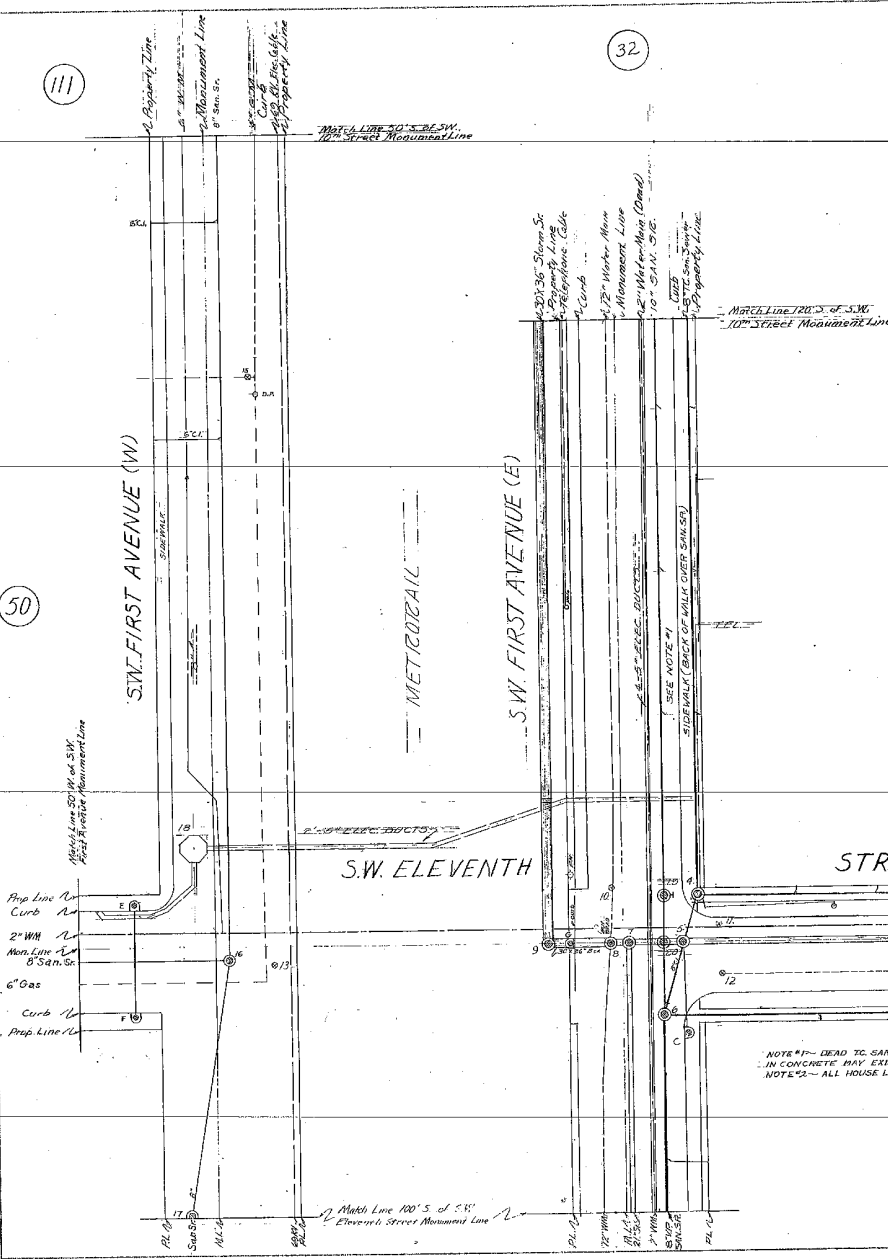


CITY OF MIAMI, FLORIDA  
 DEPARTMENT OF ENGINEERING  
**UNDERGROUND RECORDS.**  
 S.W. 1ST. AVE. (W)  
 BET. S.W. 8TH. ST. & 10TH. ST.

DR. D. WADSWORTH DATE 7-18-27 SCALE 1" = 50'  
 CK. D. L. HARRIS DATE 8-11-27  
 APPROVED *Quincy J. Harrington* 37-111

B-22018 AM	Revised: Added 6" W.M., 8" San Sw., Elec. Duct.
DATE	SY
BY	REVISION

- REFERENCES:
- Layout
  - Deductions
  - Plot Book
  - Monument D.C. 472-25
  - SURVEY BY 110045456
  - Underground B.C. 422-53
  - 422-53
  - 422-54
  - Telephone
  - Underground B.C. 423-31
  - 423-5
  - Underground B.C. 423-18, 419, 52
  - Sanitary Sewers
  - Sanitary D.C. 4260-30
  - 427-27-39
  - 428-10, 428-11, 428-12
  - Sanitary Sewers
  - County Books
  - Underground B.C. 422-53
  - 422-54
  - INSPECTOR CHAS. SWARTZ
  - ELECTRIC
  - 424-60-56
  - 425-77
  - SANITARY
  - CASH 4216-74
  - GAS
  - 425-86-1
  - WATER
  - 7902
  - 50642



NH	Utility	Run Elev	Set Elev	Elevation of Pipe or Duct	Spec	Com
1	St. St.	4.11	4.3	1.22	36\"/>	

ON SW 7<sup>TH</sup> AVENUE

Utility	Location	Elevation	Spec	Com
Telephone	30' S of SW 11 <sup>TH</sup> St.	1.68		2 1/2"
	N of SW 11 <sup>TH</sup> St.	1.31		
	200' N of SW 11 <sup>TH</sup> St.	1.31		
	200'	1.47		
Water	350'	1.6		
	Gas	25' N of 11 <sup>TH</sup> St. on 12 <sup>TH</sup> Ave (N)	0.00'	6"
ELEC.	100' N	0.00'		
	100' N	0.00'		
	254.6' N	0.00'		
	215' N	0.00'		
WATER	215' N	0.00'		
	215' N	0.00'		

ON SW 11<sup>TH</sup> STREET

Utility	Location	Elevation	Spec	Com
Gas	60' W of SW Main Rd. N	3.37		
"	200'	2.82		
"	300'	3.14		
Gas	60' W of Main Rd. B	0.00	6"	2 1/2"

NOTE #1 - DEAD TO SANITARY LATERALS INCISED  
 IN CONCRETE MAY EXIST IN THIS AREA  
 NOTE #2 - ALL HOUSE LOTS ON THIS ARE 30' x 6'

109

NO.	DATE	DESCRIPTION

CITY OF MIAMI, FLORIDA  
 DEPARTMENT OF ENGINEERING  
**UNDERGROUND RECORDS**  
 SW 1<sup>ST</sup> AVENUE & SW 11<sup>TH</sup> STREET  
 ORIGINAL RECORD DATE 7-5-57 SCALE 1" = 20'  
 CK. C. B. [Signature] DATE 8-2-57  
 APPROVED [Signature]

29

50

32



REFERENCE

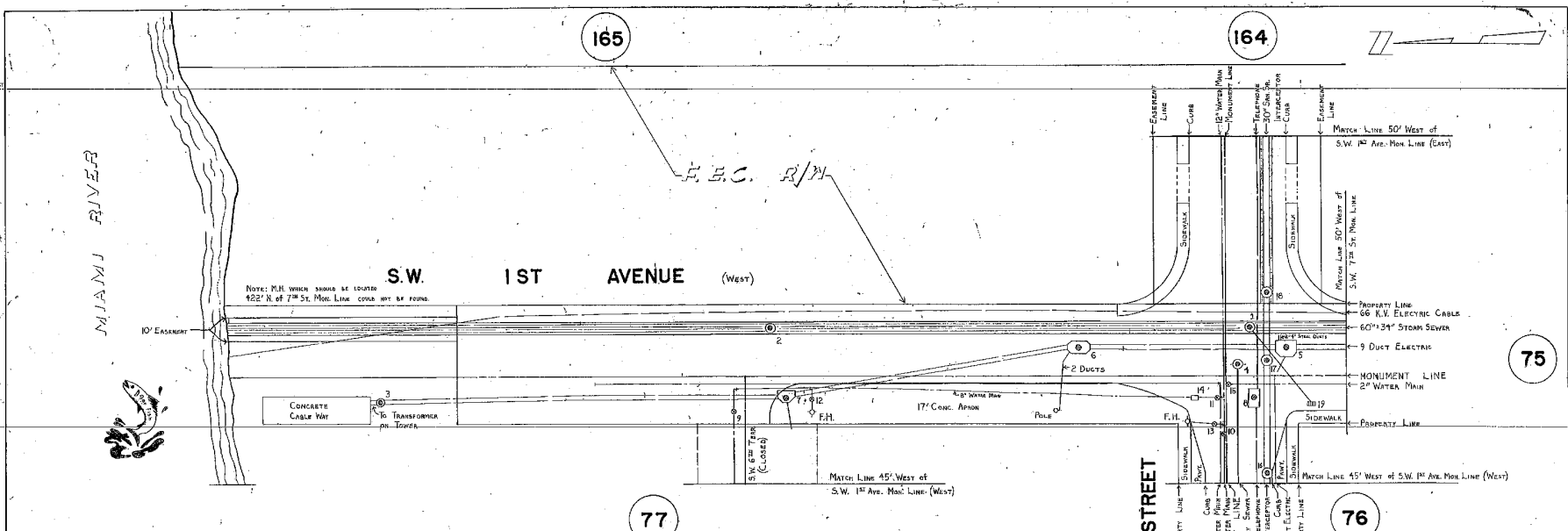
SEWERAGE  
S5-1: U.G. 408-14  
S5-2: INTERSECTION 7th St

STONE DRAIN  
S0-1: U.G. 408-14  
S0-2: U.G. 263-10  
S0-3: U.G. 260-23-24

WATER  
W1: U.G. 408-14  
W-2: U.G. 236-18  
W-3: 208-70 (Old Main)  
W-4: F-7096  
W-5: 191-2  
W-6: 194-1

ELECTRIC  
E-1: U.G. 408-14  
E-2: U.G. 263-10  
E-3: 9-19-55  
E-4: U.G. 312-39  
E-5: U.G. 231-34-30  
E-6: U.G. 111-34-32

TELEPHONE  
T-1: U.G. 408-14  
T-2: U.G. 263-10  
T-3: 8-4-54  
T-4: U.G. 34-57



MANHOLE INFORMATION

M.H.	UTILITY	RIP	BOY	ELEVATION	OF	SIZE	COVER	REF.
		DIAM.	DIAM.	TOP	OR			
				OR	DIAM.			
1	STORM S.W.	30"	30"	Inv. N	-0.56'	30"x30"	W-12	
2	"	5.68	"	" S.	-0.56'	"	"	
3	ELECTRIC	6.41	"	Inv. N.	-0.68'	"	SD-3	
4	STORM S.W.	7.35	"	" S.	-0.68'	"	"	
5	ELECTRIC	7.52	"	Inv. S.	2.09'	8"	E-2	
6	"	5.86	"	" W.	2.15'	"	55-1	
7	"	6.32	"	" N.	2.15'	"	E-2	
8	TELEPHONE	6.48	"	"	"	8"	W-3	
9	WATER MAIN	"	"	"	"	12"	W-2	
10	"	5.16	"	"	"	"	"	
11	"	5.61	"	"	"	8"	W-2	
12	"	6.24	"	"	"	8"	W-2	
13	"	5.82	"	"	"	6"	W-12	
14	WATER MAIN	"	"	"	"	24"	W-2	
15	WATER MAIN	5.83	"	Inv. W.	-3.30'	"	W-2	
16	STORM S.W.	5.36	"	" E.	-3.30'	30"	55-2	
17	"	7.33	"	Inv. W.	-3.26'	"	"	
18	"	8.96	"	" E.	-3.26'	"	"	
19	STORM C.B.	5.24	"	Inv. W.	-3.13'	"	"	
				" E.	-3.13'	"	"	
				Inv. N.E.	0.74'	12"	50-12	

ON S.W. 1ST AVENUE

UTILITY	LOCATION	ELEVATION	SIZE	COVER	REF.
ELECTRIC	At 7th St. Mon. L.	66.84'	0" SW	55"	E-5
"	100' N. of 7th St. Mon. L.	"	"	51"	"
"	150' N. " " "	"	"	78"	"
"	200' N. " " "	"	"	84"	"
"	At River Bulkhead	100.1.95'	"	90"	"
ELECTRIC	20' N. of 7th St. Mon. L.	100.2.72'	1" Duct	"	E-1
"	55' N. " " "	2.53'	"	"	"
"	98' N. " " "	0.99'	"	"	E-6
"	127' N. " " "	0.86'	"	"	"
"	152' N. " " "	0.42'	"	"	E-4
"	20' S. " " "	1.96'	"	"	"
WATER	1.2' N. of 7th St. Mon. L.	3.9'	8"	"	W-9
"	2.5' N. " " "	3.7'	"	"	"
"	50' N. " " "	4.2'	"	"	"
"	100' N. " " "	3.0'	"	"	"
"	150' N. " " "	3.0'	"	"	"
"	205' N. " " "	3.0'	"	"	"
WATER	"	2"	2"	"	W-3
ELECTRIC	"	2" Duct	"	"	E-3

ON S.W. 7TH STREET

UTILITY	LOCATION	ELEVATION	SIZE	COVER	REF.
WATER	20' W. of 1st Ave. Mon. L.	3.7'	12"	"	W-5
"	30' E. " " "	4.2'	"	"	"
"	80' P. " " "	4.5'	"	"	"
WATER	"	2"	"	"	W-6
TELEPHONE	23.0' W. of 1st Ave. Mon. L.	2.15'	2" Duct	"	T-3
ELECTRIC	8' E. of 1st Ave. Mon. L.	3.18'	1" Duct	"	E-4
"	At " " "	3.36'	"	"	"

CITY OF MIAMI, FLORIDA  
DEPARTMENT OF ENGINEERING  
**UNDERGROUND RECORDS**  
**S.W. 1ST AVENUE (West of RR)**  
**& S.W. 7TH STREET**

DR. R.J. FALSBY DATE 5-16-51 SCALE 1" = 20'  
CK. L.E. McCRA DATE 5-29-51

APPROVED: *[Signature]* 36-74

NO.	DATE	BY	REVISIONS

REFERENCE LAYOUT  
 T-1 MAP #34  
 SURVEY BY 1256-51  
 W-10 UG SHEET 37-23  
 HOPKINS - F-14  
 ROW DEDICATION BOOKS  
 UG 14-32,15

**MANHOLE INFORMATION**

M.H.	UTILITY	RIM ELEV.	BOX ELEV.	ELEVATION OF PIPE OR DUCT	SIZE	COVER	REF.
1	STORM	8.82		S.E. INK 4.42	10"	35-7	
2	STORM	3.02		" " 3.35	10"	35-7	
3	SAN. SE	3.17		" " 4.11	8"	35-7	
4	SAN. SE	3.31		" " 4.07	8"	35-7	
5	SAN. SE	3.53		" " 4.00	6"	35-7	
6	SAN. SE	3.61		" " 3.98	6"	35-7	
7	SAN. SE	3.80		" " 4.00	6"	35-7	
8	WATER	3.60		" " 4.00	2"	35-7	
9	PHONE	3.00		" " 3.93	5/8"	7-2	
10	ELEC.	3.02		LAT. N. 4.41	4/8"	49"	
11	ELEC.	3.02		INK 5.65	10"	35-7	
12	WATER	3.02		" " 3.93	5/8"	7-2	
13	STORM	3.02		" " 3.93	12"	35-7	
14	STORM	3.17		" " 3.93	12"	35-7	
15	W.M.	3.17		" " 3.93	16"	W-3	

NOTE: CAR TRACKS HAVE BEEN REMOVED FROM S. MIAMI AVE. CROSS TIES MAY STILL REMAIN.

WATER  
 W-1 OLD WATER  
 BOOK-400,402, 403

GAS  
 INDEX SHEET #42  
 UG 19-32  
 Q-1 PERMIT # 243-1  
 Q-2 # 422  
 Q-3 # 2803

SANITARY SEWER  
 COUNTER BOOK  
 95-1 UG. 120-39

STORM SEWER  
 UG 14-38  
 STE 2-92-327-58

TELEPHONE  
 T-1 UG 120-33  
 T-2 " 35A-42  
 T-3 " 370-37426  
 T-4 PERMIT 3-7427  
 T-5 575-963  
 T-6 575-963  
 T-7 7-13-80

ELECTRIC  
 E-2 PERMIT 8-2-54  
 E-3 PERMIT 9-9-83  
 E-4 PERMIT 9-21-66  
 E-5 " 7-24-85  
 E-6 " 6-25-69

110

21

**S. MIAMI AVE.**

UTILITY	LOCATION	ELEVATION	SIZE	COVER	REF.
GAS	170' N. OF S.W. II ST.	7.0 P. 4.1	6"	6-1	
"	" " "	" " 4.3	6"	6-1	
"	" " "	" " 6.1	6"	6-1	
"	" " "	" " 6.5	6"	6-1	
PHONE					
WATER			6"	W-1	
ELEC.			2"	W-1	
TELEPHONE			16"	W-3	

28

**S.E. MIAMI AVE. ROAD**

UTILITY	LOCATION	ELEVATION	SIZE	COVER	REF.
PHONE	FROM 11 ST. N. EXT. TO S.E. 21'S.		24"	7-3	
ELECTRIC VAULT	123' N. OF S.E. 11 ST. N.			E-2	
WATER			2"	W-1	
ELEC.			CABLE	E-8	
ELEC.			6-3"	E-8	
TELEPHONE			CABLE	7-9	
WATER			2"	W-3	

**S.W. & S.E. 11 STREET**

UTILITY	LOCATION	ELEVATION	SIZE	COVER	REF.
GAS	ON MIA. AVE. N. 100' W. OF MIA. AVE. N.	7.0 P. 3.9	6"	6-2	
"	" " "	" " 4.4	6"	6-2	
"	" " "	" " 4.0	6"	6-2	
PHONE	412' MIA. AVE. N.	7.0 P. 6.66	24"	7-1	
PHONE	" " "	" " 6.98	24"	7-1	
"	FROM 5.5' TO 168.5' E. OF MIA. AVE. N.		30"	7-3	
WATER	N. OF MIA. AVE. N.		2"	W-1	
ELEC.			CABLE	7-4	
"			"	7-6	

CITY OF MIAMI, FLORIDA  
 DEPARTMENT OF ENGINEERING  
**UNDERGROUND RECORDS**  
**S.E. & S.W. 11 ST. AT S. MIA. AVE**  
**S.E. 11 ST. AT S. MIA. AVE. RD**

11-6-83	W.S.	UPDATED
3-2-66	M.S.	REVISED TO DATE
8-7-62	B.M.	CHECKED - TRACED - REVISED TO DATE
DATE	BY	DESCRIPTION
REVISIONS		

DR. R. A. WILLIAMS DATE 3-2-56 SCALE 1" = 20'  
 CR. S. MENARD DATE 8-6-62  
 APPROVED BY *Henry J. Hernandez* 8-9-62 **37-29T**

30

S.E.

REFERENCE  
 LAYOUT  
 DETAIL PLAT # 34  
 L 95 192-30  
 1 215-14  
 SUB. BK. 1256-51  
 R/W DEDICATION BK.

WATER  
 WM-1 UG 104-24  
 WM-2 OLD WATER BK.  
 WM-3 E-7985  
 WM-4 E-8385

GAS  
 G-1 PERMITS # 249  
 G-2 UG 104-50  
 G-3 FLORIDAGAS CO. I-B-808

TELEPHONE  
 T-1 UG 125-54  
 T-2 PERMITS DATE 3-17-41  
 T-3 " " " 3-16-70  
 T-4 " " " 9-23-40  
 T-5 " " " 5-11-53

SEWER  
 SS-1 UG 120-3758  
 SS-2 45' BUILT  
 WATER SERVICE  
 PL AND B. 56  
 WATER BOOK  
 SS-3 36540-18

ELECTRIC  
 E-1 PERMIT DATE 8-28-69  
 E-2 PERMIT DATE 3-15-66

TV CABLE  
 TV-1 PERMIT DATE 1-18-68

**MANHOLE INFORMATION**

M.H.	UTILITY	CONV. ELEV.	ELEVATION OF PIPE OR DUCT	SIZE	COVER	REF.
1	SAN. SE.	5.44	N. INK 3.22	6"	35-1	
2	STORM	5.15	S. " (-) 3.28	24"	OR 147	
3	STORM	5.88	S. " (-) 0.20	15"	35-1	
4	SAN. SE.	6.09	W. " (-) 0.71	10"	35-1	
5	PHONE	5.80	W. " (-) 0.71	10"	35-1	
6	WATER	5.78	W. " (-) 0.71	6"	35-1	
7	WATER	5.55	W. " (-) 0.71	6"	35-1	
8	WATER	5.72	W. " (-) 0.71	6"	35-1	
9	WATER	6.34	W. " (-) 0.71	6"	35-1	
10	SAN. SE.	7.05	W. INK 3.51	6"	35-1	
11	WATER	6.17	S. E. " 4.01	6"	35-1	
12	SAN. SE.	6.17	E. INK (-) 0.88	24"	35-2	
13	SAN. SE.	6.41	W. " (-) 0.85	24"	35-2	
14	C.B.E.	5.97	S. " (-) 3.05	8"	35-2	
15	"	5.66	W. " (-) 0.67	24"	35-2	
16	"	5.57	N.W. " 1.58	10"	35-1	
17	"	5.52	S. E. " 2.84	6"	35-1	
18	SAN. SE.	6.37	N.W. INK 3.20	6"	35-1	
19	SAN. SE.	4.84	E. INK 1.18	24"	35-3	
20	STORM	5.91	E. INK 0.88	24"	35-3	
21	"	5.48	E. INK 2.16	15"	"	
22	"	5.35	W. INK 2.08	15"	"	
23	WATER	6.48	E. INK 2.03	12"	"	
24	ELEC.	TEL.	W. INK 2.03	12"	"	
25	"	"	W. INK 2.03	12"	"	
26	"	"	W. INK 2.03	12"	"	

**S. MIAMI AVENUE**

UTILITY	LOCATION	ELEVATION	SIZE	COVER	REF.
GAS	15' S. OF 10 ST. N	T.O.P. 2.4	6"	G-1	
"	"	" 3.0	6"	"	
"	"	" 3.68	3"	"	
WATER	AT 10 ST. N	T.O.P. 3.49	6"	WM-2	
PHONE	FROM 10 S. ST. 10 ST	"	30"	T-3	

**S. E. & S. W. 10 STREET**

UTILITY	LOCATION	ELEVATION	SIZE	COVER	REF.
PHONE	AT 10 S. M. SIDE ST	T.O.P. 4.52	"	T-1	
"	AT 10 S. M. SIDE ST	" 3.59	"	"	
"	AT CURB S. SIDE ST. 75' E. M. M. AVE	" 3.65	"	"	
GAS	277.5' W. M. M. AVE. ROAD	T.O.P. 3.81	2"	G-2	
"	200' " " " "	" 3.86	2"	"	
"	100' " " " "	" 3.98	2"	"	
"	10.0' " " " "	" 3.78	2"	"	
WATER	RETICED	"	"	"	
WATER	73.4' W. M. M. AVE. AT 10 S. ST	T.O.P. 4.38	6"	WM-3	
"	77.4' " " " "	" 2.38	6"	3.0"	
"	120' " " " "	" 2.16	6"	3.0"	
PHONE	AT MATCH LINE # 10 S. ST. 10 S. ST	T.O.P. 3.81	3.5"	T-3	
"	AT 10 S. ST. 10 S. ST	" 4.0	4.0"	"	
"	AT 10 S. ST. 10 S. ST	" 4.0	4.0"	"	
"	AT 10 S. ST. 10 S. ST	" 1.0	11"	3.1"	
"	AT 10 S. ST. 10 S. ST	" 1.0	11"	3.1"	
"	AT 10 S. ST. 10 S. ST	" 1.0	11"	3.1"	

**S. E. MIAMI AVE. ROAD**

UTILITY	LOCATION	ELEVATION	SIZE	COVER	REF.
GAS	54' N. OF S. E. MIAMI AVE. ROAD	T.O.P. 3.70	2"	G-2	
"	100' " " " "	" 3.66	2"	"	
"	15' " " " "	" 3.44	2"	"	
WATER	AT 10 S. ST. 10 S. ST	10.9	4.0	WM-3	
GAS	" " " " "	" 3.6	2"	G-2	
"	" " " " "	" 4.7	2"	"	
"	" " " " "	" 4.8	2"	"	

32

22

29

CITY OF MIAMI, FLORIDA  
 DEPARTMENT OF ENGINEERING  
**UNDERGROUND RECORDS**  
**SE. & SW. 10 ST. AT S. MIA. AVE.**  
**SE. 10 ST. AT S. MIA. AVE. ROAD**

DR. R.A. WILLIAMS DATE 4-7-56 SCALE 1" = 20'  
 CK. S. WARETS DATE 4-28-56  
 APPROVED *Richard S. Maroney* 8-2-62

37-30

REVISIONS

NO.	DATE	BY	REVISIONS
11-06-65	ACK		REVISED TO DATE
8-27-71	AB		ADDED SOUTHSIDE SAN.
3-3-66	RRE		REVISED TO DATE
1-25-66	MXB		MATCH LINE ON SE. 10th ST. (E) MOVED EAST
8-2-62	B.M.		TRACED & REFS AD TO DATE



REFERENCES  
LAYOUT  
FDL10 121 B  
T&T MAP 35  
SURVEY BOOK 1250-51  
U.S. BK. 120-36

WATER  
M&T OLG. WATER BOOK  
SHEETS 903&94-3  
M&T E-177D

SANITARY SEWER  
S&T U.S. 105-GO  
COUNTER BOOK

STORM SEWER  
S&T U.S. 100-135-36  
S&T-2 " 406-25

TELEPHONE  
T-1 U.S. 521-H  
T-2 " 274-55  
T-3 " 244-55  
T-4 " 129-25  
T-5 " 235-4

GAS  
GAS ATLAS  
PHOENIX

129

23

30

**MANHOLE INFORMATION**

M.N.	UTILITY	DATE	ROD	ELEVATION OF PIPE OR DUCT	SIZE	CORR.	REF.
1	STM.S.E.	4.49	E. I.N.V.	25.112	27" DIA		50-1
2	STM.S.E.	5.05	W. "	1.18	36" DIA		
			N. "	1.47	12"		
3	SAN.S.E.	4.87	S. "	0.59	12"		50-1
			W. "	1.35	36" DIA		
4	SAN.S.E.	4.80	N.W. "	0.83	12"		
			S.W. "	0.69	12"		
5	SAN.S.E.	4.87	E. "	2.66	6"		50-1
			W. "	2.67	6"		
6	SAN.S.E.	4.80	N. "	2.66	6"		50-1
			W. "	2.50	6"		
7	WATER	5.24	E. "	2.66	6"		50-1
			W. "	2.50	6"		
8	"	4.80	"	"	"	"	"
9	STM.S.E.	4.87	T.O.P.	1.59	4"	W-2	50-1
10	STM.S.E.	4.87	E. I.N.V.	1.58	36" DIA		50-1
			W. "	1.58	36" DIA		
11	SAN.S.E.	4.79	N.E. "	1.55	12"		50-1
			S.E. "	1.63	12"		
12	SAN.S.E.	4.60	W. "	1.80	36" DIA		50-1
			N.W. "	3.30	6"		
13	C.B."E.	5.06	T.O.P.	4.05	6"		50-1
			ELEV. TO M&T				
M	"	5.25	S.E.	1.45	12"		50-1
N	"	5.19	N.W.	1.15	12"		50-1
14	"	5.27	N.E.	1.62	12"		50-1
17	"	7.3	N.E.	2.43	12"		50-2
18	"	7.3	S.W.	2.87	12"		50-2
19	"	4.57	W. "	2.09	12"		50-2

**S. MIAMI AVE.**

UTILITY	LOCATION	ELEVATION	SIZE	CORR.	REF.
TELEPHONE	25.8' W. OF M.H. 6	T.O.P. 3.25	2.1"	7-4	
"	60' N. "	" 3.25	2.06"	7-4	
GAS	"	"	"	"	"
WATER	"	"	"	"	"
TELEPHONE	"	"	"	"	"

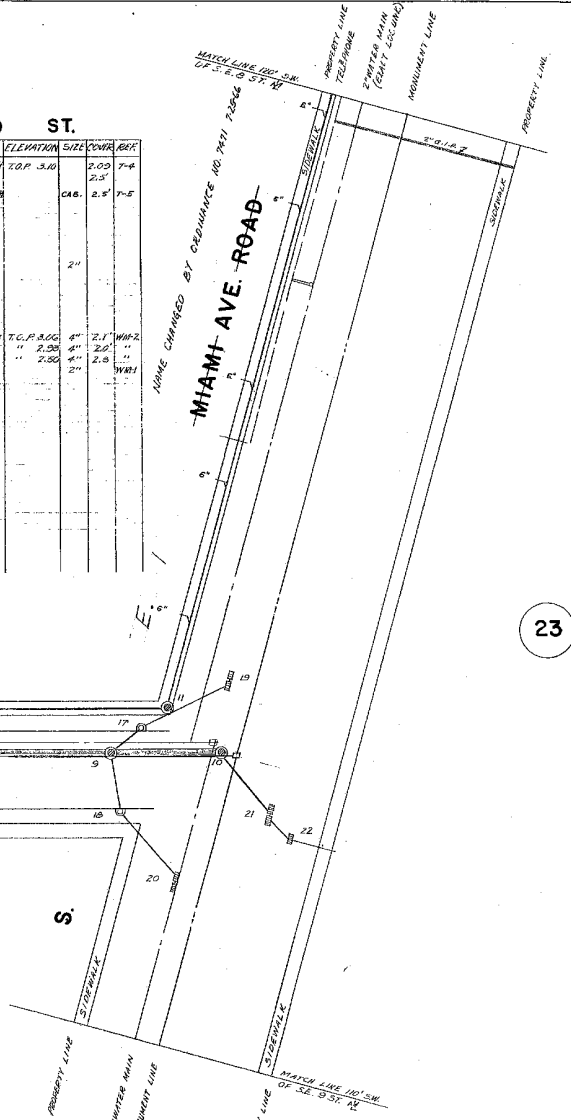
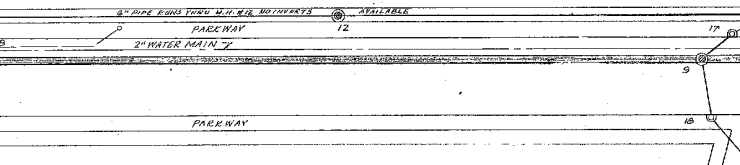
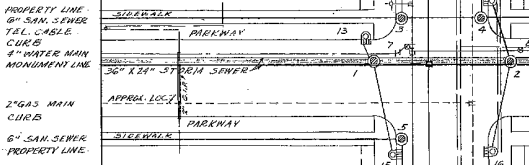
**S.W. & S.E. 9 ST.**

UTILITY	LOCATION	ELEVATION	SIZE	CORR.	REF.
TELEPHONE	71' E. OF MIAMI AVE N. 30.5' N.	T.O.P. 3.10	2.09	7-4	
TEL.	71.5' W. OF MIAMI AVE	"	2.5'	7-5	
GAS	"	"	2"	"	"
WATER	104' W. MIAMI AVE N. 30.0' N.	T.O.P. 3.00	4"	2.1	W-2
"	120.0' " " "	" 2.36	4"	2.8	"
"	" " " "	" 2.36	4"	2.8	W-1
"	" " " "	"	2"	"	"

NOTE: CAR TRACKS HAVE BEEN REMOVED FROM S. MIAMI AVE. CROSS TIES MAY STILL REMAIN.

**S.W. 9 ST.**

**S.E. 9 ST.**



**MANHOLE INFORMATION**

M.N.	UTILITY	DATE	ROD	ELEVATION OF PIPE OR DUCT	SIZE	CORR.	REF.
19	C.B."E.	4.78	S.W. I.N.V.	2.51	12"		50-2
20	C.B."E.	4.46	N.W. "	2.95	12"		50-2
21	"	5.12	N.W. "	2.77	12"		50-2
22	C.B."E.	4.80	S.E. "	4.77	12"		50-2
			E. "	2.60	6"		50-2
			N.W. "	2.72	12"		50-2

**S. MIAMI AVE. ROAD**

UTILITY	LOCATION	ELEVATION	SIZE	CORR.	REF.
TELEPHONE	115' N. OF S.E. 9 ST. N.	"	2.5"	7-1	
"	171.9' N. " " "	"	2.5"	7-2	
"	125.5' " " "	"	2.5"	7-3	
WATER	"	"	2"	W-1	

CITY OF MIAMI, FLORIDA  
DEPARTMENT OF ENGINEERING  
**UNDERGROUND RECORDS**  
**S.W. & S.E. 9 ST. AT S. MIAMI AVE.**  
**S.E. 9 ST. AT S. MIA. AVE. RD.**

DR. R.A. WILLIAMS DATE 3-28-50 SCALE 1" = 20'  
CK. H. MIGNARD DATE 7-27-62  
APPROVED *Anthony J. Mansueto* 7-27-62

DATE	BY	DESCRIPTION
		REVISIONS



REFERENCES:  
 MISC.:  
 R-1: P.V. BK. 884-51 4  
 R-2: SK 121, SUR. 1188-47  
 R-3: UG. 124-22, 26  
 R-4: SUR. BK. 675-27  
 R-5: P.V. BK. 333-33  
 R-5: OLD MANILA 37-33

ELECTRIC:

GAS:  
 G-1: PHOENIX 315, 4  
 G-2: GAS ATLAS 54, 62  
 G-3: UG. 124-22, 26

SANITARY SEWER:  
 SS-1: UG. 22-26, 28, 30, 32, 34  
 SS-2: SAN. LATERAL 35-35  
 SS-3: INT. 35 BUILTS (26)  
 SS-4: INT. 35 BUILTS (26)  
 SS-5: INT. 35 BUILTS (26)  
 SS-6: INT. 35 BUILTS (26)  
 SS-7: INT. 35 BUILTS (26)  
 SS-8: INT. 35 BUILTS (26)  
 SS-9: INT. 35 BUILTS (26)  
 SS-10: INT. 35 BUILTS (26)  
 SS-11: INT. 35 BUILTS (26)  
 SS-12: INT. 35 BUILTS (26)  
 SS-13: INT. 35 BUILTS (26)  
 SS-14: INT. 35 BUILTS (26)  
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 SS-18: INT. 35 BUILTS (26)  
 SS-19: INT. 35 BUILTS (26)  
 SS-20: INT. 35 BUILTS (26)  
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 SS-22: INT. 35 BUILTS (26)  
 SS-23: INT. 35 BUILTS (26)  
 SS-24: INT. 35 BUILTS (26)  
 SS-25: INT. 35 BUILTS (26)  
 SS-26: INT. 35 BUILTS (26)  
 SS-27: INT. 35 BUILTS (26)  
 SS-28: INT. 35 BUILTS (26)  
 SS-29: INT. 35 BUILTS (26)  
 SS-30: INT. 35 BUILTS (26)  
 SS-31: INT. 35 BUILTS (26)  
 SS-32: INT. 35 BUILTS (26)  
 SS-33: INT. 35 BUILTS (26)  
 SS-34: INT. 35 BUILTS (26)  
 SS-35: INT. 35 BUILTS (26)  
 SS-36: INT. 35 BUILTS (26)  
 SS-37: INT. 35 BUILTS (26)  
 SS-38: INT. 35 BUILTS (26)  
 SS-39: INT. 35 BUILTS (26)  
 SS-40: INT. 35 BUILTS (26)  
 SS-41: INT. 35 BUILTS (26)  
 SS-42: INT. 35 BUILTS (26)  
 SS-43: INT. 35 BUILTS (26)  
 SS-44: INT. 35 BUILTS (26)  
 SS-45: INT. 35 BUILTS (26)  
 SS-46: INT. 35 BUILTS (26)  
 SS-47: INT. 35 BUILTS (26)  
 SS-48: INT. 35 BUILTS (26)  
 SS-49: INT. 35 BUILTS (26)  
 SS-50: INT. 35 BUILTS (26)

STORM DRAINAGE:  
 SD-1: UG. 124-22, 26, 30, 32, 34  
 SD-2: SR. 250-27, 29, 32  
 SD-3: MISC. 34, 4-11

TELEPHONE:  
 T-1: PERMIT 2-5-53

WATER:  
 W-1: UG. 22-26, 28, 30, 32, 34  
 W-2: E-775  
 W-3: UG. 124-22, 26

MANHOLES

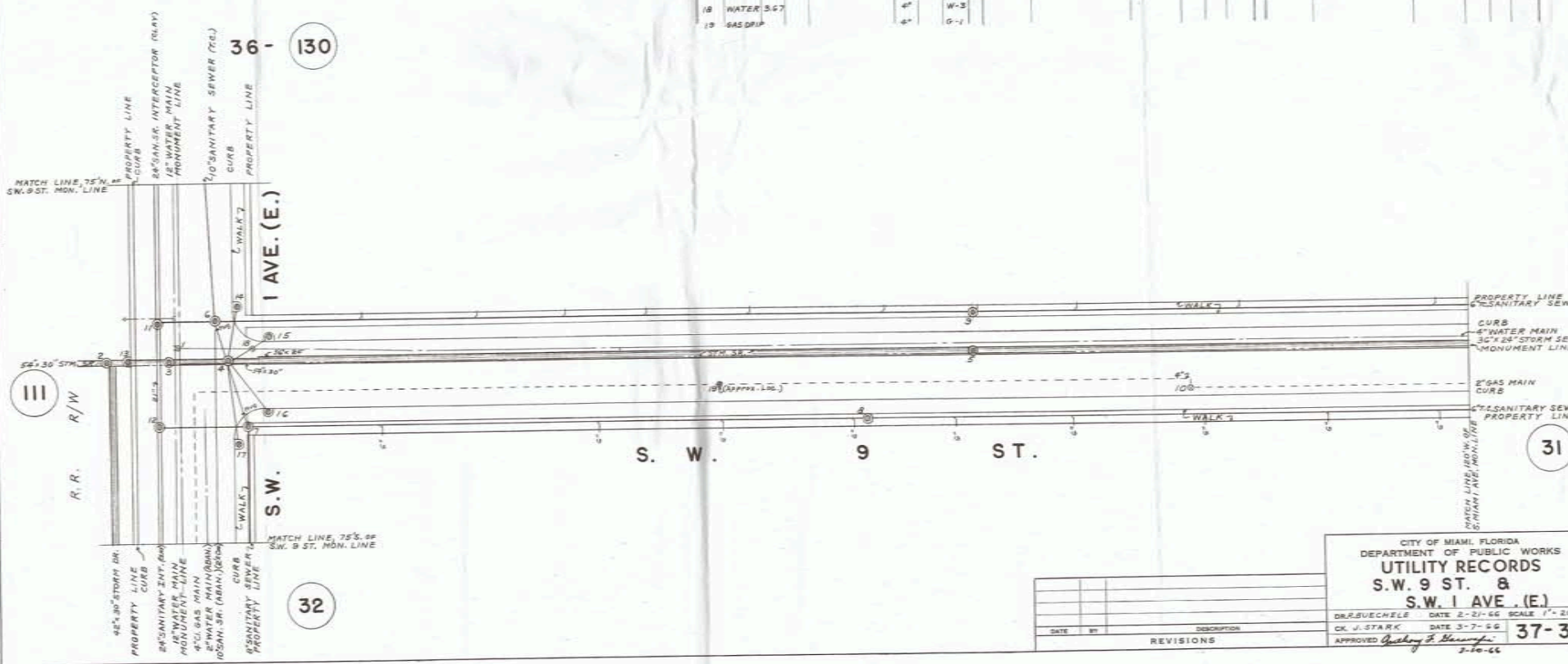
M.H.	UTILITY	R/W	SO	ELEVATION OF	PIPE OR DUCT	SIZE	CON.	REF.
1	WATER	4.2		T.O.P. BYAL: 1.05	4"	4"	W-2	
2	STM. SR.	4.35	0.15	W. Inv.: 0.15 S. " = 0.15 E. " = 0.15	30"	30"	SD-2	
3	STM. SR.	4.12		W. Inv.: 0.15	30"	30"	SD-2	
4	STM. SR.	3.95	0.60	E. Inv.: 0.60 N.-W. Inv.: 0.81 N. E. " = 0.87 S.-S. E. " = 0.79	30"	30"	SD-2	
5	STM. SR.	4.42	0.75	E. Inv.: 0.75	30"	30"	SD-2	
6	SAN. SR.	3.89		W. Inv.: 0.85 S. E. " = 1.42 E. " = 1.87 N. " = 1.10	8"	8"	SS-12	
7	SAN. SR.	3.85		N.W. Inv.: 1.41 S. " = 1.43 E. " = 1.43 W. " = 1.37	8"	8"	SS-3	
8	SAN. SR.	4.00		E. Inv.: 1.69 W. " = 1.73	8"	8"	SS-2	
9	SAN. SR.	4.41		E. Inv.: 1.82 W. " = 1.80	8"	8"	SS-2	
10	GAS				2"	2"	G-1, 2	
11	SAN. SR.	4.00		N.E. Inv.: 2.04 E. " = -0.71	8"	8"	SS-3	
12	SAN. SR.	3.88		N.E. Inv.: 2.04 E. " = -0.70	8"	8"	SS-3	
13	CB*F-3	4.23	-0.01	E. Inv.: 0.21	12"	12"	SD-1	
14	CB*F-3	4.01		S. Inv.: 0.57	12"	12"	SD-1	
15	CB*F-3	3.88		SW. Inv.: 0.55	12"	12"	SD-1	
16	CB*F-3	3.87		N.W. Inv.: 1.54	12"	12"	SD-1	
17	CB*F-3	3.94		N. Inv.: 1.27	12"	12"	SD-1	
18	WATER	3.67			4"	4"	W-3	
19	GAS DRIP				4"	4"	G-1	

S.W. 9 ST.

UTILITY	LOCATION	ELEVATION	SIZE	CON.	REF.
WATER	2 1/2" W.P. AVE. NE	T.O.P.: 1.96 194'E. " = -0.39 155'E. " = -0.21 100'E. " = 1.31 200'E. " = 1.69 300'E. " = 1.82 400'E. " = 2.23	4"	W-2	
GAS	5 5/8" SLSL - 1/4" W.P.	T.O.P.: 2.41 UNK. " = 1.91	4"	G-1	

S.W. 1 AVE.

UTILITY	LOCATION	ELEVATION	SIZE	CON.	REF.
GAS	12" x 7 1/2" W.P. 9 ST. W	T.O.P.: 0.57 100' W. W.P. 9 ST. W " = 0.71 15' S. " = 0.53 50' S. " = 1.01	4"	G-1	
WATER	100' W. W.P. 9 ST. W	T.O.P.: 1.02	12"	W-1	



CITY OF MIAMI, FLORIDA  
 DEPARTMENT OF PUBLIC WORKS  
**UTILITY RECORDS**  
**S.W. 9 ST. & S.W. 1 AVE. (E.)**

DATE	BY	DESCRIPTION	SCALE
			1" = 20'

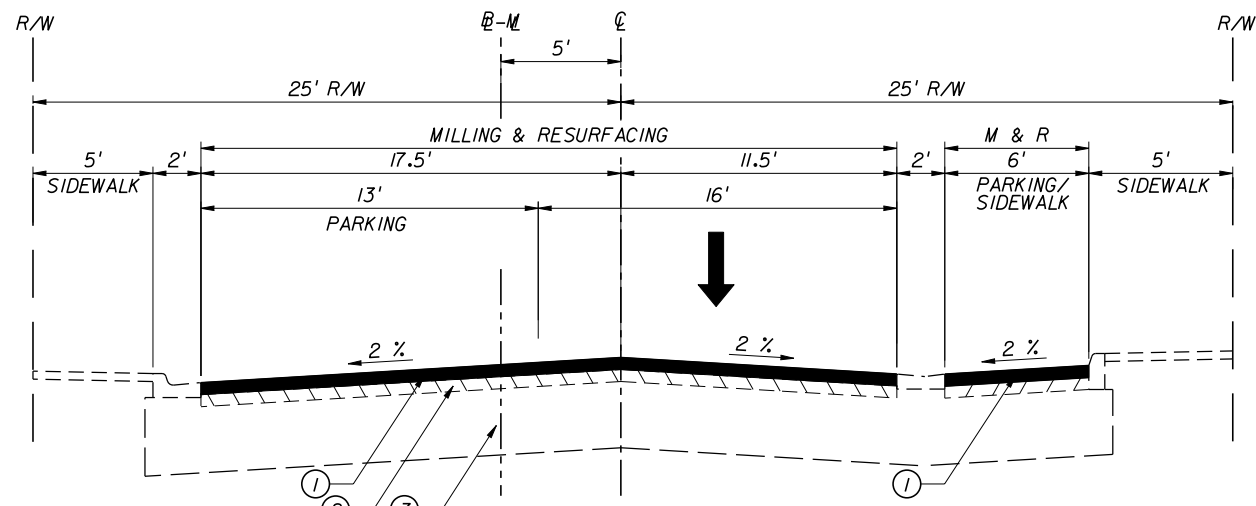
APPROVED: *Anthony F. Blawie* 2-10-66

31

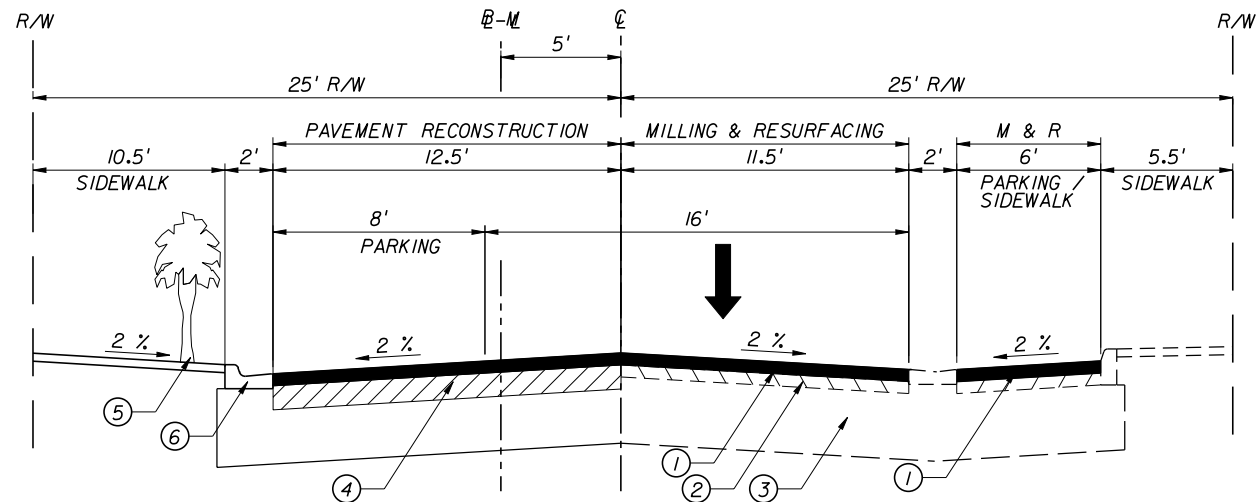
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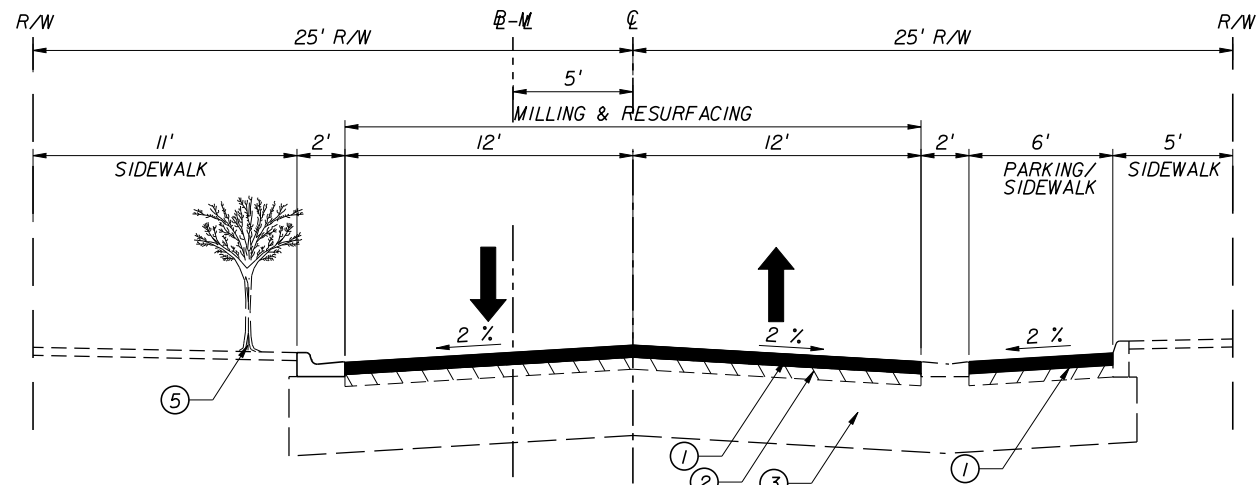
**APPENDIX B – ROADWAY TYPICAL SECTIONS**



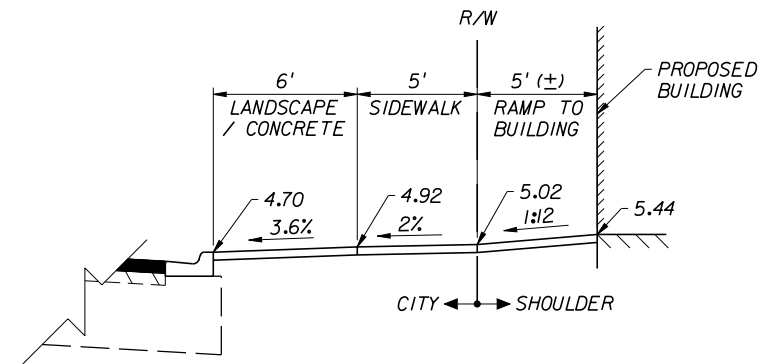
**TYPICAL SECTION S.W. 9th STREET**  
FROM STA. 10+00.00 TO STA. 12+29.60  
N.T.S.



**TYPICAL SECTION S.W. 9th STREET**  
FROM STA. 12+29.60 TO STA. 16+42.85  
N.T.S.



**TYPICAL SECTION S.E. 9th STREET**  
FROM STA. 16+81.21 TO STA. 19+67.76  
N.T.S.



**SECTION A-A**  
(SEE SHEET No. 13)  
N.T.S.

- ① PROPOSED MILLING & RESURFACING (MILL 1" AND RESURFACE WITH 1" OF SUPERPAVE ASPHALT PER DOT STANDARDS), REFER TO PLANS FOR LIMITS.
- ② EXISTING LIMEROCK BASE (8" MINIMUM THICKNESS)
- ③ EXISTING SUBGRADE.
- ④ RECONSTRUCT PAVEMENT SECTION PER CITY OF MIAMI PUBLIC WORKS STANDARD 35-85-37. REFER TO SHEET No. 17 AND No. 23.
- ⑤ REFER TO ROADWAY PLANS FOR PLANTER LOCATIONS.
- ⑥ PROPOSED CURB AND GUTTER TYPE "F", REFER TO ROADWAY PLANS FOR LOCATIONS.



REVISIONS			
DATE	DESCRIPTION	DATE	DESCRIPTION

**T·Y·LIN INTERNATIONAL**  
201 ALHAMBRA CIRCLE SUITE 900  
Coral Gables, Florida. 33134  
Phone: 305 / 567-1888 Fax: 305 / 567-1771

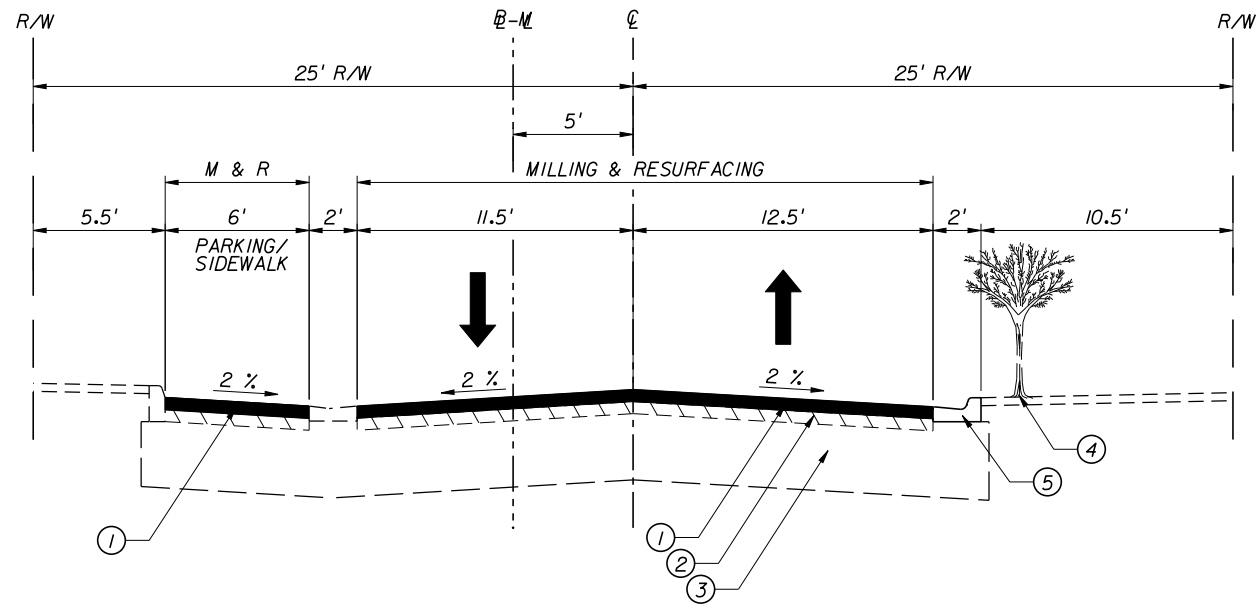


**CITY OF MIAMI**  
MARY BRICKELL VILLAGE  
DRAINAGE AND ROADWAY IMPROVEMENTS - PHASE 1  
SWISE 9th STREET FROM W 1st AVENUE TO E 1st AVENUE (BRICKELL PLAZA)  
SWISE 10th STREET FROM W 1st AVENUE TO E 1st AVENUE (BRICKELL PLAZA)  
SWISE 11th STREET FROM W 1st AVENUE TO SOUTH MIAMI AVENUE  
SW 12th STREET FROM W 1st AVENUE TO SE 1st AVENUE (BRICKELL PLAZA)  
CITY OF MIAMI PROJECT NUMBER: B-30637

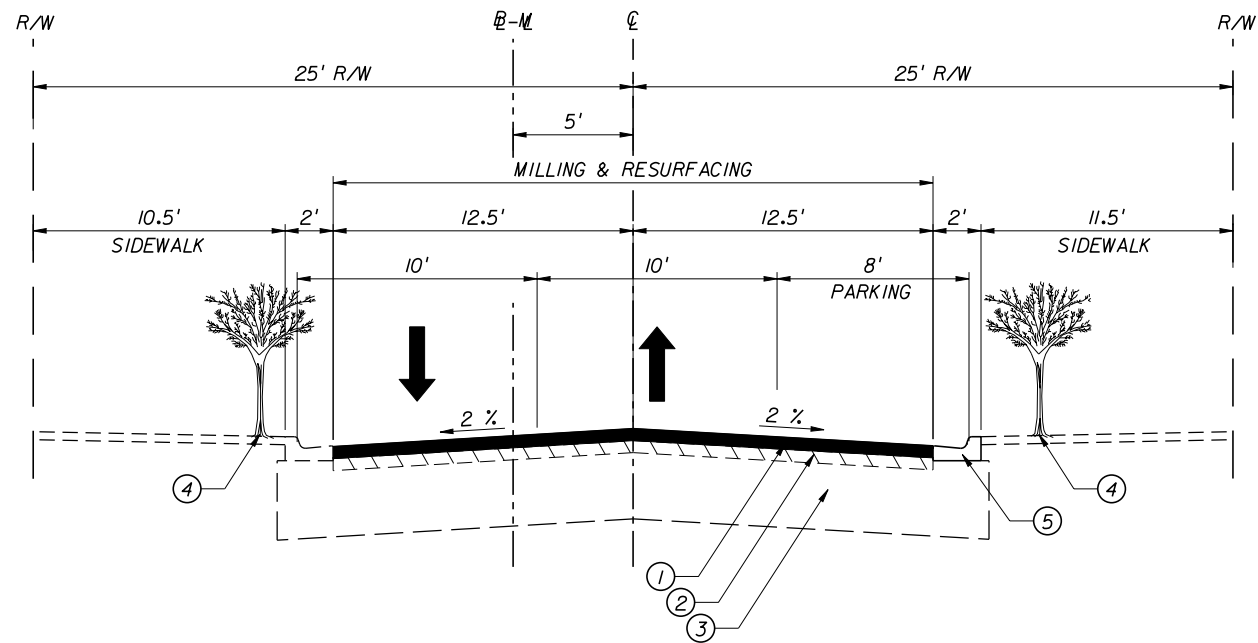
**TYPICAL SECTION**  
**S.W./S.E. 9th STREET**

SHEET NO.  
**4**

FOR CONSTRUCTION 100% PLANS



**TYPICAL SECTION S.W. 10th STREET**  
FROM S.W. 1st AVENUE TO SOUTH MIAMI AVENUE  
N.T.S.



**TYPICAL SECTION S.E. 10th STREET**  
FROM SOUTH MIAMI AVENUE TO  
S.E. 1st AVENUE (BRICKELL AVENUE)  
N.T.S.

- ① PROPOSED MILLING & RESURFACING (MILL 1" AND RESURFACING WITH 1" OF SUPERPAVE ASPHALT PER DOT STANDARDS), REFER TO PLANS FOR LIMITS.
- ② EXISTING LIMEROCK BASE (8" MINIMUM THICKNESS)
- ③ EXISTING SUBGRADE.
- ④ REFER TO ROADWAY PLANS FOR PLANTER LOCATIONS.
- ⑤ REPLACE CURB AND GUTTER TYPE "F", REFER TO ROADWAY PLANS FOR LOCATIONS.



R E V I S I O N S			
DATE	DESCRIPTION	DATE	DESCRIPTION

**T·Y·LIN INTERNATIONAL**  
201 ALHAMBRA CIRCLE SUITE 900  
Coral Gables, Florida. 33134  
Phone: 305 / 567-1888 Fax: 305 / 567-1771



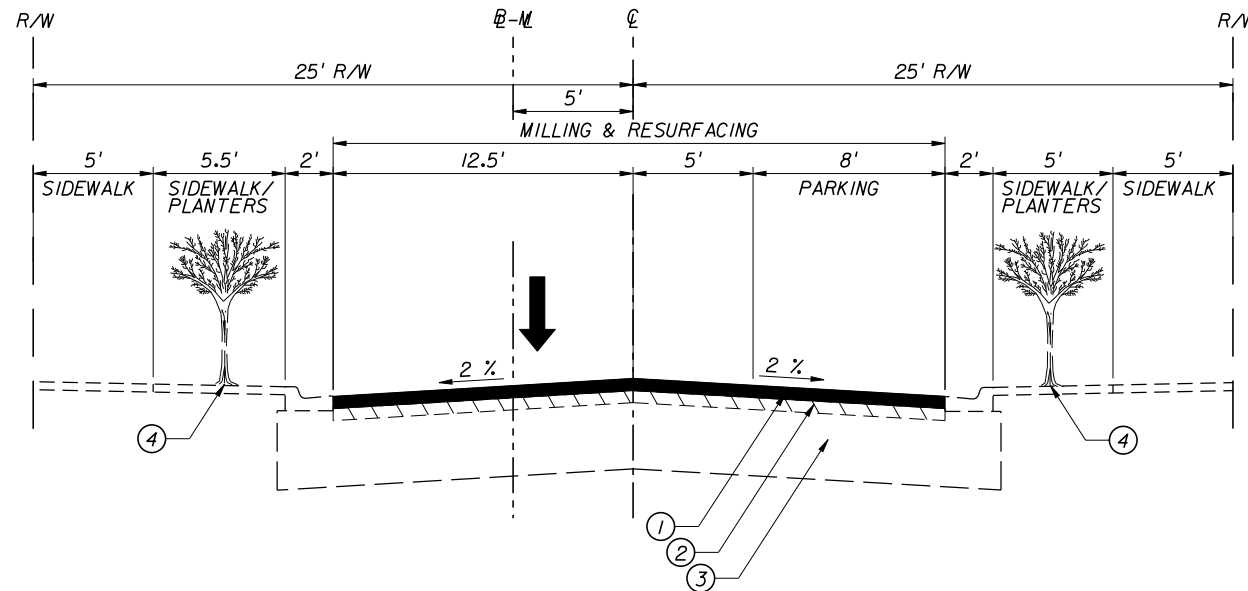
**CITY OF MIAMI**  
MARY BRICKELL VILLAGE  
DRAINAGE AND ROADWAY IMPROVEMENTS - PHASE 1  
SWISE 9th STREET FROM W 1st AVENUE TO E 1st AVENUE (BRICKELL PLAZA)  
SWISE 10th STREET FROM W 1st AVENUE TO E 1st AVENUE (BRICKELL PLAZA)  
SWISE 11th STREET FROM W 1st AVENUE TO SOUTH MIAMI AVENUE  
SW 12th STREET FROM W 1st AVENUE TO SE 1st AVENUE (BRICKELL PLAZA)  
CITY OF MIAMI PROJECT NUMBER: B-30637

TYPICAL SECTION  
S.W./S.E. 10th STREET

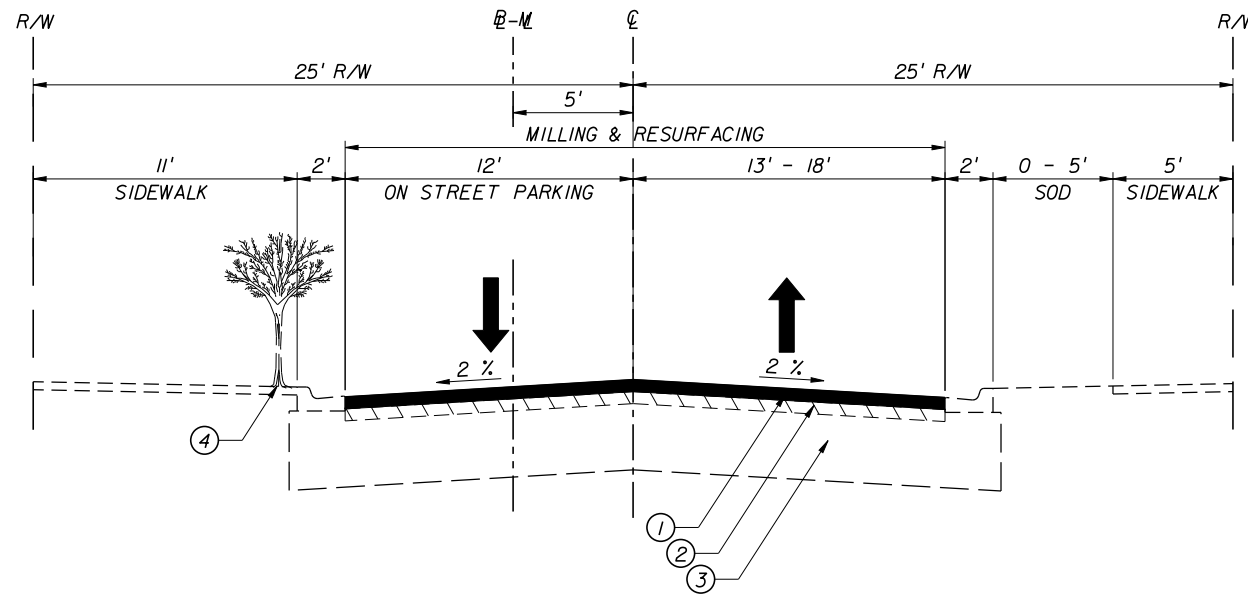
SHEET NO.

5

FOR CONSTRUCTION 100% PLANS



**TYPICAL SECTION S.W. 11th STREET**  
 FROM S.W. 1st AVENUE TO SOUTH MIAMI AVENUE  
 N.T.S.



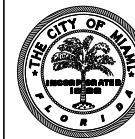
**TYPICAL SECTION S.W. 12th STREET**  
 FROM S.W. 1st AVENUE TO SOUTH MIAMI AVENUE  
 N.T.S.

- ① PROPOSED MILLING & RESURFACING (MILL 1" AND RESURFACING WITH 1" OF SUPERPAVE ASPHALT PER DOT STANDARDS), REFER TO PLANS FOR LIMITS.
- ② EXISTING LIMEROCK BASE (8" MINIMUM THICKNESS)
- ③ EXISTING SUBGRADE.
- ④ REFER TO ROADWAY PLANS FOR PLANTER LOCATIONS



R E V I S I O N S			
DATE	DESCRIPTION	DATE	DESCRIPTION

**T·Y·LIN INTERNATIONAL**  
 201 ALHAMBRA CIRCLE SUITE 900  
 Coral Gables, Florida. 33134  
 Phone: 305 / 567-1888 Fax: 305 / 567-1771



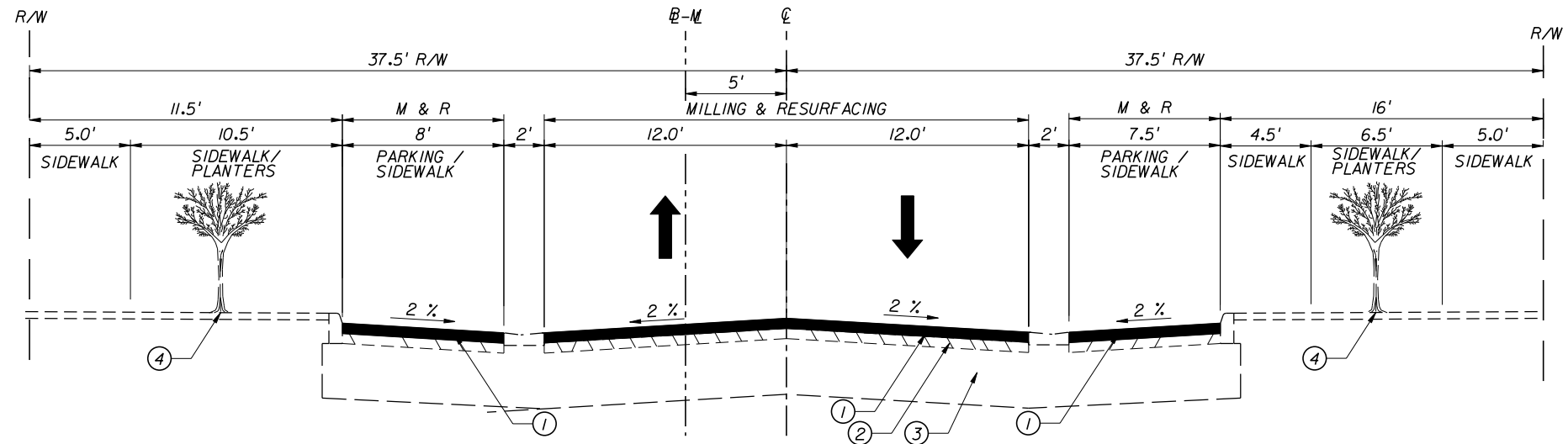
**CITY OF MIAMI**  
 MARY BRICKELL VILLAGE  
 DRAINAGE AND ROADWAY IMPROVEMENTS - PHASE 1  
 SWISE 9th STREET FROM W 1st AVENUE TO E 1st AVENUE (BRICKELL PLAZA)  
 SWISE 10th STREET FROM W 1st AVENUE TO E 1st AVENUE (BRICKELL PLAZA)  
 SWISE 11th STREET FROM W 1st AVENUE TO SOUTH MIAMI AVENUE  
 SW 12th STREET FROM W 1st AVENUE TO SE 1st AVENUE (BRICKELL PLAZA)  
 CITY OF MIAMI PROJECT NUMBER: B-30637

**TYPICAL SECTION**  
**S.W. 11th STREET**  
**& S.W. 12th STREET**

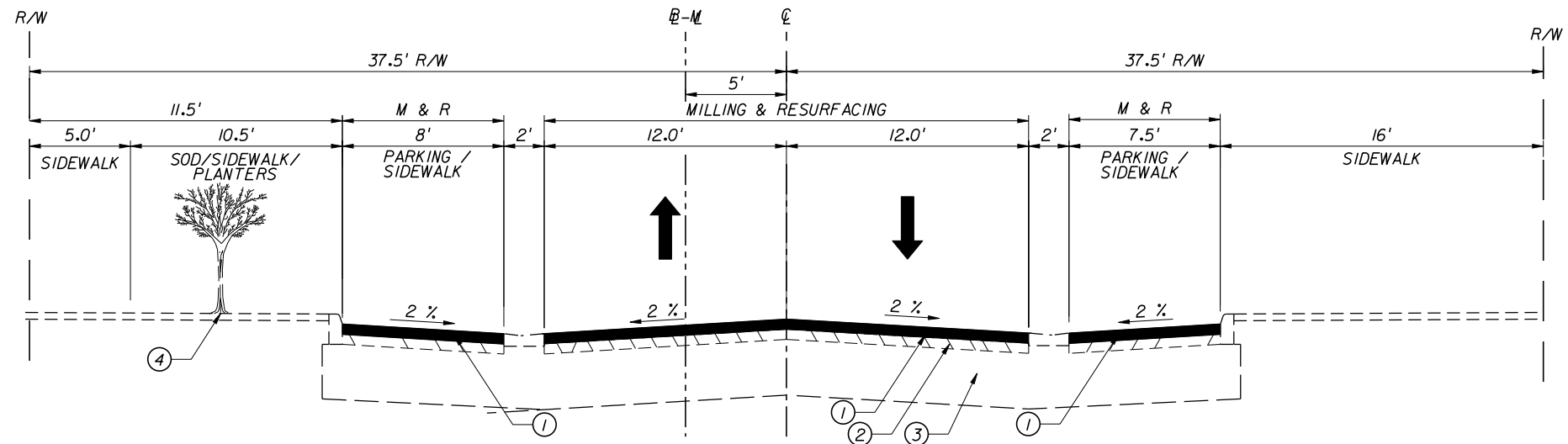
SHEET NO.  
 6

FOR CONSTRUCTION 100% PLANS





**TYPICAL SECTION S.E. 1ST AVENUE**  
 FROM 262.93' RIGHT TO 23' LEFT OF SW 9TH STREET  
 N.T.S.



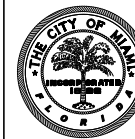
**TYPICAL SECTION S.E. 1ST AVENUE**  
 FROM 59.60' RIGHT TO 65.50' LEFT OF SW 11TH STREET  
 N.T.S.

- ① PROPOSED MILLING & RESURFACING (MILL 1" AND RESURFACING WITH 1" OF SUPERPAVE ASPHALT PER DOT STANDARDS), REFER TO PLANS FOR LIMITS.
- ② EXISTING LIMEROCK BASE (8" MINIMUM THICKNESS)
- ③ EXISTING SUBGRADE.
- ④ EXISTING PLANTER LOCATIONS



R E V I S I O N S			
DATE	DESCRIPTION	DATE	DESCRIPTION

**T·Y·LIN INTERNATIONAL**  
 201 ALHAMBRA CIRCLE SUITE 900  
 Coral Gables, Florida. 33134  
 Phone: 305 / 567-1888 Fax: 305 / 567-1771



**CITY OF MIAMI**  
 MARY BRICKELL VILLAGE  
 DRAINAGE AND ROADWAY IMPROVEMENTS - PHASE 1  
 SWISE 9th STREET FROM W 1st AVENUE TO E 1st AVENUE (BRICKELL PLAZA)  
 SWISE 10th STREET FROM W 1st AVENUE TO E 1st AVENUE (BRICKELL PLAZA)  
 SWISE 11th STREET FROM W 1st AVENUE TO SOUTH MIAMI AVENUE  
 SW 12th STREET FROM W 1st AVENUE TO SE 1st AVENUE (BRICKELL PLAZA)  
 CITY OF MIAMI PROJECT NUMBER: B-30637

**TYPICAL SECTION**  
**S.E. 1st AVENUE**  
**(BRICKELL PLAZA)**

SHEET NO.

7

FOR CONSTRUCTION 100% PLANS

## **APPENDIX C – MISCELLANEOUS CALCULATIONS**

- TABULATION OF PROJECT AREAS
- TABULATION OF SUB-BASIN STORAGE VOLUMES
- CALCULATION OF BOUNDARY CONDITION ELEVATION (NOAA TIDAL DATA)
  - PUMP DISCHARGE OPTIMIZATION CALCULATIONS
  - PUMP SIZING CALCULATIONS AND MODEL SELECTION

BASIN ID	LOWEST GRATE ELEVATION	BASIN AREA (ACRES)	CN	ADDITIONAL AREA DUE TO HIGH RISE BLDGS. (1/2 OF FACE AREA)	TOTAL DRAINAGE AREA (ACRES)	ADJACENT BUILDING DIMENSIONS			
						WIDTH	STORIES	HEIGHT	AREA (Acres)
OFFSITE	N/A	2.96	98	0.00	2.96			0.00	0.00
B-1	3.80	1.10	98	0.00	1.10			0.00	0.00
B-2	3.96	0.50	98	0.75	1.25	250.00	26.00	260.00	1.49
B-3	3.95	0.50	98	0.12	0.62	340.00	3.00	30.00	0.23
B-4	3.12	0.48	98	0.23	0.71	77.00	26.00	260.00	0.46
B-5	3.69	0.67	98	0.29	0.96	425.00	6.00	60.00	0.59
B-6	4.87	0.35	98	0.00	0.35			0.00	0.00
B-7	5.22	0.24	98	0.00	0.24			0.00	0.00
B-8	4.90	0.38	98	0.00	0.38			0.00	0.00
B-9	4.86	0.37	98	0.00	0.37			0.00	0.00
B-10	4.11	0.74	98	0.00	0.74			0.00	0.00
B-11	4.06	0.79	98	0.10	0.89	210.00	4.00	40.00	0.19
B-12	4.15	0.97	98	0.00	0.97			0.00	0.00
B-13	5.87	0.20	98	0.00	0.20			0.00	0.00
B-14	5.70	0.65	98	0.00	0.65			0.00	0.00
B-15	5.66	0.56	98	0.00	0.56			0.00	0.00
B-16	8.13	0.49	98	0.00	0.49			0.00	0.00
B-17	8.15	0.44	98	0.00	0.44			0.00	0.00
B-18	4.03	0.60	98	0.00	0.60			0.00	0.00
B-19	4.37	0.40	98	0.00	0.40			0.00	0.00
B-20	3.67	0.79	98	0.34	1.13	373.00	8.00	80.00	0.69
B-21	3.83	0.69	98	0.43	1.12	250.00	15.00	150.00	0.86
B-22	5.31	1.09	98	0.00	1.09			0.00	0.00
B-23	5.34	0.39	98	0.00	0.39			0.00	0.00
B-24	4.20	0.63	98	0.43	1.06	250.00	15.00	150.00	0.86
B-25	4.20	0.71	98	1.06	1.77	220.00	42.00	420.00	2.12
B-26	9.94	0.36	98	0.00	0.36			0.00	0.00
B-27	5.90	0.69	98	1.06	1.75	220.00	42.00	420.00	2.12
B-28	5.80	0.69	98	0.26	0.95	100.00	23.00	230.00	0.53
TOTAL BASIN AREA (acres):		16.5	TOTAL DRAINAGE AREA (acres):		21.5				
BASIN AREA FOR BMP STRUCTURE CALCULATIONS		13.8							

Surface Storage - Basin Stage (elev. CMD) vs. Storage (acre-ft) (based on Civil 3D DTM)											
Basin ID	Structure Storage	3.5	4	4.5	5	6	7	8	9	10.5	12
B-1	0.0013	-	0.0031	0.0387	0.1734	0.7710	1.5717	2.4696	3.4703	5.0287	6.5871
B-2	0.0014	-	-	0.0200	0.0808	0.2586	0.5060	0.7940	1.1270	1.6521	2.1918
B-3	0.0013	-	0.0014	0.0278	0.1191	0.4511	0.8571	1.3610	1.8650	2.6209	3.3768
B-4	0.0009	0.0013	0.0092	0.0446	0.1445	0.5415	0.9754	1.4128	1.8534	2.5198	3.1921
B-5	0.0012	-	0.0030	0.0429	0.1588	0.5515	1.0384	1.7077	2.3797	3.3877	4.3958
B-6	0.0019	-	-	-	0.0024	0.0311	0.1475	0.3786	0.6798	1.2133	1.7468
B-7	0.0021	-	-	-	-	0.0423	0.2196	0.4621	0.7046	1.0684	1.4322
B-8	0.0019	-	-	-	0.0024	0.0444	0.2148	0.5568	0.9400	1.5148	2.0896
B-9	0.0019	-	-	-	0.0019	0.0762	0.3260	0.6753	1.0444	1.5980	2.1516
B-10	0.0014	-	-	0.0050	0.0546	0.3749	0.9191	1.6202	2.3451	3.4326	4.5200
B-11	0.0014	-	-	0.0084	0.0546	0.3151	0.8961	2.0271	3.4190	5.5068	7.5946
B-12	0.0015	-	-	0.0039	0.0304	0.1711	0.4770	0.9524	1.5624	2.6467	3.7310
B-13	0.0025	-	-	-	-	0.0026	0.0224	0.0686	0.1424	0.3642	0.6021
B-14	0.0024	-	-	-	-	0.0032	0.0515	0.1856	0.4534	1.1248	1.9320
B-15	0.0023	-	-	-	-	0.0033	0.0798	0.3051	0.6773	1.4554	2.2945
B-16	0.0037	-	-	-	-	-	-	-	0.0740	0.5881	1.2283
B-17	0.0038	-	-	-	-	-	-	-	0.0596	0.6260	1.3156
B-18	0.0014	-	-	0.0064	0.0359	0.2829	0.8156	1.3831	1.9506	2.8019	3.6532
B-19	0.0016	-	-	0.0016	0.0073	0.1121	0.3848	0.7395	1.1411	1.7434	2.3458
B-20	0.0012	-	0.0031	0.0347	0.1211	0.4812	1.0491	1.8381	2.6272	3.8107	4.9943
B-21	0.0013	-	0.0016	0.0307	0.1330	0.4696	0.9242	1.4315	2.1144	3.1559	4.1974
B-22	0.0021	-	-	-	-	0.0197	0.1241	0.3267	0.6524	1.3352	2.2350
B-23	0.0021	-	-	-	-	0.0172	0.0886	0.2126	0.3729	0.7495	1.2461
B-24	0.0015	-	-	0.0020	0.0251	0.2376	0.5373	0.8959	1.3047	1.9634	2.8260
B-25	0.0015	-	-	0.0035	0.0453	0.3025	0.6905	1.2048	1.7916	2.7538	3.8005
B-26	0.0048	-	-	-	-	-	-	-	-	0.0099	0.0891
B-27	0.0025	-	-	-	-	0.0222	0.1041	0.3342	0.7004	1.4681	2.3786
B-28	0.0024	-	-	-	-	0.0025	0.0395	0.1565	0.3610	0.8406	1.4000

U.S. DEPARTMENT OF COMMERCE  
National Oceanic and Atmospheric Administration  
National Ocean Service

[Datums Page](#)

Page 1 of 5

<b>Station ID:</b> 8723165	<b>PUBLICATION DATE:</b> 05/07/2003
<b>Name:</b> MIAMI, BISCAYNE BAY FLORIDA	
<b>NOAA Chart:</b> 11468	<b>Latitude:</b> 25° 46.7' N
<b>USGS Quad:</b> MIAMI	<b>Longitude:</b> 80° 11.1' W

To reach the tidal bench marks from the intersection of Biscayne Boulevard and Port Boulevard in Miami, proceed south on Biscayne Boulevard one block to the entrance of Miamarina on the left. The bench marks are located in the vicinity of the marina and the west end of the Port Avenue bridge to the Port of Miami on Dodge Island. The tide gage and staff are located at the NW end of the northernmost pier of the marina.

**T I D A L   B E N C H   M A R K S**

**PRIMARY BENCH MARK STAMPING:** 3165 A 1985  
DESIGNATION: 872 3165 A

MONUMENTATION:	Tidal Station disk	VM#:	5770
AGENCY:	National Ocean Service (NOS)	PID:	
SETTING CLASSIFICATION:	Concrete wall		

The primary bench mark is a disk set flush in the center of a 1 m (3 ft) wide concrete wall around the parking lot, near the SE end of the northernmost pier of Miamarina, 145 m (475 ft) NNE of the inside corner of the seawall at the north side of the marina restaurant, 43 m (140 ft) west of the east face of the concrete wall on the east side of Miamarina (on the Intracoastal Waterway), 30 m (97 ft) north along the top of the concrete wall from the north end of the Dockmaster building, 23 m (77 ft) south of the NE corner of the concrete marina dock, 1 m (3 ft) above dock level, and 0.24 m (0.8 ft) above the level of the parking lot.

**BENCH MARK STAMPING:** MH 16 1962  
DESIGNATION: MH 16  
ALIAS: 872 3165 TIDAL USE

MONUMENTATION:	Survey disk	VM#:	5767
AGENCY:	US Army Corps of Engineers (USE)	PID#:	<u>AC2177</u>
SETTING CLASSIFICATION:	Concrete bulkhead		

The bench mark is a disk set flush in the top of a concrete bulkhead near its SE corner on the north side of Miamarina, near the west end of the Port Boulevard bridge leading to the Port of Miami, 10 m (33 ft) south of the south edge of the bridge, 1.83 m (6.0 ft) west of the east end of the bulkhead, and 0.64 m (2.1 ft) north of the south face of the bulkhead.



U.S. DEPARTMENT OF COMMERCE  
National Oceanic and Atmospheric Administration  
National Ocean Service

Page 2 of 5

Station ID: 8723165  
Name: MIAMI, BISCAYNE BAY  
FLORIDA  
NOAA Chart: 11468  
USGS Quad: MIAMI

PUBLICATION DATE: 05/07/2003  
Latitude: 25° 46.7' N  
Longitude: 80° 11.1' W

T I D A L B E N C H M A R K S

**BENCH MARK STAMPING: MH 16 RM 1 1962**  
DESIGNATION: MH 16 RM 1  
ALIAS: 872 3165 TIDAL USE

MONUMENTATION: Survey disk VM#: 5768  
AGENCY: US Army Corps of Engineers (USE) [PID#: AC2178](#)  
SETTING CLASSIFICATION: Concrete bulkhead

The bench mark is a disk set flush in the top of a concrete bulkhead on the north side of Miamarina, 17.37 m (57.0 ft) west of the east end of the bulkhead, 16 m (51 ft) west of bench mark MH 16 1962, 10 m (32 ft) south of the SW corner of the Port Boulevard bridge, and 0.64 m (2.1 ft) north of the south face of the bulkhead.

**BENCH MARK STAMPING: MH 16 RM 2 1962**  
DESIGNATION: MH 16 RM 2  
ALIAS: 872 3165 TIDAL USE

MONUMENTATION: Survey disk VM#: 5769  
AGENCY: US Army Corps of Engineers (USE) [PID#: AC2179](#)  
SETTING CLASSIFICATION: Concrete bulkhead

The bench mark is a disk set flush in the top of a concrete bulkhead near the west end of the Port Boulevard bridge leading to the Port of Miami, 27 m (87 ft) north of bench mark MH 16 1962, and 6 m (20 ft) south of the north end of the bulkhead.





U.S. DEPARTMENT OF COMMERCE

**MLLW NGVD Calculation:**

Bench Mark Stamping: MIAMI EL. 15.491  
Per PID# AC2183,  
stamping located at elevation of 4.636m NGVD (15.21' NGVD)

Bench Mark Stamping: MIAMI EL. 15.491 is located 4.804m above MLLW,  
Therefore MLLW elevation = -0.168m NGVD (-0.551' NGVD) or  
**-0.27' MIAMI Datum**

**MHHW Calculation for Modeling:**

MHHW= 0.723m above MLLW

MHHW= 0.555m NGVD = 1.82' NGVD = **2.10' MIAMI Datum**

**MHHW Check:**

NAVD 88 = 0.643m above MLLW

MHHW= 0.723m above MLLW

so

MHHW= 0.08m NAVD

convert to NGVD:

MHHW= 0.553m NGVD = 1.81' NGVD = **2.07' MIAMI Datum**

**Highest Observed Water Level:**

NAVD 88 = 0.643m above MLLW

HOWL= 1.103m above MLLW

so

HOWL= 0.46m NAVD

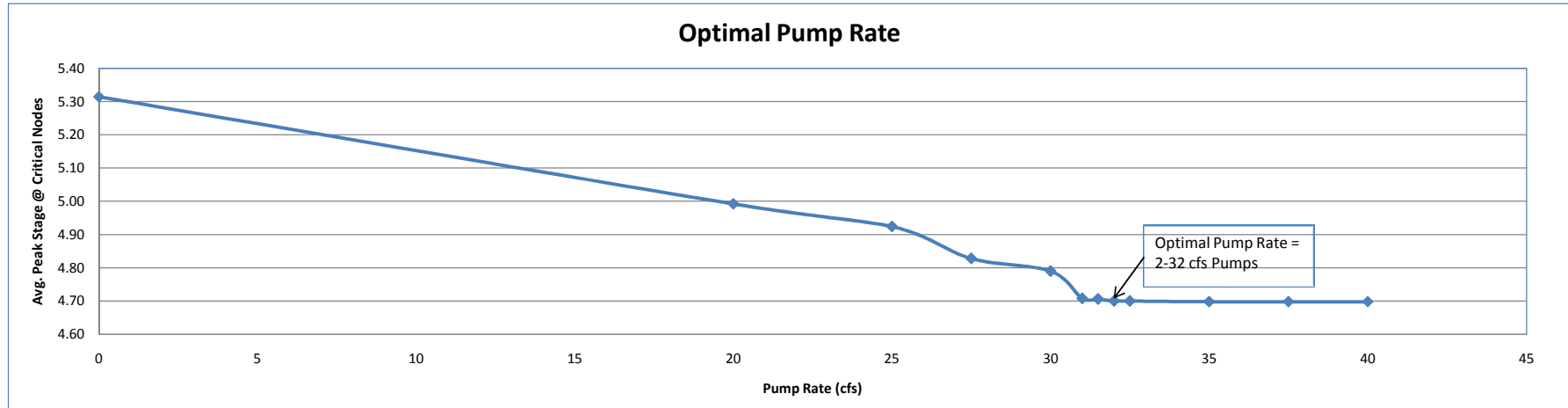
convert to NGVD:

MHHW= 0.933m NGVD = 3.06' NGVD= **3.32' MIAMI Datum**





Critical Basins	10yr-24hr Peak Stage Elevation											
	Exist. Gravity	Variable Pump Rate (cfs per pump, station will be duplex)										
	0	20	25	27.5	30	31	31.5	32	32.5	35	37.5	40
B-10	5.45	5.04	4.97	4.87	4.83	4.75	4.74	4.74	4.74	4.74	4.74	4.74
B-11	5.47	5.05	4.98	4.89	4.85	4.77	4.77	4.76	4.76	4.76	4.76	4.76
B-12	5.57	5.11	5.04	4.95	4.92	4.84	4.85	4.85	4.85	4.84	4.84	4.84
B-20	5.04	4.88	4.81	4.71	4.67	4.58	4.58	4.57	4.57	4.57	4.57	4.57
B-21	5.04	4.88	4.82	4.72	4.68	4.60	4.59	4.58	4.58	4.58	4.58	4.58
<b>Average Stage</b>	<b>5.31</b>	<b>4.99</b>	<b>4.92</b>	<b>4.83</b>	<b>4.79</b>	<b>4.71</b>	<b>4.71</b>	<b>4.70</b>	<b>4.70</b>	<b>4.70</b>	<b>4.70</b>	<b>4.70</b>





**BRICKELL 13th STREET  
STORM WATER PUMP  
STATION DESIGN**

**Head Loss Calculations (Based on Hazen-Williams Equation)**

**System Curves:**

24" Discharge				48" Force Main			
Pump Flow gpm	Friction Head	Velocity fps	Velocity Head	Total Flow gpm	Friction Head	Velocity fps	Velocity Head
0	0.00	0.0	0.00	0	0.00	0.0	0.00
5000	0.84	3.3	0.17	10000	0.05	1.6	0.04
6000	1.17	3.9	0.24	12000	0.07	2.0	0.06
7000	1.56	4.6	0.33	14000	0.09	2.3	0.08
8000	2.00	5.3	0.43	16000	0.11	2.6	0.11
9000	2.48	5.9	0.54	18000	0.14	3.0	0.14
10000	3.02	6.6	0.67	20000	0.17	3.3	0.17
11000	3.60	7.2	0.81	22000	0.20	3.6	0.20
12342	4.46	8.1	1.02	24684	0.25	4.1	0.26
13000	4.91	8.6	1.14	26000	0.28	4.3	0.28
14568	6.06	9.6	1.43	29136	0.34	4.8	0.36
15000	6.39	9.9	1.51	30000	0.36	4.9	0.38
16000	7.21	10.5	1.72	32000	0.41	5.3	0.43
17000	8.06	11.2	1.94	34000	0.46	5.6	0.48
18000	8.96	11.8	2.18	36000	0.51	5.9	0.54
19000	9.91	12.5	2.43	38000	0.56	6.2	0.61
20000	10.89	13.2	2.69	40000	0.62	6.6	0.67

60"x36" (52" equiv. round) Gravity Main				Total Dynamic Head			
Total Flow gpm	Friction Head	Velocity fps	Velocity Head	Pump Flow gpm	Max. T.D.H. feet	Min. T.D.H. feet	Avg. T.D.H. feet
0	0.00	0.0	0.00	0	13.8	1.0	7.4
10000	0.22	1.5	0.03	5000	15.1	2.3	8.7
12000	0.31	1.8	0.05	6000	15.7	2.9	9.3
14000	0.41	2.1	0.07	7000	16.3	3.5	9.9
16000	0.53	2.4	0.09	8000	17.1	4.3	10.7
18000	0.66	2.7	0.11	9000	17.9	5.1	11.5
20000	0.80	3.0	0.14	10000	18.8	6.0	12.4
22000	0.95	3.3	0.17	11000	19.7	6.9	13.3
24684	1.18	3.7	0.21	12342	21.2	8.4	14.8
26000	1.30	3.9	0.23	13000	21.9	9.1	15.5
29136	1.60	4.3	0.29	14568	23.9	11.1	17.5
30000	1.69	4.5	0.31	15000	24.4	11.6	18.0
32000	1.91	4.8	0.35	16000	25.8	13.0	19.4
34000	2.13	5.1	0.40	17000	27.3	14.5	20.9
36000	2.37	5.3	0.44	18000	28.8	16.0	22.4
38000	2.62	5.6	0.49	19000	30.4	17.6	24.0
40000	2.88	5.9	0.55	20000	32.1	19.3	25.7

**BRICKELL 13th STREET  
 STORM WATER PUMP  
 STATION DESIGN**

	Operating Points		
	Maximum	Minimum	Average
Pump Rate, gpm	14361.6	14361.6	14361.6
T.D.H., feet	23.9	11.1	17.5

**Basis of Design Pump Curve:**

Based on Manufacturer Recommendations:

Peak Flow (1 pump): 9119 gpm

FROM PUMP CURVE

TDH (both pumps on, max.): 27.2'

Manufacturer: Flygt  
 Model: CP 3531/735  
 Curve No. : C3531-63-1440  
 Motor: 43-44-14AA  
 Imp. Diameter: 615 mm  
 Discharge: 19.5  
 Motor Horsepower: 90  
 Motor Speed: 500 rpm  
 Voltage: 460  
 Cycle: 60 Hz  
 Phase: 3  
 Curve date: 2-12-2009

Pump Curve		
Flow cfs	Flow gpm	Total Head
35.7	16000	0.0
29.9	13411	12.9
29.3	13142	14.0
28.7	12897	15.0
27.3	12264	17.5
25.8	11594	20.0
24.2	10867	22.5
22.5	10084	25.0
20.6	9226	27.5
18.5	8322	30.0
16.4	7382	32.5
14.3	6421	35.0
12.1	5451	37.5
10.0	4477	40.0
7.8	3497	42.5
5.6	2495	45.0
3.3	1459	47.5
0.8	380	50.0
0.0	0.0	51.2

**Net Positive Suction Head Check**

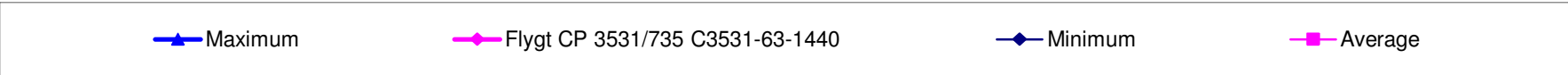
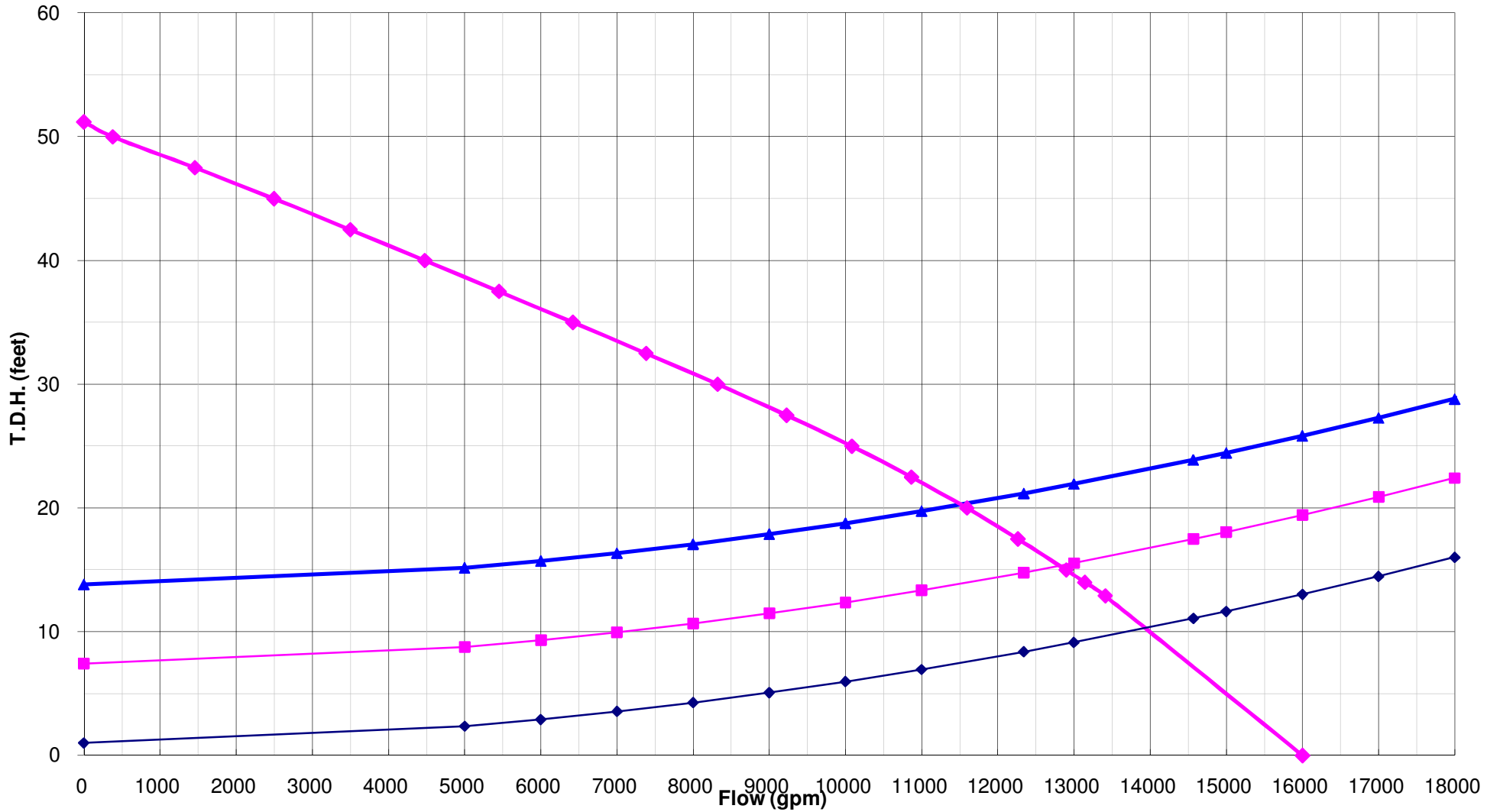
$$NPSH_{available} = h_{atm} + h_{z(suction)} + h_{f(suction)} + h_{vp}$$

$h_{atm}$ (atmospheric pressure)	33.9'
$h_z$ (head on suction side)	2.0' (distance from low water level to pump suction inlet)
$h_f$ (friction loss on suction pipe)	0.0' (no pipe on suction side)
$h_{vp}$ (vapor pressure of water at 70 deg.F)	1.2'

$NPSH_{required}$  = (refer to manufacturer pump curve for  $NPSH_{required}$ )

$NPSH_{available}$  = 37.07 **ok**

### SYSTEM CURVES vs. PUMP PERFORMANCE CURVE



## **APPENDIX D – WATER QUALITY CALCULATIONS**

- EXFILTRATION TRENCH CALCULATIONS
- WATER QUALITY TREATMENT CALCULATIONS FOR BMP



**CITY OF MIAMI CAPITAL IMPROVEMENTS PROGRAM**  
**MARY BRICKELL VILLAGE DRAINAGE IMPROVEMENTS**  
**WATER QUALITY CALCULATIONS**  
**EXISTING BASIN B-16 and B-17**

Prepared by: FA

**Volumetric Retention Treatment Required:**

Impervious Area=	<b>0.93</b> ac.
Pervious Area=	<b>0.00</b> ac.
<b>Total Area=</b>	<b>0.93 ac.</b>

**SFWMD CRITERIA:**

- a) First inch of runoff from the developed project:  
 ( 1 In x = D.A. Ac. x 1 Ft/12 In ) = **0.078 Ac.-Ft.**
- b) 2.5 inches times the percentage of imperviousness:  
 Percent Impervious = **100%**  
 ( 2.5 In x % Impervious ) = **2.50** in. to be treated  
 Volume required to be treated = ( in. to be treated x D.A. Ac x 1 Ft/12 In ) = **0.194 Ac.-Ft.**

**DERM CRITERIA:**

$$t_{1"} = \frac{2940 \times F^{-0.11}}{308.5 \times C - 60.5 ( 0.5895 + F^{-0.67} )}$$

WHERE:

- $t_{1"}$  = time to generate 1" of runoff, in minutes  
 F = **5** Frequency in years, DCPW Manual, Part II, Section D4-Water Control, Table I  
 Cwtd = **0.90** weighted runoff coefficient ( from the rational formula )  
 Tc = **10** time of concentration, in minutes

**CONTRIBUTING AREA AND ROUGHNESS COEFFICIENT CRITERIA.**

Pervious Areas = 0.00 Ac.,  $C_{PERV} = 0.2$

Imperv. Areas = 0.93 Ac.,  $C_{IMP} = 0.9$

$C = (A_{IMP} \times C_{IMP} + A_{PERV} \times C_{PERV}) / A_T = 0.90$

$t_{1"} = 11.1$  MIN.

TOTAL TIME OF CONCENTRATION ( $T_T$ ) :  $T_T = t_{1"} + T_C = 21.12$  MIN.

**STORM INTENSITY ( Dade County Rainfall Intensity-Duration-Frequency Curves)**

$$i = \frac{308.5}{48.6 \times F^{-0.11} + T_T ( 0.5895 + F^{-0.67} )} = 5.11 \text{ IN/HR.}$$

RUNOFF FLOW  $Q_{1"} = C \times I \times A_T = 4.28$  CFS FOR THE 1<sup>ST</sup> INCH OF RUNOFF

**TOTAL RUNOFF VOLUME TO BE TREATED  $V_{1"}$  (FOR 1 INCH):**

$V_{1"} = 60 Q_{1"} T_T = 5,423$  CF = **0.124** Ac.-Ft.

**Volume Treatment Required= 0.194 ac-ft.**

**Volume Provided by exfiltrator trench System (following SFWMD Exfiltration Trench Equation Derivation):**

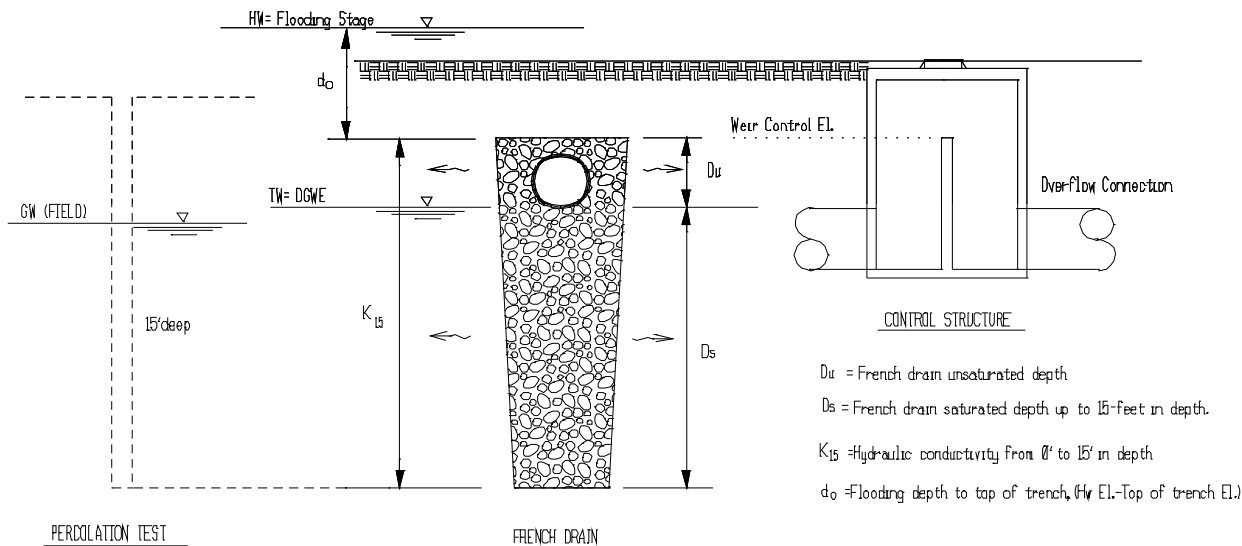
**EXFILTRATION TRENCH BASIN**

**Volume Storage in Exfiltrator Trench:**

WE=	8.00	(Lowest Ground Elev. or Control Weir Elev., ft., NGVD)
GW=	2.00	(DERM October Average Groundwater Level, ft., NGVD)
WDTH=	4	(Exfiltrator Trench width, ft.)
TOP EL.=	6.50	(Exfiltrator Trench Top Elev., ft., NGVD)
BOT. EL.=	-7.00	(Exfiltrator Trench Botom Elev., ft., NGVD)
d=	2.00	(Exfiltrator Trench Pipe diameter, ft.)
INV. EL.=	3.00	(Exfiltrator Trench Pipe Invert Elev., ft., NGVD)
d <sub>enc.</sub> =	-1.00	(pipe encroachment below GW, (GW-INV. EL), ft.)
V <sub>pipe</sub> =	3.14	ft <sup>3</sup> /ft
V <sub>trench</sub> =	4.17	ft <sup>3</sup> /ft (assume 20% voids for 15 years in service)
V <sub>dry</sub> =V <sub>pipe</sub> +V <sub>trench</sub> =	7.31	ft <sup>3</sup> /ft

**Volume Exfiltrated through Exfiltrator Trench:**

V <sub>SIDE-EXF.</sub> =	(KS1H1+KS2H2) 3600
V <sub>SIDE-EXF.</sub> =	Volume exfiltrated out a side in 1-hour (ft3/ft)
S <sub>1</sub> =	Unsaturated trench surfac (ft <sup>2</sup> )
S <sub>2</sub> =	Saturated trench surface (ft <sup>2</sup> )
H <sub>1</sub> =	Average head on unsaturated surface (ft. head)
H <sub>2</sub> =	Head on saturated surface (ft. head)



**$V_{SIDE-EXF.(2-sides)} = 2*(K*S_1*H_1+K*S_2*H_2) 3600 = 2*(K_{15}*D_u*(D_u/2+D_s))*3600 = E*3600$**

K <sub>15-avg.</sub> =	5.00E-04 cfs/ft <sup>2</sup> -ft	D <sub>u</sub> =	4.5 ft.
		D <sub>s</sub> =	9.00 ft.

E= 5.06E-02 cfs/ft (Using directly perc. test results and SFWMD F.D. Eq.)

E\*3600= 182 ft<sup>3</sup>/ft = V<sub>ext.</sub>

**Treatment Unit Volume provided by Exfiltration Trench:**

$$V_{\text{dry}} = 7.31 \text{ ft}^3/\text{ft}$$

$$V_{\text{exf.}} = 182 \text{ ft}^3/\text{ft}$$

$$V_{\text{FD-Unit}} = V_{\text{dry}} + V_{\text{side-exf.}} = 190 \text{ ft}^3/\text{ft} = 0.0044 \text{ ac-ft/ft} = 0.0522 \text{ ac-in/ft}$$

**Existing FD Length= 100 ft**

**Treatment Volume provided by Exfiltration Trench:**

$$V_{\text{FD}} = V_{\text{FD-Unit}} \times L_{\text{FD}} = 18,956 \text{ ft}^3 = 0.435 \text{ ac-ft.} = 5 \text{ ac-in}$$

<b>V<sub>provided</sub>=</b>	<b>0.435 ac-ft</b>
<b>V<sub>required</sub>=</b>	<b>0.194 ac-ft</b>

**Factor of Safety = 2.2 >>>> Water Quality Criteria is met.**

**CITY OF MIAMI CAPITAL IMPROVEMENTS PROGRAM**  
**MARY BRICKELL VILLAGE DRAINAGE IMPROVEMENTS**  
**WATER QUALITY CALCULATIONS**  
**EXISTING BASIN B-27 and B-28**

Prepared by: FA

**Volumetric Retention Treatment Required:**

Impervious Area=	<b>1.38</b> ac.
Pervious Area=	<b>0.00</b> ac.
<b>Total Area=</b>	<b>1.38 ac.</b>

**SFWMD CRITERIA:**

- a) First inch of runoff from the developed project:  
 ( 1 In x = D.A. Ac. x 1 Ft/12 In ) = **0.115 Ac.-Ft.**
- b) 2.5 inches times the percentage of imperviousness:  
 Percent Impervious = **100%**  
 ( 2.5 In x % Impervious ) = **2.50** in. to be treated  
 Volume required to be treated = ( in. to be treated x D.A. Ac x 1 Ft/12 In ) = **0.288 Ac.-Ft.**

**DERM CRITERIA:**

$$t_{1"} = \frac{2940 \times F^{-0.11}}{308.5 \times C - 60.5 ( 0.5895 + F^{-0.67} )}$$

WHERE:

- $t_{1"}$  = time to generate 1" of runoff, in minutes  
 F = **5** Frequency in years, DCPW Manual, Part II, Section D4-Water Control, Table I  
 Cwtd = **0.90** weighted runoff coefficient ( from the rational formula )  
 Tc = **10** time of concentration, in minutes

**CONTRIBUTING AREA AND ROUGHNESS COEFFICIENT CRITERIA.**

Pervious Areas = 0.00 Ac.,  $C_{PERV} = 0.2$

Imperv. Areas = 1.38 Ac.,  $C_{IMP} = 0.9$

$C = (A_{IMP} \times C_{IMP} + A_{PERV} \times C_{PERV}) / A_T = 0.90$

$t_{1"} = 11.1$  MIN.

**TOTAL TIME OF CONCENTRATION ( $T_T$ ):**  $T_T = t_{1"} + T_C = 21.12$  MIN.

**STORM INTENSITY ( Dade County Rainfall Intensity-Duration-Frequency Curves)**

$$i = \frac{308.5}{48.6 \times F^{-0.11} + T_T ( 0.5895 + F^{-0.67} )} = 5.11 \text{ IN/HR.}$$

**RUNOFF FLOW**  $Q_{1"} = C \times I \times A_T = 6.35$  CFS **FOR THE 1<sup>ST</sup> INCH OF RUNOFF**

**TOTAL RUNOFF VOLUME TO BE TREATED  $V_{1"}$  (FOR 1 INCH):**

$V_{1"} = 60 Q_{1"} T_T = 8,047$  CF = **0.185** Ac.-Ft.

**Volume Treatment Required= 0.288 ac-ft.**

**Volume Provided by exfiltrator trench System (following SFWMD Exfiltration Trench Equation Derivation):**

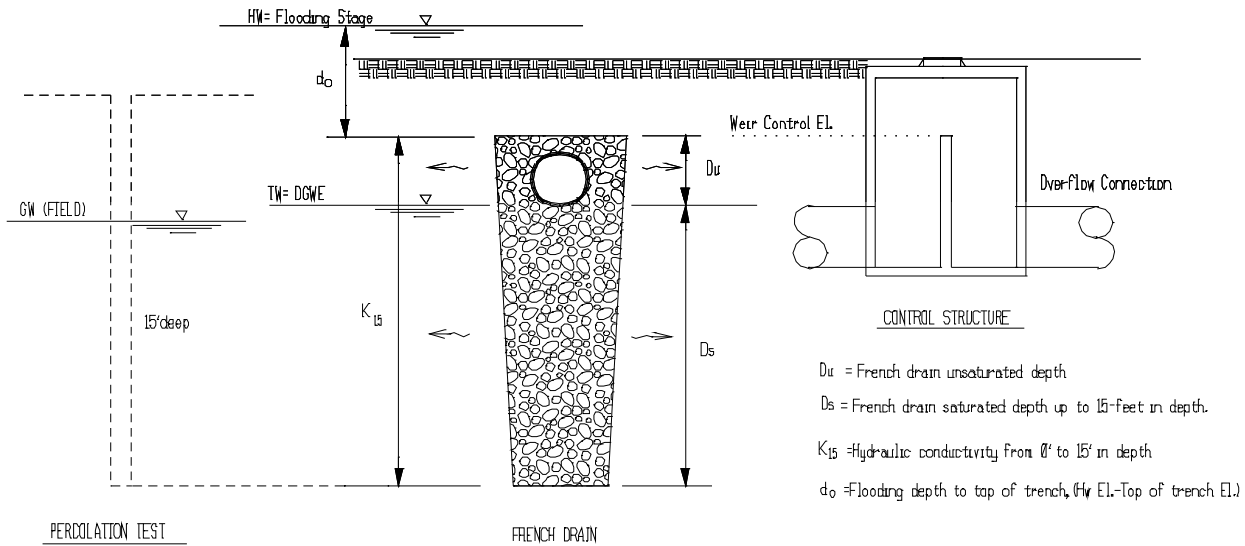
**EXFILTRATION TRENCH BASIN**

**Volume Storage in Exfiltrator Trench:**

WE=	7.00	(Lowest Ground Elev. or Control Weir Elev., ft., NGVD)
GW=	2.00	(DERM October Average Groundwater Level, ft., NGVD)
WDTH=	4	(Exfiltrator Trench width, ft.)
TOP EL.=	5.50	(Exfiltrator Trench Top Elev., ft., NGVD)
BOT. EL.=	-8.00	(Exfiltrator Trench Botom Elev., ft., NGVD)
d=	2.00	(Exfiltrator Trench Pipe diameter, ft.)
INV. EL.=	2.50	(Exfiltrator Trench Pipe Invert Elev., ft., NGVD)
d <sub>enc.</sub> =	-0.50	(pipe encroachment below GW, (GW-INV. EL), ft.)
V <sub>pipe</sub> =	3.14	ft <sup>3</sup> /ft
V <sub>trench</sub> =	3.37	ft <sup>3</sup> /ft (assume 20% voids for 15 years in service)
V <sub>dry</sub> =V <sub>pipe</sub> +V <sub>trench</sub> =	6.51	ft <sup>3</sup> /ft

**Volume Exfiltrated through Exfiltrator Trench:**

V <sub>SIDE-EXF.</sub> =	(KS1H1+KS2H2) 3600
V <sub>SIDE-EXF.</sub> =	Volume exfiltrated out a side in 1-hour (ft3/ft)
S <sub>1</sub> =	Unsaturated trench surfaec (ft <sup>2</sup> )
S <sub>2</sub> =	Saturated trench surface (ft <sup>2</sup> )
H <sub>1</sub> =	Average head on unsaturated surface (ft. head)
H <sub>2</sub> =	Head on saturated surface (ft. head)



**$V_{\text{SIDE-EXF. (2-sides)}} = 2*(K*S_1*H_1+K*S_2*H_2) 3600 = 2*(K_{15}*D_u*(D_u/2+D_s))*3600 = E*3600$**

K <sub>15-avg.</sub> =	5.00E-04 cfs/ft <sup>2</sup> -ft	D <sub>u</sub> =	3.5 ft.
		D <sub>s</sub> =	10.00 ft.

E= 4.11E-02 cfs/ft (Using directly perc. test results and SFWMD F.D. Eq.)

E\*3600= 148 ft<sup>3</sup>/ft = V<sub>ext.</sub>

**Treatment Unit Volume provided by Exfiltration Trench:**

$$V_{\text{dry}} = 6.51 \text{ ft}^3/\text{ft}$$

$$V_{\text{exf.}} = 148 \text{ ft}^3/\text{ft}$$

$$V_{\text{FD-Unit}} = V_{\text{dry}} + V_{\text{side-exf.}} = 155 \text{ ft}^3/\text{ft} = 0.0035 \text{ ac-ft/ft} = 0.0426 \text{ ac-in/ft}$$

**Existing FD Length= 200 ft**

**Treatment Volume provided by Exfiltration Trench:**

$$V_{\text{FD}} = V_{\text{FD-Unit}} \times L_{\text{FD}} = 30,913 \text{ ft}^3 = 0.710 \text{ ac-ft.} = 9 \text{ ac-in}$$

<b>V<sub>provided</sub>=</b>	<b>0.710 ac-ft</b>
<b>V<sub>required</sub>=</b>	<b>0.288 ac-ft</b>

**Factor of Safety = 2.5 >>>> Water Quality Criteria is met.**



**Post-Development Drainage Conditions**  
**Mary Brickell Village Drainage Improvements**  
**WATER QUALITY CALCULATIONS**

Prepared by: FA

**Volumetric Retention Treatment Required:**

Impervious Area=	13.80 ac.
Pervious Area=	0.00 ac.
<b>Total Area=</b>	<b>13.80 ac.</b>

**SFWMD CRITERIA:**

- a) First inch of runoff from the developed project:  
 ( 1 In x 9.95 Ac. x 1 Ft/12 In ) = 1.15 Ac.-Ft.
- b) 2.5 inches times the percentage of imperviousness:  
 Percent Impervious = 100%  
 ( 2.5 In x 1.00 ) = 2.50 in. to be treated  
 Volume required to be treated = ( 2.5 In x 9.95 Ac x 1 Ft/12 In ) = 2.88 Ac.-Ft.

**DERM CRITERIA:**

$$t_{1"} = \frac{2940 \times F^{-0.11}}{308.5 \times C - 60.5 ( 0.5895 + F^{-0.67} )}$$

WHERE:

- $t_{1"}$  = time to generate 1" of runoff, in minutes  
 F = 5 frequency in years, DCPW Manual, Part II, Section D4-Water Control, Table I  
 Cwd = 0.90 weighted runoff coefficient ( from the rational formula )  
 Tc = 166 time of concentration, in minutes

**CONTRIBUTING AREA AND ROUGHNESS COEFFICIENT CRITERIA.**

Pervious Areas = 0.00 Ac.,  $C_{PERV}$  = 0.2  
 Imperv. Areas = 13.80 Ac.,  $C_{IMP}$  = 0.9

$$C = (A_{IMP} \times C_{IMP} + A_{PERV} \times C_{PERV}) / A_T = 0.90$$

$t_{1"}$  = 11.12 MIN.

**TOTAL TIME OF CONCENTRATION ( $T_T$ ):**  $T_T = t_{1"} + T_C = 177.12$  MIN.

**STORM INTENSITY ( Dade County Rainfall Intensity-Duration-Frequency Curves)**

$$i = \frac{308.5}{48.6 \times F^{-0.11} + T_T ( 0.5895 + F^{-0.67} )} = 1.50 \text{ IN/HR.}$$

**RUNOFF FLOW**  $Q_{1"} = C \times I \times A_T = 18.66$  CFS **FOR THE 1<sup>ST</sup> INCH OF RUNOFF**

**TOTAL RUNOFF VOLUME TO BE TREATED  $V_{1"}$  (FOR 1 INCH):**

$V_{1"} = 60 Q_{1"} T_T = 198,265$  CF = 4.55 Ac.-Ft.

**Volume Treatment Required= 4.55 ac-ft.**

**Post-Development Drainage Conditions**  
**Mary Brickell Village Drainage Improvements**  
**WATER QUALITY CALCULATIONS**

Prepared by: FA

**Peak Treatment Flow:** 18.66 CFS  
**Downstream Defender Size Required:** 10 Feet, Dia.

(From Hydro International supplied design chart)



**Downstream Defender® Design Chart**

Model Number	Peak Treatment Flow (cfs)	Maximum Inlet Pipe Diameter (inches)	Maximum Outlet Pipe Diameter (inches)	Headloss at Peak Treatment Flow (inches)	Continuous Oil Storage Capacity (gallons)	Spill Containment Capacity (gallons)	Sediment Storage Capacity (cubic yards)	Unit Diameter (feet)
4-FT	3.0	12	12	5	70	188	0.70	4
6-FT	8.0	18	18	8	230	634	2.10	6
8-FT	15.0	24	24	8	525	1,504	4.65	8
10-FT	25.0	30	30	10	1,050	2,937	8.70	10

**NOTES:**

1. Peak Treatment Flow rate is based on keeping headloss at a minimum and removal efficiencies within a desirable range. Higher flow rates are possible if lower removal efficiencies and higher headlosses are acceptable.
2. Headloss is defined as the difference between the top water level upstream and the top water level downstream of the unit.
  - AutoCAD drawings and Microsoft Word specifications available on disk.
  - For pricing, delivery, and custom design, please call Hydro International's Contracts Department.

Hydro International • 94 Hutchins Drive • Portland, ME 04102  
 Tel: (207) 756-6200 • Fax: (207) 756-6212 • E-mail: hiltech@hil-tech.com

[www.hydro-international.biz](http://www.hydro-international.biz)

**Head Losses through Downstream Defender System**

Head Loss Calculations (Based on Hazen-Williams Equation)

$H_f = 0.002083 \times L(100/C)^{1.85} (Q^{1.85}/d^{4.8655})$	
Incoming Pipe Diameter(in.)=	30
In/Out Pipe Lengths(ft)=	10
Resistance Coef. (c)=	120
flow(gpm)=	8372.78
$h_f$ (friction loss,ft)=	0.01748
$h_{sd}$ (head loss through unit, from chart)	0.83330
<b><math>h_{Total}</math> through system</b>	<b>0.85</b>
Influent Pipe Invert	-0.70
Weir Elevation	2.65

C=0.453 english

**TR-55 Time of Concentration Calculations for Water Quality Calculations**  
**Post-Development Drainage Conditions**  
**Mary Brickell Village Drainage Project**

**Sheet Flow (flow length less than 100ft)**

Segment ID	Surface Description (table 3-1)	Manning's Roughness Coefficient, n (table 3-1)	Flow Length, L (ft)	2-yr 24-hr rainfall, P <sub>2</sub> (in)	Furthest Point Elev. (ft.)	Discharge Point Elev. (ft.)	Slope, s (ft/ft)	T <sub>1</sub> = [0.007(nL) <sup>0.8</sup> ] / [P <sub>2</sub> <sup>0.5</sup> s <sup>0.4</sup> ]
1	Smooth (asphalt)	0.011	100	6.00	8.50	7.50	0.0100	0.02
<i>Total Sheet Flow Time of Concentration:</i>								0.02 hours

**Shallow Concentrated Flow**

Segment ID	Surface Description (paved or unpaved)	Flow Length, L (ft)	Furthest Point Elev. (ft.)	Discharge Point Elev. (ft.)	Watercourse Slope, s (ft/ft)	Average Velocity, V (ft/s) (figure 3-1)	T <sub>1</sub> = L / (3600V)
1	paved	250	7.50	5.50	0.0080	2	0.03
<i>Total Shallow Concentrated Flow Time of Concentration:</i>							0.03 hours

**Channel/Pipe Flow**

Segment ID	C.S. flow area, a	Wetted Perimeter, p <sub>w</sub>	Hydraulic Radius, r=a/p <sub>w</sub>	Channel Slope, s	Manning's Roughness Coefficient, n	V(ft/s) = 1.49r <sup>2/3</sup> s <sup>1/2</sup> / n	Channel Length, L	T <sub>1</sub> = L / (3600V)
23"X14"	2.24	6.17	0.363	0.005	0.012	0.158	78	0.137
30"X19"	3.96	8.17	0.485	0.005	0.012	0.192	381	0.553
36"X24"	6.00	10.00	0.600	0.005	0.012	0.221	877	1.103
54"X30"	11.25	14.00	0.804	0.005	0.012	0.268	167	0.173
60"X36"	15.00	16.00	0.938	0.005	0.012	0.297	810	0.757
<i>Total Shallow Concentrated Flow Time of Concentration:</i>								2.72 hours

**Watershed Total Time of Concentration: 2.78 hours**

**Watershed Total Time of Concentration: 166.61 min**

**Table 3-1** Roughness coefficients (Manning's n) for sheet flow

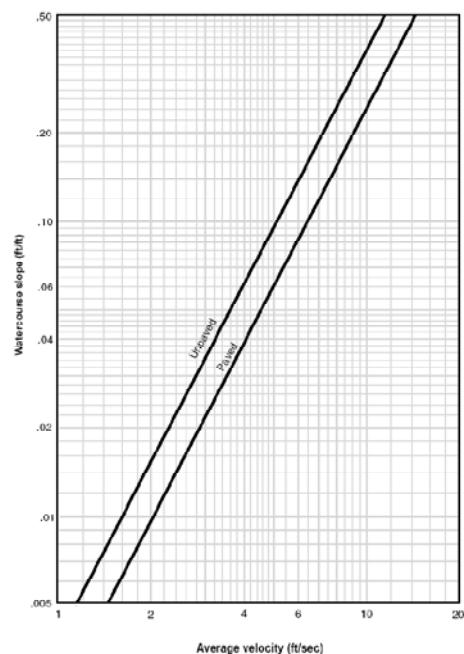
Surface description	n <sup>1</sup>
Smooth surfaces (concrete, asphalt, gravel, or bare soil) .....	0.011
Fallow (no residue) .....	0.05
Cultivated soils:	
Residue cover ≤20% .....	0.06
Residue cover >20% .....	0.17
Grass:	
Short grass prairie .....	0.15
Dense grasses <sup>2</sup> .....	0.24
Bermudagrass .....	0.41
Range (natural) .....	0.13
Woods: <sup>3</sup>	
Light underbrush .....	0.40
Dense underbrush .....	0.80

<sup>1</sup> The n values are a composite of information compiled by Engman (1986).

<sup>2</sup> Includes species such as weeping lovegrass, bluegrass, buffalo grass, blue grama grass, and native grass mixtures.

<sup>3</sup> When selecting n, consider cover to a height of about 0.1 ft. This is the only part of the plant cover that will obstruct sheet flow.

**Figure 3-1** Average velocities for estimating travel time for shallow concentrated flow



## **APPENDIX E – EXISTING FLOODING CONDITIONS DOCUMENTATION**

- FIELD VISIT PICTURES



Field Visit April 15, 2009





Field Visit April 15, 2009





Field Visit April 15, 2009





Field Visit April 15, 2009



Field Visit April 15, 2009





Field Visit April 15, 2009





Field Visit April 15, 2009





Field Visit April 15, 2009



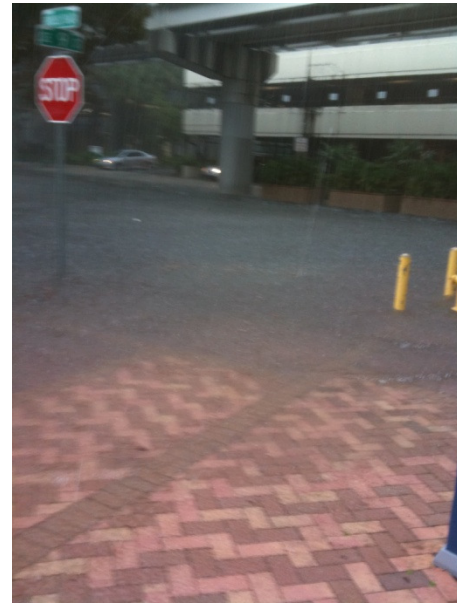
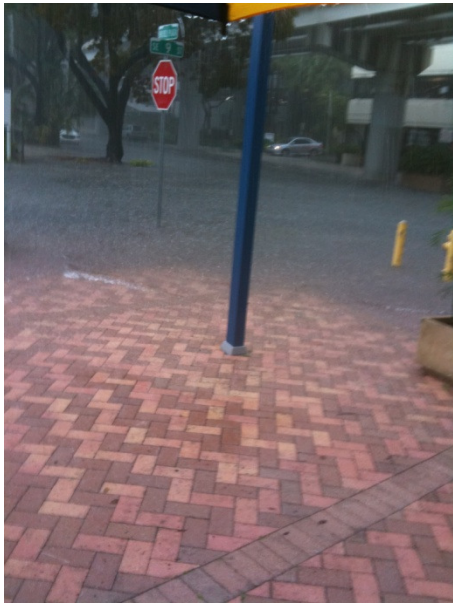


Field Visit April 15, 2009

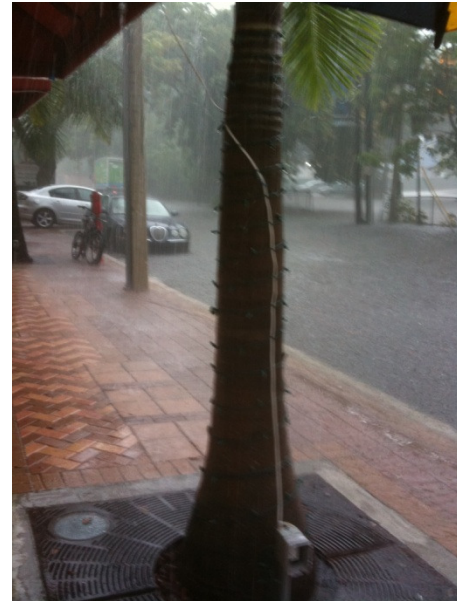


Field Visit April 15, 2009





Field Visit December 17, 2009

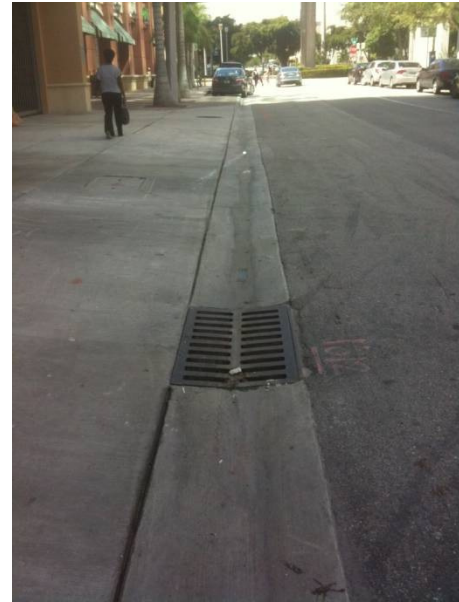


Field Visit December 17, 2009

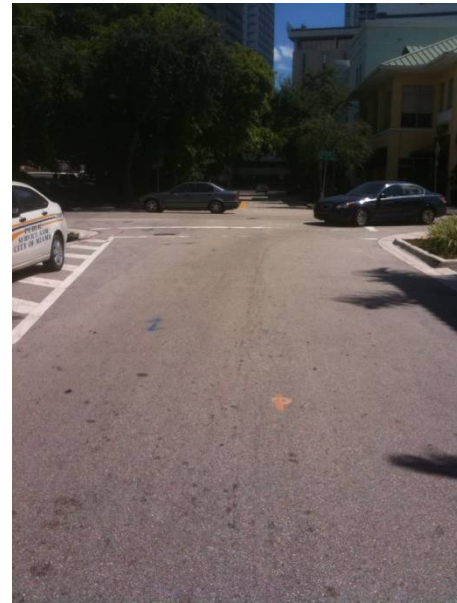


Field Visit December 17, 2009





Site Visit October 8, 2010



Site Visit October 8, 2010

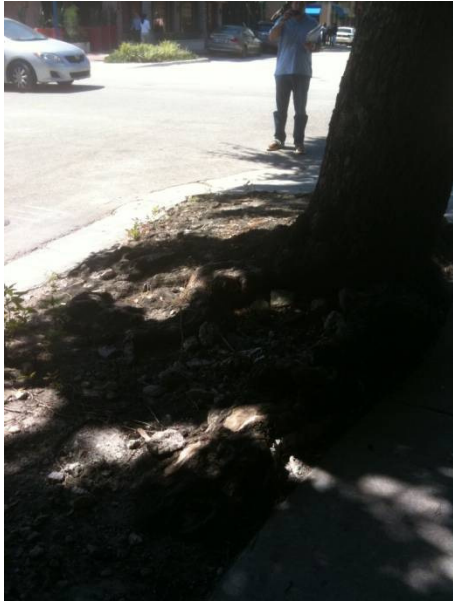


Site Visit October 8, 2010



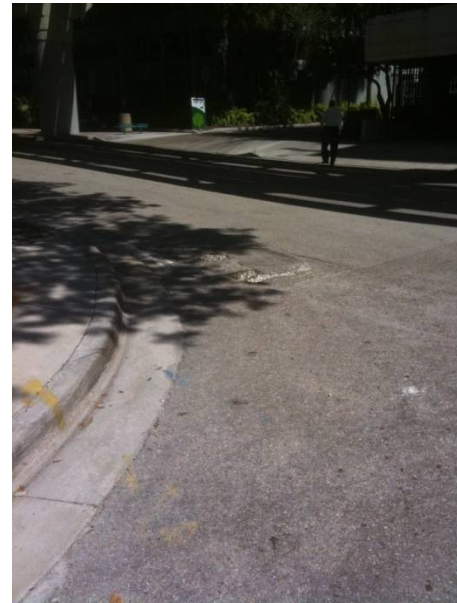


Site Visit October 8, 2010



Site Visit October 8, 2010

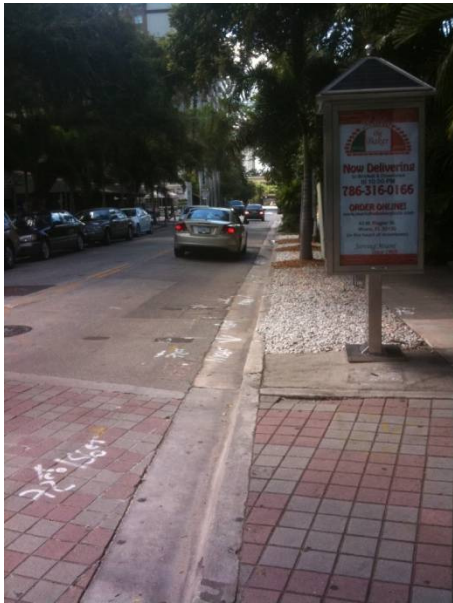
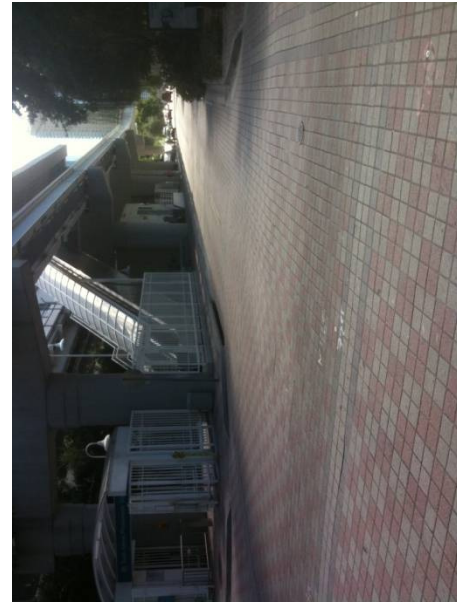




Site Visit October 8, 2010



Site Visit October 8, 2010

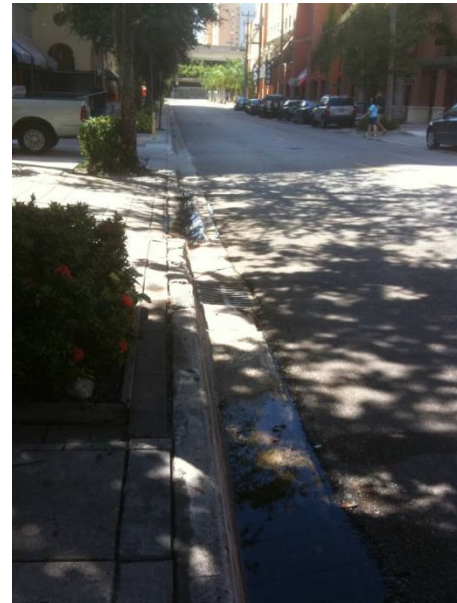
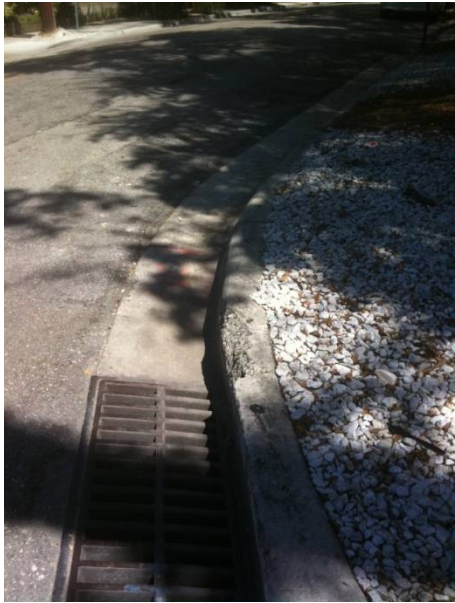


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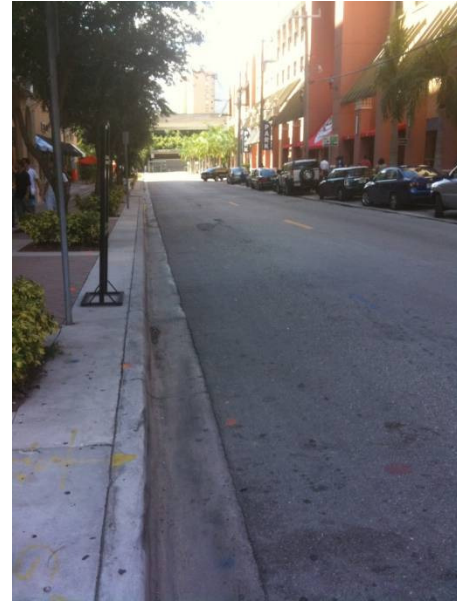


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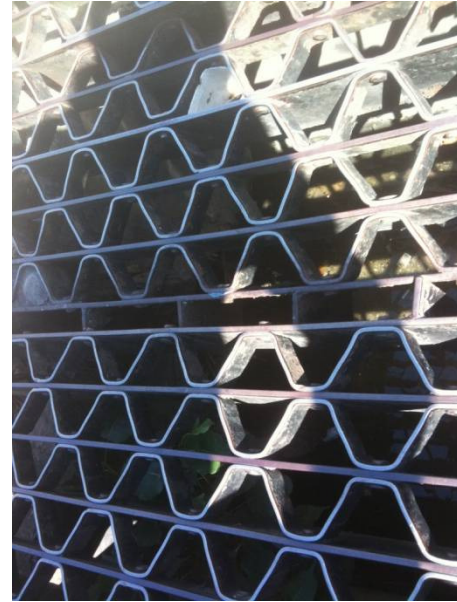


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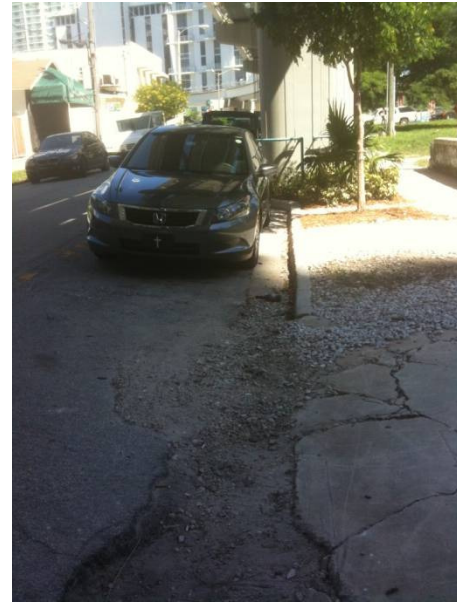


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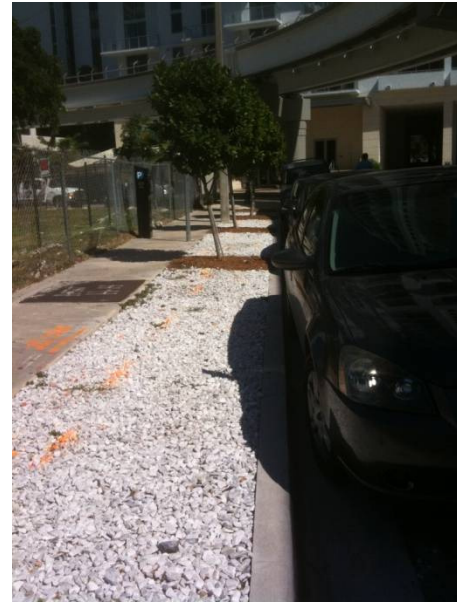
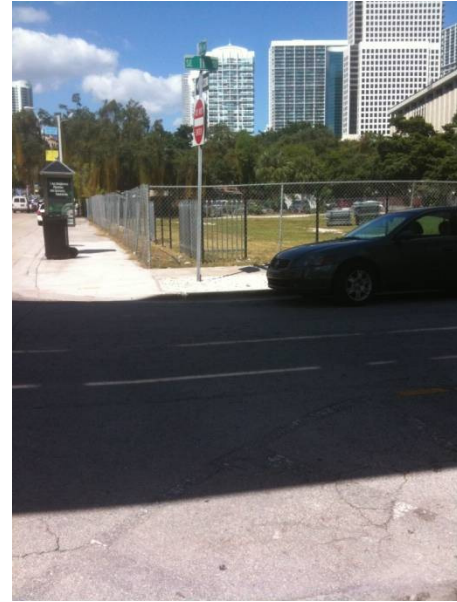




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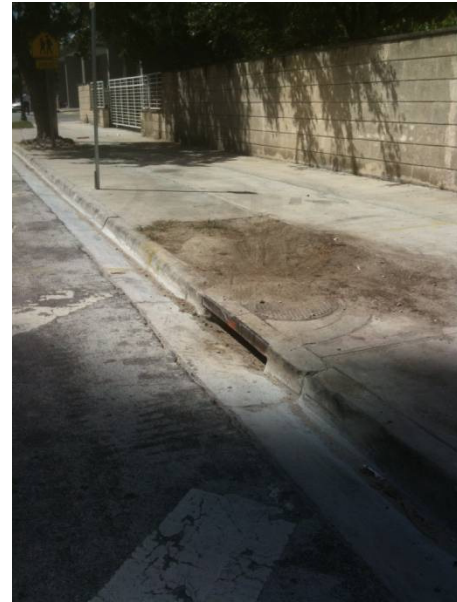
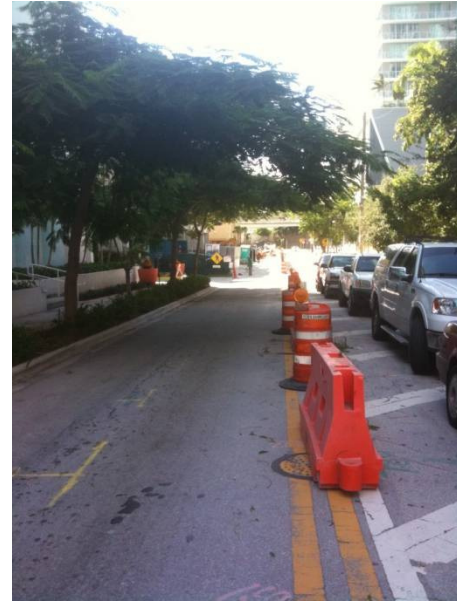


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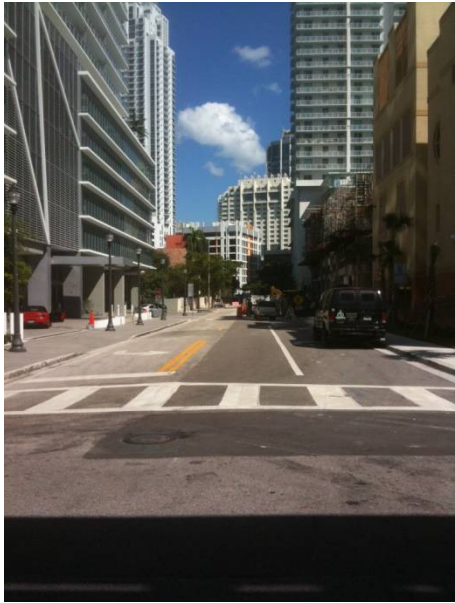


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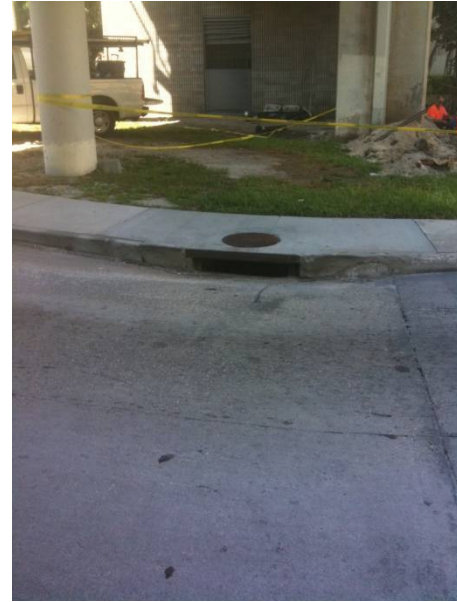


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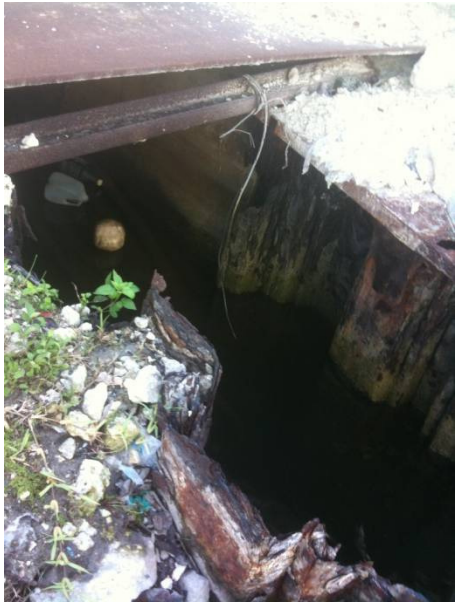


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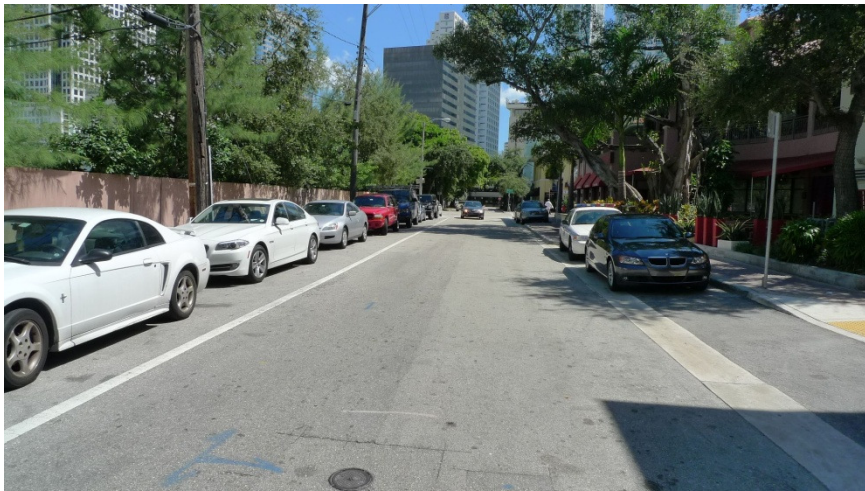


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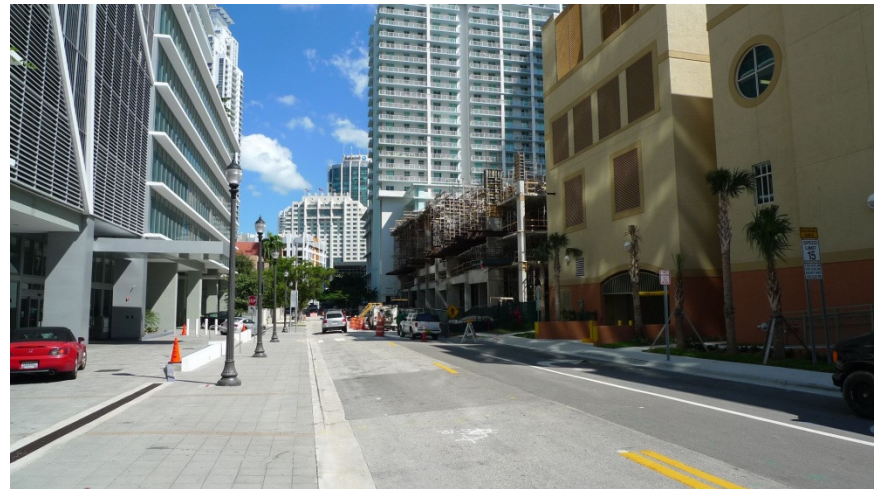
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## **APPENDIX F – ICPR PRE-DEVELOPMENT MODEL**

- NODE – LINK DIAGRAM
- COMPLETE INPUT REPORT
- NODE MAXIMUM CONDITIONS REPORT
- LINK MAXIMUM CONDITIONS REPORT

Mary Brickell Village Drainage Improvements  
 Node Link Diagram  
 Pre Mitigation Condition

Nodes

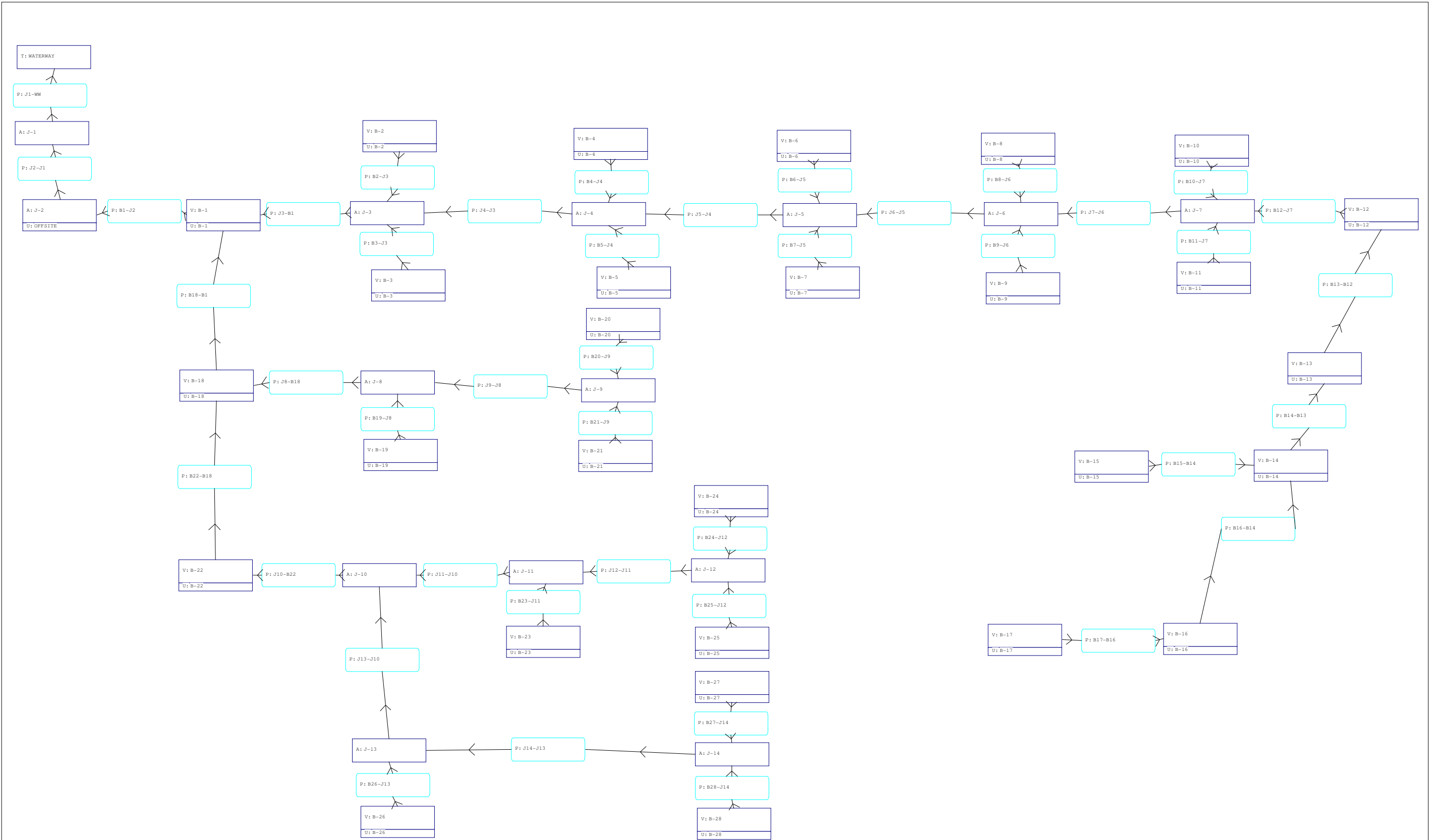
A Stage/Area  
 V Stage/Volume  
 T Time/Stage  
 M Manhole

Basins

O Overland Flow  
 U SCS Unit CN  
 S SBUH CN  
 Y SCS Unit GA  
 Z SBUH GA

Links

P Pipe  
 W Weir  
 C Channel  
 D Drop Structure  
 B Bridge  
 R Rating Curve  
 H Breach  
 E Percolation  
 F Filter  
 X Exfil Trench





Mary Brickell Village Drainage Improvements  
Input Data Report  
Pre Mitigation Condition

---

Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.650	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-15	Node: B-15	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.560	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-16	Node: B-16	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.490	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-17	Node: B-17	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.440	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-18	Node: B-18	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.600	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-19	Node: B-19	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.400	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-2	Node: b-2	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	



Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 1.250	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

Name: B-20	Node: B-20	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 1.130	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

Name: B-21	Node: B-21	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 1.120	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

Name: B-22	Node: B-22	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 1.090	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

Name: B-23	Node: B-23	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.390	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

Name: B-24	Node: B-24	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 1.060	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	





Mary Brickell Village Drainage Improvements  
 Input Data Report  
 Pre Mitigation Condition

Area(ac): 2.960                      Time Shift(hrs): 0.00  
 Curve Number: 98.00                Max Allowable Q(cfs): 999999.000  
 DCIA(%): 0.00

For Tc calculation see Offisite basin Tc calculations spreadsheet.

=====  
 === Nodes =====  
 =====

Name: B-1                      Base Flow(cfs): 0.000                Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 3.800  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
3.800	0.0013
4.000	0.0031
4.500	0.0387
5.000	0.1734
6.000	0.7710
7.000	1.5717
8.000	2.4696
9.000	3.4703
10.500	5.0287
12.000	6.5871

Name: B-10                      Base Flow(cfs): 0.000                Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 4.110  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
4.110	0.0014
4.500	0.0050
5.000	0.0546
6.000	0.3749
7.000	0.9191
8.000	1.6202
9.000	2.3451
10.500	3.4326
12.000	4.5200

Name: B-11                      Base Flow(cfs): 0.000                Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 4.060  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
4.060	0.0014
4.500	0.0084
5.000	0.0546
6.000	0.3151
7.000	0.8961
8.000	2.0271
9.000	3.4190
10.500	5.5068
12.000	7.5946

Name: B-12                      Base Flow(cfs): 0.000                Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 4.150  
 Type: Stage/Volume



Stage(ft)	Volume(af)
2.600	0.0000
4.150	0.0015
4.500	0.0039
5.000	0.0304
6.000	0.1711
7.000	0.4770
8.000	0.9524
9.000	1.5624
10.500	2.6467
12.000	3.7310

Name: B-13                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 5.870  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
5.870	0.0025
6.000	0.0026
7.000	0.0224
8.000	0.0686
9.000	0.1424
10.500	0.3642
12.000	0.6021

Name: B-14                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 5.700  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
5.700	0.0024
6.000	0.0032
7.000	0.0515
8.000	0.1856
9.000	0.4534
10.500	1.1248
12.000	1.9320

Name: B-15                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 5.660  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
5.660	0.0023
6.000	0.0033
7.000	0.0798
8.000	0.3051
9.000	0.6773
10.500	1.4554
12.000	2.2945

Name: B-16                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 8.130  
 Type: Stage/Volume

Stage (ft)	Volume (af)
2.600	0.0000
8.130	0.0037
9.000	0.0740
10.500	0.5881
12.000	1.2283

Name: B-17                              Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                              Warn Stage(ft): 8.150  
 Type: Stage/Volume

Stage (ft)	Volume (af)
2.600	0.0000
8.150	0.0038
9.000	0.0596
10.500	0.6260
12.000	1.3156

Name: B-18                              Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                              Warn Stage(ft): 4.030  
 Type: Stage/Volume

Stage (ft)	Volume (af)
2.600	0.0000
4.030	0.0014
4.500	0.0064
5.000	0.0359
6.000	0.2829
7.000	0.8156
8.000	1.3831
9.000	1.9506
10.500	2.8019
12.000	3.6532

Name: B-19                              Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                              Warn Stage(ft): 4.370  
 Type: Stage/Volume

Stage (ft)	Volume (af)
2.600	0.0000
4.370	0.0016
4.500	0.0017
5.000	0.0073
6.000	0.1121
7.000	0.3848
8.000	0.7395
9.000	1.1411
10.500	1.7434
12.000	2.3458

Name: B-2                              Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                              Warn Stage(ft): 3.960  
 Type: Stage/Volume

Stage (ft)	Volume (af)
2.600	0.0000
3.960	0.0014

Mary Brickell Village Drainage Improvements  
 Input Data Report  
 Pre Mitigation Condition

4.500	0.0200
5.000	0.0808
6.000	0.2586
7.000	0.5060
8.000	0.7940
9.000	1.1270
10.500	1.6521
12.000	2.1918

-----  
 Name: B-20                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 3.670  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
3.670	0.0012
4.000	0.0031
4.500	0.0347
5.000	0.1211
6.000	0.4812
7.000	1.0491
8.000	1.8381
9.000	2.6272
10.500	3.8107
12.000	4.9943

-----  
 Name: B-21                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 3.830  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
3.830	0.0013
4.000	0.0016
4.500	0.0307
5.000	0.1330
6.000	0.4696
7.000	0.9242
8.000	1.4315
9.000	2.1144
10.500	3.1559
12.000	4.1974

-----  
 Name: B-22                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 5.310  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
5.310	0.0021
6.000	0.0197
7.000	0.1241
8.000	0.3267
9.000	0.6524
10.500	1.3352
12.000	2.2350

-----  
 Name: B-23                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 5.340  
 Type: Stage/Volume

Stage (ft)	Volume (af)
2.600	0.0000
5.340	0.0021
6.000	0.0172
7.000	0.0886
8.000	0.2126
9.000	0.3729
10.500	0.7495
12.000	1.2461

Name: B-24                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 4.200  
 Type: Stage/Volume

Stage (ft)	Volume (af)
2.600	0.0000
4.200	0.0015
4.500	0.0020
5.000	0.0251
6.000	0.2376
7.000	0.5373
8.000	0.8959
9.000	1.3047
10.500	1.9634
12.000	2.8260

Name: B-25                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 4.200  
 Type: Stage/Volume

Stage (ft)	Volume (af)
2.600	0.0000
4.200	0.0015
4.500	0.0035
5.000	0.0453
6.000	0.3025
7.000	0.6905
8.000	1.2048
9.000	1.7916
10.500	2.7538
12.000	3.8005

Name: B-26                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 9.940  
 Type: Stage/Volume

Stage (ft)	Volume (af)
2.600	0.0000
9.940	0.0048
10.500	0.0099
12.000	0.0891

Name: B-27                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 5.900  
 Type: Stage/Volume

Stage (ft)	Volume (af)
------------	-------------



Mary Brickell Village Drainage Improvements  
 Input Data Report  
 Pre Mitigation Condition

2.600	0.0000
5.900	0.0025
6.000	0.0222
7.000	0.1041
8.000	0.3342
9.000	0.7004
10.500	1.4681
12.000	2.3786

-----  
 Name: B-28                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 5.800  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
5.800	0.0024
6.000	0.0025
7.000	0.0395
8.000	0.1565
9.000	0.3610
10.500	0.8406
12.000	1.4000

-----  
 Name: B-3                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 3.960  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
3.960	0.0013
4.000	0.0014
4.500	0.0278
5.000	0.1191
6.000	0.4511
7.000	0.8571
8.000	1.3610
9.000	1.8650
10.500	2.6209
12.000	3.3768

-----  
 Name: B-4                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 3.120  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
3.120	0.0009
3.500	0.0013
4.000	0.0092
4.500	0.0446
5.000	0.1445
6.000	0.5415
7.000	0.9754
8.000	1.4128
9.000	1.8534
10.500	2.5198
12.000	3.1921

-----  
 Name: B-5                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 3.690  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
3.690	0.0012
4.000	0.0030
4.500	0.0429
5.000	0.1588
6.000	0.5515
7.000	1.0384
8.000	1.7077
9.000	2.3797
10.500	3.3877
12.000	4.3958

Name: B-6                                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                                      Warn Stage(ft): 4.870  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
4.870	0.0019
5.000	0.0024
6.000	0.0311
7.000	0.1475
8.000	0.3786
9.000	0.6798
10.500	1.2133
12.000	1.7468

Name: B-7                                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                                      Warn Stage(ft): 5.220  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
5.220	0.0012
6.000	0.0403
7.000	0.2176
8.000	0.4601
9.000	0.7026
10.500	1.0663
12.000	1.4301

Name: B-8                                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                                      Warn Stage(ft): 4.900  
 Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
4.900	0.0019
5.000	0.0024
6.000	0.0444
7.000	0.2148
8.000	0.5568
9.000	0.9400
10.500	1.5148
12.000	2.0896

Name: B-9                                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                                      Warn Stage(ft): 4.860

Type: Stage/Volume

Stage(ft)	Volume(af)
2.600	0.0000
4.860	0.0019
5.000	0.0020
6.000	0.0762
7.000	0.3260
8.000	0.6753
9.000	1.0444
10.500	1.5980
12.000	2.1516

Name: J-1                                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                                      Warn Stage(ft): 5.800  
 Type: Stage/Area

Stage(ft)	Area(ac)
2.600	0.0006
5.800	0.0006

Name: J-10                                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                                      Warn Stage(ft): 5.860  
 Type: Stage/Area

Stage(ft)	Area(ac)
2.600	0.0006
5.860	0.0006

Name: J-11                                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                                      Warn Stage(ft): 5.950  
 Type: Stage/Area

Stage(ft)	Area(ac)
2.600	0.0006
5.950	0.0006

Name: J-12                                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                                      Warn Stage(ft): 4.650  
 Type: Stage/Area

Stage(ft)	Area(ac)
2.600	0.0006
4.650	0.0006

Name: J-13                                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                                      Warn Stage(ft): 10.080  
 Type: Stage/Area

Stage(ft)	Area(ac)
2.600	0.0006
10.080	0.0006





Group: BASE  
 Type: Stage/Area

Warn Stage(ft): 4.400

Stage(ft)	Area(ac)
2.600	0.0006
4.400	0.0006

Name: J-8  
 Group: BASE  
 Type: Stage/Area

Base Flow(cfs): 0.000

Init Stage(ft): 2.600  
 Warn Stage(ft): 4.860

Stage(ft)	Area(ac)
2.600	0.0006
4.860	0.0006

Name: J-9  
 Group: BASE  
 Type: Stage/Area

Base Flow(cfs): 0.000

Init Stage(ft): 2.600  
 Warn Stage(ft): 4.000

Stage(ft)	Area(ac)
2.600	0.0006
4.000	0.0006

Name: WATERWAY  
 Group: BASE  
 Type: Time/Stage

Base Flow(cfs): 0.000

Init Stage(ft): 2.600  
 Warn Stage(ft): 2.600

Outfall Discharge to Miami River,  
 Tidal Data at Miami Marina NOAA Station used to determine mean high-high water.  
 MHHW determined to be 2.6' City of Miami Datum

Time(hrs)	Stage(ft)
0.00	2.600
100.00	2.600

==== Pipes =====

Name: B1-J2	From Node: B-1	Length(ft): 119.00
Group: BASE	To Node: J-2	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Rectangular	Rectangular	Exit Loss Coef: 0.00
Span(in): 54.00	54.00	Bend Loss Coef: 0.70
Rise(in): 30.00	30.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 0.150	-0.250	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: B10-J7	From Node: B-10	Length(ft): 11.00
Group: BASE	To Node: J-7	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 12.00	12.00	Bend Loss Coef: 0.70
Rise(in): 12.00	12.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 2.170	1.550	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B11-J7	From Node: B-11	Length(ft): 19.00
Group: BASE	To Node: J-7	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 12.00	12.00	Bend Loss Coef: 0.70
Rise(in): 12.00	12.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 2.010	1.550	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B12-J7	From Node: B-12	Length(ft): 61.00
Group: BASE	To Node: J-7	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Rectangular	Rectangular	Exit Loss Coef: 0.00
Span(in): 30.00	30.00	Bend Loss Coef: 0.00
Rise(in): 19.00	19.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 1.800	1.800	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: B13-B12	From Node: B-13	Length(ft): 320.00
Group: BASE	To Node: B-12	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Rectangular	Rectangular	
Span(in): 30.00	30.00	

Rise(in): 19.00	19.00	Exit Loss Coef: 0.00
Invert(ft): 1.320	0.360	Bend Loss Coef: 0.70
Manning's N: 0.012000	0.012000	Outlet Ctrl Spec: Use dc or tw
Top Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
Bot Clip(in): 0.000	0.000	Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: B14-B13	From Node: B-14	Length(ft): 78.00
Group: BASE	To Node: B-13	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Rectangular	Rectangular	Exit Loss Coef: 0.00
Span(in): 23.00	23.00	Bend Loss Coef: 0.00
Rise(in): 14.00	14.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 1.750	1.770	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: B15-B14	From Node: B-15	Length(ft): 22.00
Group: BASE	To Node: B-14	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 12.00	12.00	Bend Loss Coef: 0.55
Rise(in): 12.00	12.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 1.950	1.770	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B16-B14	From Node: B-16	Length(ft): 349.00
Group: BASE	To Node: B-14	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 15.00	15.00	Bend Loss Coef: 0.00
Rise(in): 15.00	15.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 2.550	1.800	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

```

-----
Name: B17-B16          From Node: B-17          Length(ft): 30.00
Group: BASE           To Node: B-16             Count: 1
                        UPSTREAM      DOWNSTREAM
Geometry: Circular    Circular
Span(in): 12.00       12.00
Rise(in): 12.00       12.00
Invert(ft): 2.800     2.480
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
                        Friction Equation: Automatic
                        Solution Algorithm: Most Restrictive
                        Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.55
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

```

-----
Name: B18-B1          From Node: B-18          Length(ft): 350.00
Group: BASE           To Node: B-1             Count: 1
                        UPSTREAM      DOWNSTREAM
Geometry: Rectangular Rectangular
Span(in): 42.00       42.00
Rise(in): 30.00       30.00
Invert(ft): 0.590     0.150
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
                        Friction Equation: Automatic
                        Solution Algorithm: Most Restrictive
                        Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

```

-----
Name: B19-J8          From Node: B-19          Length(ft): 32.00
Group: BASE           To Node: J-8             Count: 1
                        UPSTREAM      DOWNSTREAM
Geometry: Circular    Circular
Span(in): 12.00       12.00
Rise(in): 12.00       12.00
Invert(ft): 2.110     1.950
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
                        Friction Equation: Automatic
                        Solution Algorithm: Most Restrictive
                        Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:



Circular Concrete: Square edge w/ headwall

```

-----
Name: B2-J3           From Node: B-2           Length(ft): 17.00
Group: BASE           To Node: J-3             Count: 1
                        UPSTREAM           DOWNSTREAM
Geometry: Circular    Circular
Span(in): 12.00       12.00
Rise(in): 12.00       12.00
Invert(ft): 0.510     0.270
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
Friction Equation: Automatic
Solution Algorithm: Most Restrictive
Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

```

-----
Name: B20-J9          From Node: B-20          Length(ft): 12.00
Group: BASE           To Node: J-9             Count: 1
                        UPSTREAM           DOWNSTREAM
Geometry: Circular    Circular
Span(in): 18.00       18.00
Rise(in): 18.00       18.00
Invert(ft): 1.800     1.800
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
Friction Equation: Automatic
Solution Algorithm: Most Restrictive
Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

```

-----
Name: B21-J9          From Node: B-21          Length(ft): 40.00
Group: BASE           To Node: J-9             Count: 1
                        UPSTREAM           DOWNSTREAM
Geometry: Circular    Circular
Span(in): 18.00       18.00
Rise(in): 18.00       18.00
Invert(ft): 1.500     1.500
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
Friction Equation: Automatic
Solution Algorithm: Most Restrictive
Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

```

-----
Name: B22-B18          From Node: B-22          Length(ft): 346.00
  
```

Group: BASE	To Node: B-18	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Rectangular	Rectangular	Entrance Loss Coef: 0.50
Span(in): 36.00	36.00	Exit Loss Coef: 0.00
Rise(in): 30.00	30.00	Bend Loss Coef: 0.00
Invert(ft): 1.110	0.590	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	Stabilizer Option: None
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: B23-J11	From Node: B-23	Length(ft): 31.00
Group: BASE	To Node: J-11	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Circular	Circular	Entrance Loss Coef: 0.50
Span(in): 15.00	15.00	Exit Loss Coef: 0.00
Rise(in): 15.00	15.00	Bend Loss Coef: 0.70
Invert(ft): 3.400	3.250	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	Stabilizer Option: None
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B24-J12	From Node: B-24	Length(ft): 13.00
Group: BASE	To Node: J-12	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Circular	Circular	Entrance Loss Coef: 0.50
Span(in): 12.00	12.00	Exit Loss Coef: 0.00
Rise(in): 12.00	12.00	Bend Loss Coef: 0.70
Invert(ft): 2.500	2.100	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	Stabilizer Option: None
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B25-J12	From Node: B-25	Length(ft): 21.00
Group: BASE	To Node: J-12	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Circular	Circular	Entrance Loss Coef: 0.50
Span(in): 12.00	12.00	Exit Loss Coef: 0.00
Rise(in): 12.00	12.00	

Invert(ft): 2.410	2.120	Bend Loss Coef: 0.70
Manning's N: 0.012000	0.012000	Outlet Ctrl Spec: Use dc or tw
Top Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
Bot Clip(in): 0.000	0.000	Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B26-J13	From Node: B-26	Length(ft): 41.00
Group: BASE	To Node: J-13	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 12.00	12.00	Bend Loss Coef: 0.00
Rise(in): 12.00	12.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 5.110	4.440	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B27-J14	From Node: B-27	Length(ft): 9.00
Group: BASE	To Node: J-14	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 12.00	12.00	Bend Loss Coef: 0.70
Rise(in): 12.00	12.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 2.770	2.500	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B28-J14	From Node: B-28	Length(ft): 26.00
Group: BASE	To Node: J-14	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 12.00	12.00	Bend Loss Coef: 0.70
Rise(in): 12.00	12.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 2.800	2.500	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
Circular Concrete: Square edge w/ headwall

---

Name: B3-J3	From Node: B-3	Length(ft): 37.00
Group: BASE	To Node: J-3	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 12.00	12.00	Bend Loss Coef: 0.70
Rise(in): 12.00	12.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 0.870	1.350	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
Circular Concrete: Square edge w/ headwall

---

Name: B4-J4	From Node: B-4	Length(ft): 6.00
Group: BASE	To Node: J-4	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 12.00	12.00	Bend Loss Coef: 0.70
Rise(in): 12.00	12.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 1.370	1.000	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
Circular Concrete: Square edge w/ headwall

---

Name: B5-J4	From Node: B-5	Length(ft): 18.00
Group: BASE	To Node: J-4	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 12.00	12.00	Bend Loss Coef: 0.70
Rise(in): 12.00	12.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 1.640	1.000	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
Circular Concrete: Square edge w/ headwall



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-----
Name: B6-J5           From Node: B-6           Length(ft): 9.00
Group: BASE           To Node: J-5             Count: 1
                        UPSTREAM           DOWNSTREAM
Geometry: Circular    Circular
Span(in): 12.00      12.00
Rise(in): 12.00      12.00
Invert(ft): 1.820    1.470
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000  0.000
Bot Clip(in): 0.000  0.000
                        Friction Equation: Automatic
                        Solution Algorithm: Most Restrictive
                        Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

```

-----
Name: B7-J5           From Node: B-7           Length(ft): 33.00
Group: BASE           To Node: J-5             Count: 1
                        UPSTREAM           DOWNSTREAM
Geometry: Circular    Circular
Span(in): 12.00      12.00
Rise(in): 12.00      12.00
Invert(ft): 0.970    0.590
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000  0.000
Bot Clip(in): 0.000  0.000
                        Friction Equation: Automatic
                        Solution Algorithm: Most Restrictive
                        Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

```

-----
Name: B8-J6           From Node: B-8           Length(ft): 20.00
Group: BASE           To Node: J-6             Count: 1
                        UPSTREAM           DOWNSTREAM
Geometry: Circular    Circular
Span(in): 12.00      12.00
Rise(in): 12.00      12.00
Invert(ft): 1.390    0.800
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000  0.000
Bot Clip(in): 0.000  0.000
                        Friction Equation: Automatic
                        Solution Algorithm: Most Restrictive
                        Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

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-----
Name: B9-J6           From Node: B-9           Length(ft): 32.00
Group: BASE           To Node: J-6             Count: 1
  
```

	UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
			Solution Algorithm: Most Restrictive
Geometry:	Circular	Circular	Flow: Both
Span(in):	12.00	12.00	Entrance Loss Coef: 0.50
Rise(in):	12.00	12.00	Exit Loss Coef: 0.00
Invert(ft):	1.460	0.450	Bend Loss Coef: 0.70
Manning's N:	0.012000	0.012000	Outlet Ctrl Spec: Use dc or tw
Top Clip(in):	0.000	0.000	Inlet Ctrl Spec: Use dc
Bot Clip(in):	0.000	0.000	Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name:	J1-WW	From Node:	J-1	Length(ft):	450.00
Group:	BASE	To Node:	WATERWAY	Count:	1
	UPSTREAM	DOWNSTREAM	Friction Equation: Automatic		
Geometry:	Rectangular	Rectangular	Solution Algorithm: Most Restrictive		
Span(in):	60.00	60.00	Flow: Both		
Rise(in):	36.00	36.00	Entrance Loss Coef: 0.50		
Invert(ft):	-0.680	-0.800	Exit Loss Coef: 1.00		
Manning's N:	0.012000	0.012000	Bend Loss Coef: 0.00		
Top Clip(in):	0.000	0.000	Outlet Ctrl Spec: Use dc or tw		
Bot Clip(in):	0.000	0.000	Inlet Ctrl Spec: Use dc		
			Stabilizer Option: None		

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name:	J10-B22	From Node:	J-10	Length(ft):	45.00
Group:	BASE	To Node:	B-22	Count:	1
	UPSTREAM	DOWNSTREAM	Friction Equation: Automatic		
Geometry:	Rectangular	Rectangular	Solution Algorithm: Most Restrictive		
Span(in):	36.00	36.00	Flow: Both		
Rise(in):	30.00	30.00	Entrance Loss Coef: 0.50		
Invert(ft):	1.200	1.110	Exit Loss Coef: 0.00		
Manning's N:	0.012000	0.012000	Bend Loss Coef: 0.70		
Top Clip(in):	0.000	0.000	Outlet Ctrl Spec: Use dc or tw		
Bot Clip(in):	0.000	0.000	Inlet Ctrl Spec: Use dc		
			Stabilizer Option: None		

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name:	J11-J10	From Node:	J-11	Length(ft):	22.00
Group:	BASE	To Node:	J-10	Count:	1
	UPSTREAM	DOWNSTREAM	Friction Equation: Automatic		
Geometry:	Rectangular	Rectangular	Solution Algorithm: Most Restrictive		
Span(in):	24.00	24.00	Flow: Both		
Rise(in):	15.00	15.00	Entrance Loss Coef: 0.50		
Invert(ft):	1.280	1.200	Exit Loss Coef: 0.00		
			Bend Loss Coef: 0.00		

Manning's N: 0.012000	0.012000	Outlet Ctrl Spec: Use dc or tw
Top Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
Bot Clip(in): 0.000	0.000	Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: J12-J11	From Node: J-12	Length(ft): 351.00
Group: BASE	To Node: J-11	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Rectangular	Rectangular	Exit Loss Coef: 0.00
Span(in): 24.00	24.00	Bend Loss Coef: 0.00
Rise(in): 15.00	15.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 1.950	1.280	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: J13-J10	From Node: J-13	Length(ft): 348.00
Group: BASE	To Node: J-10	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 21.00	21.00	Bend Loss Coef: 0.70
Rise(in): 21.00	21.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 1.160	0.780	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: J14-J13	From Node: J-14	Length(ft): 392.00
Group: BASE	To Node: J-13	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Circular	Circular	Exit Loss Coef: 0.00
Span(in): 21.00	21.00	Bend Loss Coef: 0.70
Rise(in): 21.00	21.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 2.000	1.060	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: J2-J1	From Node: J-2	Length(ft): 360.00
Group: BASE	To Node: J-1	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Rectangular	Rectangular	Exit Loss Coef: 0.00
Span(in): 60.00	60.00	Bend Loss Coef: 0.00
Rise(in): 36.00	36.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): -0.250	-0.680	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: J3-B1	From Node: J-3	Length(ft): 48.00
Group: BASE	To Node: B-1	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Rectangular	Rectangular	Exit Loss Coef: 0.00
Span(in): 54.00	54.00	Bend Loss Coef: 0.00
Rise(in): 30.00	30.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 0.690	0.150	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: J4-J3	From Node: J-4	Length(ft): 230.00
Group: BASE	To Node: J-3	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
UPSTREAM	DOWNSTREAM	Entrance Loss Coef: 0.50
Geometry: Rectangular	Rectangular	Exit Loss Coef: 0.00
Span(in): 36.00	36.00	Bend Loss Coef: 0.00
Rise(in): 24.00	24.00	Outlet Ctrl Spec: Use dc or tw
Invert(ft): 0.750	0.690	Inlet Ctrl Spec: Use dc
Manning's N: 0.012000	0.012000	Stabilizer Option: None
Top Clip(in): 0.000	0.000	
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares



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-----
Name: J5-J4           From Node: J-5           Length(ft): 383.00
Group: BASE           To Node: J-4             Count: 1
                        UPSTREAM       DOWNSTREAM
Geometry: Rectangular Rectangular
Span(in): 36.00       36.00
Rise(in): 24.00       24.00
Invert(ft): 1.160     0.750
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
                        Friction Equation: Automatic
                        Solution Algorithm: Most Restrictive
                        Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.00
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

```

-----
Name: J6-J5           From Node: J-6           Length(ft): 50.00
Group: BASE           To Node: J-5             Count: 1
                        UPSTREAM       DOWNSTREAM
Geometry: Rectangular Rectangular
Span(in): 36.00       36.00
Rise(in): 24.00       24.00
Invert(ft): -1.050    -1.120
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
                        Friction Equation: Automatic
                        Solution Algorithm: Most Restrictive
                        Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.00
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

```

-----
Name: J7-J6           From Node: J-7           Length(ft): 264.00
Group: BASE           To Node: J-6             Count: 1
                        UPSTREAM       DOWNSTREAM
Geometry: Rectangular Rectangular
Span(in): 36.00       36.00
Rise(in): 24.00       24.00
Invert(ft): 1.560     1.330
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
                        Friction Equation: Automatic
                        Solution Algorithm: Most Restrictive
                        Flow: Both
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.00
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

```

-----
Name: J8-B18          From Node: J-8           Length(ft): 53.00
Group: BASE           To Node: B-18            Count: 1
                        Friction Equation: Automatic
  
```

Mary Brickell Village Drainage Improvements  
 Input Data Report  
 Pre Mitigation Condition

	UPSTREAM	DOWNSTREAM	Solution Algorithm: Most Restrictive
Geometry:	Rectangular	Rectangular	Flow: Both
Span(in):	36.00	36.00	Entrance Loss Coef: 0.50
Rise(in):	30.00	30.00	Exit Loss Coef: 0.00
Invert(ft):	0.810	0.650	Bend Loss Coef: 0.70
Manning's N:	0.012000	0.012000	Outlet Ctrl Spec: Use dc or tw
Top Clip(in):	0.000	0.000	Inlet Ctrl Spec: Use dc
Bot Clip(in):	0.000	0.000	Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: J9-J8	From Node: J-9	Length(ft): 294.00
Group: BASE	To Node: J-8	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
		Flow: Both
Geometry: Rectangular	Rectangular	Entrance Loss Coef: 0.50
Span(in): 24.00	24.00	Exit Loss Coef: 0.00
Rise(in): 15.00	15.00	Bend Loss Coef: 0.00
Invert(ft): 1.300	0.740	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	Stabilizer Option: None
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

==== Hydrology Simulations =====

Name: 100yr-72hr  
 Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\pre results\100yr-72hr.R

Override Defaults: Yes  
 Storm Duration(hrs): 72.00  
 Rainfall File: Sfwmd72  
 Rainfall Amount(in): 14.00

Time(hrs)	Print Inc(min)
48.000	15.00
56.000	5.00
64.000	1.00
72.000	5.00
72.330	5.00

Name: 10yr-24hr  
 Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\pre results\10yr-24hr.R3

Override Defaults: Yes  
 Storm Duration(hrs): 24.00  
 Rainfall File: Flmod  
 Rainfall Amount(in): 7.90

Time(hrs)	Print Inc(min)
8.000	15.00
10.000	5.00

14.000            1.00  
 16.000            5.00  
 24.000            15.00  
 24.330            5.00

-----  
 Name: 1hr\_calibrate  
 Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\pre results\1hr\_calibrat

Override Defaults: Yes  
 Storm Duration(hrs): 1.00  
     Rainfall File: Fdot-1  
 Rainfall Amount(in): 2.00

Time(hrs)	Print Inc(min)
1.000	1.00
1.330	1.00

-----  
 Name: 25yr-72hr  
 Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\pre results\25yr-72hr.R3

Override Defaults: Yes  
 Storm Duration(hrs): 72.00  
     Rainfall File: Sfwmd72  
 Rainfall Amount(in): 12.00

Time(hrs)	Print Inc(min)
48.000	15.00
56.000	5.00
64.000	1.00
72.000	5.00
72.330	5.00

-----  
 Name: 5yr-24hr  
 Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\pre results\5yr-24hr.R32

Override Defaults: Yes  
 Storm Duration(hrs): 24.00  
     Rainfall File: Flmod  
 Rainfall Amount(in): 6.30

Time(hrs)	Print Inc(min)
8.000	15.00
10.000	5.00
14.000	1.00
16.000	5.00
24.000	15.00
24.330	5.00

=====  
 ==== Routing Simulations =====  
 =====

Name: 100yr-72hr            Hydrology Sim: 100yr-72hr  
 Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\pre results\100yr-72hr.I

Execute: Yes            Restart: No            Patch: No  
 Alternative: No

Max Delta Z(ft): 1.00            Delta Z Factor: 0.01000  
 Time Step Optimizer: 10.000  
 Start Time(hrs): 0.000            End Time(hrs): 96.00  
 Min Calc Time(sec): 0.0500        Max Calc Time(sec): 60.0000  
 Boundary Stages: 25/100yr River    Boundary Flows:

Time(hrs)	Print Inc(min)
48.000	15.000

Mary Brickell Village Drainage Improvements  
 Input Data Report  
 Pre Mitigation Condition

56.000            5.000  
 64.000            1.000  
 72.000            5.000  
 96.000            15.000

Group            Run  
 -----  
 BASE            Yes

Name: 10yr-24hr            Hydrology Sim: 10yr-24hr  
 Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\pre results\10yr-24hr.I3

Execute: Yes            Restart: No            Patch: No  
 Alternative: No

Max Delta Z(ft): 1.00            Delta Z Factor: 0.01000  
 Time Step Optimizer: 10.000  
 Start Time(hrs): 0.000            End Time(hrs): 48.00  
 Min Calc Time(sec): 0.0500            Max Calc Time(sec): 60.0000  
 Boundary Stages:            Boundary Flows:

Time(hrs)            Print Inc(min)  
 -----  
 8.000            5.000  
 16.000            1.000  
 24.000            5.000  
 48.000            15.000

Group            Run  
 -----  
 BASE            Yes

Name: 1hr\_calibrate            Hydrology Sim: 1hr\_calibrate  
 Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\pre results\1hr\_calibrat

Execute: Yes            Restart: No            Patch: No  
 Alternative: No

Max Delta Z(ft): 1.00            Delta Z Factor: 0.01000  
 Time Step Optimizer: 10.000  
 Start Time(hrs): 0.000            End Time(hrs): 25.00  
 Min Calc Time(sec): 0.0500            Max Calc Time(sec): 60.0000  
 Boundary Stages:            Boundary Flows:

Time(hrs)            Print Inc(min)  
 -----  
 1.000            1.000  
 25.000            15.000

Group            Run  
 -----  
 BASE            Yes

Name: 25yr-72hr            Hydrology Sim: 25yr-72hr  
 Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\pre results\25yr-72hr.I3

Execute: Yes            Restart: No            Patch: No  
 Alternative: No

Max Delta Z(ft): 1.00            Delta Z Factor: 0.01000  
 Time Step Optimizer: 10.000  
 Start Time(hrs): 0.000            End Time(hrs): 96.00  
 Min Calc Time(sec): 0.0500            Max Calc Time(sec): 60.0000  
 Boundary Stages: 25/100yr River            Boundary Flows:



Time(hrs)	Print Inc(min)
48.000	15.000
56.000	5.000
64.000	1.000
72.000	5.000
96.000	15.000

Group	Run
BASE	Yes

Name: 5yr-24hr                      Hydrology Sim: 5yr-24hr  
 Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\pre results\5yr-24hr.I32

Execute: Yes                      Restart: No                      Patch: No  
 Alternative: No

Max Delta Z(ft): 1.00	Delta Z Factor: 0.01000
Time Step Optimizer: 10.000	
Start Time(hrs): 0.000	End Time(hrs): 48.00
Min Calc Time(sec): 0.0500	Max Calc Time(sec): 60.0000
Boundary Stages:	Boundary Flows:

Time(hrs)	Print Inc(min)
8.000	5.000
16.000	1.000
24.000	5.000
48.000	15.000

Group	Run
BASE	Yes

==== Boundary Conditions =====

Name: 25/100yr River                      Node: WATERWAY                      Type: Stage

Time(hrs)	Stage(ft)
0.000	3.800
1000.000	3.800

Mary Brickell Village Drainage Improvements  
Node Maximum Comparison Report  
Pre Mitigation Condition

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
B-1	BASE	100yr-72hr	60.50	5.171	3.800	0.0069	20917	60.54	37.752	60.82	38.658
B-1	BASE	10yr-24hr	12.34	4.419	3.800	0.0092	6548	12.32	44.042	12.53	44.565
B-1	BASE	1hr_calibrate	0.83	3.969	3.800	0.0086	1562	0.81	39.434	0.87	39.454
B-1	BASE	25yr-72hr	60.45	5.032	3.800	0.0069	19297	60.52	36.088	60.75	36.784
B-1	BASE	5yr-24hr	12.30	4.199	3.800	0.0098	4053	12.30	41.968	12.39	42.134
B-10	BASE	100yr-72hr	60.85	5.920	4.110	0.0033	18054	60.02	4.597	62.66	2.518
B-10	BASE	10yr-24hr	12.65	5.449	4.110	-0.0063	13491	12.03	3.493	13.55	3.545
B-10	BASE	1hr_calibrate	0.95	4.856	4.110	-0.0060	7185	0.65	2.194	1.26	2.893
B-10	BASE	25yr-72hr	60.75	5.747	4.110	0.0033	16376	60.02	3.939	62.22	2.392
B-10	BASE	5yr-24hr	12.52	5.178	4.110	-0.0066	10865	12.03	2.782	13.14	3.286
B-11	BASE	100yr-72hr	60.85	5.935	4.060	0.0033	17633	60.02	5.528	62.66	2.450
B-11	BASE	10yr-24hr	12.66	5.474	4.060	-0.0054	12730	12.03	4.201	13.44	3.366
B-11	BASE	1hr_calibrate	0.96	4.886	4.060	-0.0059	6468	0.65	2.639	1.28	2.889
B-11	BASE	25yr-72hr	60.75	5.762	4.060	0.0033	15797	60.02	4.738	62.13	2.316
B-11	BASE	5yr-24hr	12.53	5.207	4.060	-0.0048	9890	12.03	3.345	13.13	3.133
B-12	BASE	100yr-72hr	60.60	6.046	4.150	0.0031	10088	60.02	14.066	60.12	9.983
B-12	BASE	10yr-24hr	12.49	5.572	4.150	0.0045	7394	12.05	12.330	12.11	9.364
B-12	BASE	1hr_calibrate	0.87	4.934	4.150	0.0043	3856	0.67	9.104	0.74	7.621
B-12	BASE	25yr-72hr	60.56	5.857	4.150	0.0031	8963	60.02	12.958	60.10	9.486
B-12	BASE	5yr-24hr	12.38	5.279	4.150	0.0039	5779	12.05	10.915	12.15	8.638
B-13	BASE	100yr-72hr	60.44	6.287	5.870	0.0031	755	60.04	8.322	60.05	8.053
B-13	BASE	10yr-24hr	12.39	5.799	5.870	0.0044	137	12.04	7.833	12.05	7.754
B-13	BASE	1hr_calibrate	0.83	5.084	5.870	0.0046	137	0.68	6.339	0.68	6.263
B-13	BASE	25yr-72hr	60.35	6.075	5.870	0.0031	546	60.05	7.882	60.03	7.806
B-13	BASE	5yr-24hr	12.32	5.469	5.870	0.0042	137	12.05	7.352	12.06	7.273
B-14	BASE	100yr-72hr	60.30	6.690	5.700	0.0027	3100	60.03	8.487	60.12	7.143
B-14	BASE	10yr-24hr	12.33	6.161	5.700	0.0049	1587	12.07	7.431	12.05	6.890
B-14	BASE	1hr_calibrate	0.78	5.330	5.700	0.0051	128	0.67	5.836	0.68	5.756
B-14	BASE	25yr-72hr	60.25	6.448	5.700	0.0027	2408	60.02	7.825	60.10	6.879
B-14	BASE	5yr-24hr	12.23	5.776	5.700	0.0046	353	12.03	6.679	12.05	6.601
B-15	BASE	100yr-72hr	60.38	6.808	5.660	0.0032	5643	60.02	3.479	59.70	1.931
B-15	BASE	10yr-24hr	12.35	6.296	5.660	-0.0072	3164	12.03	2.644	11.90	1.945
B-15	BASE	1hr_calibrate	0.76	5.440	5.660	0.0054	114	0.65	1.660	0.68	1.570
B-15	BASE	25yr-72hr	60.30	6.568	5.660	0.0027	4482	60.02	2.981	59.73	1.895
B-15	BASE	5yr-24hr	12.20	5.915	5.660	0.0047	1319	12.03	2.105	11.99	1.885
B-16	BASE	100yr-72hr	60.22	7.754	8.130	0.0041	1549	60.03	4.616	60.18	3.530
B-16	BASE	10yr-24hr	12.29	6.954	8.130	0.0057	1044	12.05	3.644	12.23	3.048
B-16	BASE	1hr_calibrate	0.77	5.826	8.130	0.0060	332	0.67	2.553	0.75	2.397
B-16	BASE	25yr-72hr	60.19	7.367	8.130	0.0034	1305	60.03	4.077	60.16	3.272
B-16	BASE	5yr-24hr	12.20	6.411	8.130	0.0055	701	12.06	3.032	12.19	2.709
B-17	BASE	100yr-72hr	60.22	7.916	8.150	0.0043	1326	60.02	2.733	60.19	1.672
B-17	BASE	10yr-24hr	12.29	7.074	8.150	0.0059	897	12.03	2.077	12.24	1.444
B-17	BASE	1hr_calibrate	0.77	5.900	8.150	0.0062	298	0.65	1.305	0.76	1.134

Mary Brickell Village Drainage Improvements  
Node Maximum Comparison Report  
Pre Mitigation Condition

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
B-17	BASE	25yr-72hr	60.19	7.506	8.150	0.0036	1117	60.02	2.342	60.17	1.550
B-17	BASE	5yr-24hr	12.20	6.506	8.150	0.0057	607	12.03	1.654	12.20	1.282
B-18	BASE	100yr-72hr	60.51	5.453	4.030	0.0054	11401	60.00	25.088	60.51	19.269
B-18	BASE	10yr-24hr	12.34	4.774	4.030	-0.0073	4396	12.05	24.146	12.36	21.626
B-18	BASE	1hr_calibrate	0.84	4.243	4.030	0.0068	887	0.67	21.240	0.81	19.040
B-18	BASE	25yr-72hr	60.44	5.286	4.030	-0.0062	9679	60.01	24.115	60.38	18.328
B-18	BASE	5yr-24hr	12.30	4.513	4.030	-0.0078	1706	12.06	22.805	12.28	20.336
B-19	BASE	100yr-72hr	60.53	5.504	4.370	0.0055	5399	60.02	2.485	59.67	1.167
B-19	BASE	10yr-24hr	12.33	4.871	4.370	0.0032	1941	12.03	1.888	11.94	1.498
B-19	BASE	1hr_calibrate	0.81	4.307	4.370	0.0039	114	0.65	1.186	0.70	1.146
B-19	BASE	25yr-72hr	60.45	5.334	4.370	0.0055	4432	60.02	2.129	59.69	1.157
B-19	BASE	5yr-24hr	12.25	4.591	4.370	0.0034	676	12.03	1.504	12.01	1.428
B-2	BASE	100yr-72hr	60.41	5.732	3.960	0.0052	8528	60.02	7.765	60.31	3.248
B-2	BASE	10yr-24hr	12.38	5.038	3.960	-0.0029	6625	12.03	5.901	12.44	3.316
B-2	BASE	1hr_calibrate	0.85	4.412	3.960	-0.0035	2969	0.65	3.706	0.87	2.753
B-2	BASE	25yr-72hr	60.37	5.505	3.960	0.0052	7904	60.02	6.654	60.28	2.967
B-2	BASE	5yr-24hr	12.33	4.728	3.960	-0.0031	4824	12.03	4.699	12.36	3.033
B-20	BASE	100yr-72hr	60.69	5.618	3.670	0.0064	16927	60.02	7.019	62.05	2.271
B-20	BASE	10yr-24hr	12.54	5.037	3.670	-0.0059	11928	12.03	5.334	13.22	2.906
B-20	BASE	1hr_calibrate	0.91	4.493	3.670	-0.0088	5093	0.65	3.350	1.31	2.816
B-20	BASE	25yr-72hr	60.64	5.440	3.670	0.0064	15393	60.02	6.015	61.82	2.165
B-20	BASE	5yr-24hr	12.43	4.780	3.670	-0.0069	8765	12.03	4.248	12.87	2.649
B-21	BASE	100yr-72hr	60.68	5.624	3.830	0.0064	15189	60.02	6.957	62.69	2.255
B-21	BASE	10yr-24hr	12.54	5.044	3.830	-0.0089	12028	12.03	5.287	13.27	3.051
B-21	BASE	1hr_calibrate	0.92	4.499	3.830	-0.0079	5713	0.65	3.321	1.20	2.585
B-21	BASE	25yr-72hr	60.64	5.445	3.830	0.0064	14212	60.02	5.962	62.28	2.195
B-21	BASE	5yr-24hr	12.44	4.786	3.830	-0.0088	9199	12.03	4.210	12.96	2.844
B-22	BASE	100yr-72hr	60.37	5.679	5.310	0.0090	1807	60.05	17.540	60.06	16.944
B-22	BASE	10yr-24hr	12.32	5.024	5.310	0.0081	488	12.07	15.990	12.08	15.811
B-22	BASE	1hr_calibrate	0.82	4.429	5.310	0.0072	252	0.72	13.310	1.32	14.012
B-22	BASE	25yr-72hr	60.32	5.491	5.310	0.0096	1193	60.05	16.150	60.05	15.822
B-22	BASE	5yr-24hr	12.28	4.727	5.310	0.0068	370	12.07	14.562	12.08	14.439
B-23	BASE	100yr-72hr	60.33	5.873	5.340	-0.0019	1758	60.02	2.423	59.91	1.782
B-23	BASE	10yr-24hr	12.32	5.240	5.340	-0.0039	481	12.03	1.841	12.07	1.604
B-23	BASE	1hr_calibrate	0.83	4.595	5.340	0.0026	259	0.65	1.156	0.67	1.044
B-23	BASE	25yr-72hr	60.29	5.666	5.340	-0.0019	1275	60.02	2.076	59.95	1.657
B-23	BASE	5yr-24hr	12.29	4.919	5.340	0.0031	368	12.03	1.466	12.07	1.299
B-24	BASE	100yr-72hr	60.67	6.213	4.200	0.0049	11834	60.02	6.584	61.93	1.981
B-24	BASE	10yr-24hr	12.57	5.635	4.200	-0.0060	9143	12.03	5.004	13.66	2.627
B-24	BASE	1hr_calibrate	0.93	4.979	4.200	-0.0060	5439	0.65	3.143	1.21	2.160
B-24	BASE	25yr-72hr	60.62	5.982	4.200	0.0049	11057	60.02	5.643	61.66	1.890
B-24	BASE	5yr-24hr	12.48	5.310	4.200	-0.0057	7348	12.03	3.984	13.23	2.367

Mary Brickell Village Drainage Improvements  
Node Maximum Comparison Report  
Pre Mitigation Condition

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
B-25	BASE	100yr-72hr	60.69	6.426	4.200	0.0047	16439	60.02	10.995	62.74	2.889
B-25	BASE	10yr-24hr	12.62	5.863	4.200	-0.0081	13145	12.03	8.356	13.81	4.912
B-25	BASE	1hr_calibrate	0.97	5.149	4.200	-0.0099	8413	0.65	5.248	1.41	4.608
B-25	BASE	25yr-72hr	60.64	6.177	4.200	0.0047	15043	60.02	9.422	62.33	2.780
B-25	BASE	5yr-24hr	12.54	5.518	4.200	-0.0078	10858	12.03	6.653	13.36	4.719
B-26	BASE	100yr-72hr	60.09	6.746	9.940	0.0033	114	60.02	2.236	60.03	2.141
B-26	BASE	10yr-24hr	12.05	5.926	9.940	0.0018	130	12.03	1.699	12.05	1.697
B-26	BASE	1hr_calibrate	0.66	5.719	9.940	0.0062	133	0.65	1.067	0.65	1.065
B-26	BASE	25yr-72hr	60.10	6.414	9.940	0.0029	114	60.02	1.916	60.03	1.828
B-26	BASE	5yr-24hr	12.05	5.815	9.940	-0.0007	132	12.03	1.353	12.05	1.351
B-27	BASE	100yr-72hr	60.55	7.705	5.900	0.0052	11163	60.02	10.870	61.22	3.867
B-27	BASE	10yr-24hr	12.51	6.938	5.900	-0.0094	6751	12.03	8.261	13.01	4.545
B-27	BASE	1hr_calibrate	0.91	5.843	5.900	-0.0090	4160	0.65	5.189	1.16	3.793
B-27	BASE	25yr-72hr	60.49	7.355	5.900	0.0052	8994	60.02	9.316	61.41	3.751
B-27	BASE	5yr-24hr	12.43	6.379	5.900	-0.0099	6348	12.03	6.578	12.84	4.204
B-28	BASE	100yr-72hr	60.37	7.542	5.800	0.0049	5332	60.02	5.901	59.68	3.127
B-28	BASE	10yr-24hr	12.36	6.817	5.800	-0.0069	2892	12.03	4.485	11.87	3.103
B-28	BASE	1hr_calibrate	0.77	5.769	5.800	0.0065	114	0.65	2.817	0.67	2.703
B-28	BASE	25yr-72hr	60.30	7.215	5.800	0.0049	4139	60.02	5.057	59.71	3.060
B-28	BASE	5yr-24hr	12.26	6.299	5.800	0.0050	1576	12.03	3.571	11.95	3.038
B-3	BASE	100yr-72hr	60.65	5.282	3.960	0.0054	12579	60.02	3.851	61.91	1.530
B-3	BASE	10yr-24hr	12.43	4.627	3.960	-0.0085	6677	12.03	2.927	12.81	1.706
B-3	BASE	1hr_calibrate	0.86	4.151	3.960	-0.0086	2391	0.65	1.838	0.59	1.674
B-3	BASE	25yr-72hr	60.61	5.133	3.960	0.0054	11856	60.02	3.300	61.58	1.476
B-3	BASE	5yr-24hr	12.35	4.399	3.960	-0.0065	4332	12.03	2.331	11.87	1.647
B-4	BASE	100yr-72hr	60.76	5.479	3.120	0.0048	15439	60.02	4.410	62.63	2.070
B-4	BASE	10yr-24hr	12.56	4.879	3.120	0.0025	11275	12.03	3.352	13.23	2.645
B-4	BASE	1hr_calibrate	0.92	4.380	3.120	0.0030	4936	0.65	2.105	1.20	2.131
B-4	BASE	25yr-72hr	60.70	5.324	3.120	0.0048	14650	60.02	3.780	62.22	2.011
B-4	BASE	5yr-24hr	12.45	4.650	3.120	0.0025	8030	12.03	2.669	12.94	2.328
B-5	BASE	100yr-72hr	60.78	5.508	3.690	0.0046	16423	60.02	5.963	62.76	2.269
B-5	BASE	10yr-24hr	12.59	4.933	3.690	-0.0054	12690	12.03	4.532	13.31	2.948
B-5	BASE	1hr_calibrate	0.94	4.429	3.690	-0.0072	6088	0.65	2.846	1.27	2.543
B-5	BASE	25yr-72hr	60.72	5.350	3.690	0.0046	15549	60.02	5.110	62.35	2.209
B-5	BASE	5yr-24hr	12.49	4.703	3.690	-0.0060	9549	12.03	3.609	13.02	2.722
B-6	BASE	100yr-72hr	60.65	5.705	4.870	0.0037	2437	60.02	2.174	59.74	1.459
B-6	BASE	10yr-24hr	12.44	5.176	4.870	0.0033	1142	12.03	1.652	12.00	1.534
B-6	BASE	1hr_calibrate	0.86	4.626	4.870	0.0037	113	0.65	1.038	0.67	0.979
B-6	BASE	25yr-72hr	60.60	5.542	4.870	0.0037	2037	60.02	1.863	59.78	1.377
B-6	BASE	5yr-24hr	12.35	4.924	4.870	0.0033	354	12.03	1.316	12.05	1.257
B-7	BASE	100yr-72hr	60.68	5.699	5.220	0.0038	3469	60.02	1.491	59.93	0.814
B-7	BASE	10yr-24hr	12.47	5.166	5.220	0.0038	1058	12.03	1.133	12.09	0.736
B-7	BASE	1hr_calibrate	0.87	4.617	5.220	0.0037	605	0.65	0.712	0.89	0.497



Mary Brickell Village Drainage Improvements  
Node Maximum Comparison Report  
Pre Mitigation Condition

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B-7	BASE	25yr-72hr	60.62	5.536	5.220	0.0038	2665	60.02	1.278	60.00	0.760
B-7	BASE	5yr-24hr	12.37	4.914	5.220	0.0032	850	12.03	0.902	12.13	0.597
B-8	BASE	100yr-72hr	60.68	5.791	4.900	0.0035	3873	60.02	2.360	59.72	1.484
B-8	BASE	10yr-24hr	12.48	5.291	4.900	0.0035	2073	12.03	1.794	11.96	1.558
B-8	BASE	1hr_calibrate	0.85	4.726	4.900	0.0039	114	0.65	1.127	0.66	1.059
B-8	BASE	25yr-72hr	60.62	5.624	4.900	0.0035	3272	60.02	2.023	59.76	1.414
B-8	BASE	5yr-24hr	12.37	5.032	4.900	0.0035	1141	12.03	1.428	12.06	1.366
B-9	BASE	100yr-72hr	60.72	5.789	4.860	0.0035	5914	60.02	2.298	59.71	1.391
B-9	BASE	10yr-24hr	12.51	5.291	4.860	-0.0048	3209	12.03	1.747	11.95	1.475
B-9	BASE	1hr_calibrate	0.85	4.729	4.860	0.0039	114	0.65	1.097	0.66	1.029
B-9	BASE	25yr-72hr	60.65	5.623	4.860	0.0035	5012	60.02	1.970	59.75	1.332
B-9	BASE	5yr-24hr	12.39	5.034	4.860	0.0035	1814	12.03	1.391	12.05	1.332
J-1	BASE	100yr-72hr	60.27	4.337	5.800	0.0091	214	60.27	46.750	60.27	46.750
J-1	BASE	10yr-24hr	12.29	3.293	5.800	0.0077	214	12.29	53.104	12.29	53.103
J-1	BASE	1hr_calibrate	0.82	3.107	5.800	0.0074	214	0.82	45.433	0.82	45.433
J-1	BASE	25yr-72hr	60.26	4.279	5.800	0.0091	214	60.26	44.124	60.26	44.124
J-1	BASE	5yr-24hr	12.25	3.201	5.800	0.0077	214	12.25	49.446	12.25	49.446
J-10	BASE	100yr-72hr	60.38	5.747	5.860	-0.0083	133	60.53	11.719	60.54	11.725
J-10	BASE	10yr-24hr	12.32	5.094	5.860	-0.0088	133	12.66	12.187	12.71	12.224
J-10	BASE	1hr_calibrate	0.82	4.485	5.860	0.0072	133	0.92	10.659	1.32	11.125
J-10	BASE	25yr-72hr	60.33	5.553	5.860	0.0082	133	60.44	11.184	60.46	11.188
J-10	BASE	5yr-24hr	12.29	4.790	5.860	-0.0089	133	12.51	11.467	12.52	11.507
J-11	BASE	100yr-72hr	60.43	5.847	5.950	0.0051	133	62.81	5.573	61.93	5.122
J-11	BASE	10yr-24hr	12.34	5.210	5.950	0.0076	133	13.20	7.015	13.67	7.026
J-11	BASE	1hr_calibrate	0.83	4.586	5.950	0.0040	134	1.33	5.824	1.34	6.116
J-11	BASE	25yr-72hr	60.36	5.643	5.950	0.0051	133	62.33	5.432	62.41	4.984
J-11	BASE	5yr-24hr	12.30	4.898	5.950	0.0028	133	13.25	6.485	13.25	6.664
J-12	BASE	100yr-72hr	60.59	6.101	4.650	0.0047	131	62.43	4.836	62.47	4.861
J-12	BASE	10yr-24hr	12.47	5.486	4.650	-0.0053	131	13.69	6.569	13.69	6.674
J-12	BASE	1hr_calibrate	0.89	4.843	4.650	0.0035	131	1.31	5.313	1.34	5.522
J-12	BASE	25yr-72hr	60.56	5.877	4.650	0.0047	131	62.27	4.639	62.33	4.682
J-12	BASE	5yr-24hr	12.39	5.169	4.650	0.0048	131	13.25	6.074	13.26	6.232
J-13	BASE	100yr-72hr	60.26	6.539	10.080	0.0058	146	60.09	7.246	60.11	7.203
J-13	BASE	10yr-24hr	12.33	5.840	10.080	0.0038	150	12.33	6.863	12.37	6.868
J-13	BASE	1hr_calibrate	0.82	5.029	10.080	0.0047	164	0.78	5.871	0.81	5.860
J-13	BASE	25yr-72hr	60.25	6.279	10.080	0.0058	146	60.11	6.858	60.14	6.832
J-13	BASE	5yr-24hr	12.29	5.433	10.080	0.0037	153	12.28	6.374	12.32	6.375
J-14	BASE	100yr-72hr	60.42	7.161	6.500	0.0047	131	60.69	6.166	60.70	6.189
J-14	BASE	10yr-24hr	12.39	6.431	6.500	0.0044	131	12.63	6.067	12.65	6.106
J-14	BASE	1hr_calibrate	0.83	5.460	6.500	-0.0049	131	0.85	4.998	0.88	5.016
J-14	BASE	25yr-72hr	60.35	6.856	6.500	0.0047	131	60.53	5.874	60.61	5.892
J-14	BASE	5yr-24hr	12.33	5.949	6.500	0.0042	131	12.45	5.554	12.47	5.586

Mary Brickell Village Drainage Improvements  
Node Maximum Comparison Report  
Pre Mitigation Condition

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J-2	BASE	100yr-72hr	60.27	4.812	5.000	0.0081	171	60.26	46.752	60.27	46.750
J-2	BASE	10yr-24hr	12.29	3.906	5.000	0.0097	171	12.28	53.105	12.29	53.104
J-2	BASE	1hr_calibrate	0.82	3.556	5.000	0.0089	171	0.82	45.433	0.82	45.433
J-2	BASE	25yr-72hr	60.26	4.702	5.000	0.0081	171	60.26	44.126	60.26	44.124
J-2	BASE	5yr-24hr	12.25	3.732	5.000	0.0100	171	12.25	49.446	12.25	49.446
J-3	BASE	100yr-72hr	60.54	5.228	4.200	-0.0090	137	61.13	17.360	61.13	17.372
J-3	BASE	10yr-24hr	12.36	4.499	4.200	0.0099	137	12.84	21.340	12.83	21.372
J-3	BASE	1hr_calibrate	0.84	4.039	4.200	-0.0099	137	1.01	18.746	1.35	19.881
J-3	BASE	25yr-72hr	60.49	5.083	4.200	-0.0088	137	60.98	16.604	60.98	16.616
J-3	BASE	5yr-24hr	12.32	4.276	4.200	-0.0098	137	12.63	20.067	12.62	20.101
J-4	BASE	100yr-72hr	60.65	5.453	4.600	0.0071	160	61.36	13.798	61.36	13.814
J-4	BASE	10yr-24hr	12.45	4.823	4.600	0.0026	160	12.91	16.700	12.92	16.741
J-4	BASE	1hr_calibrate	0.87	4.327	4.600	0.0032	160	1.09	14.980	1.09	15.048
J-4	BASE	25yr-72hr	60.61	5.300	4.600	0.0071	160	61.07	13.128	61.07	13.143
J-4	BASE	5yr-24hr	12.37	4.592	4.600	0.0026	160	12.87	15.801	12.87	15.896
J-5	BASE	100yr-72hr	60.63	5.693	5.300	-0.0097	147	60.07	11.141	60.08	11.086
J-5	BASE	10yr-24hr	12.48	5.149	5.300	0.0043	147	12.69	12.855	12.71	12.874
J-5	BASE	1hr_calibrate	0.87	4.602	5.300	0.0065	147	0.83	11.696	0.85	11.686
J-5	BASE	25yr-72hr	60.62	5.529	5.300	-0.0099	147	60.08	10.887	60.08	10.838
J-5	BASE	5yr-24hr	12.38	4.898	5.300	0.0042	147	12.44	12.322	12.45	12.331
J-6	BASE	100yr-72hr	60.69	5.775	5.200	0.0096	138	60.63	10.304	60.91	10.144
J-6	BASE	10yr-24hr	12.50	5.258	5.200	0.0037	138	12.76	11.843	12.76	11.865
J-6	BASE	1hr_calibrate	0.87	4.693	5.200	0.0038	138	0.90	10.462	0.91	10.476
J-6	BASE	25yr-72hr	60.63	5.608	5.200	-0.0099	138	60.52	9.898	60.74	9.828
J-6	BASE	5yr-24hr	12.39	4.998	5.200	0.0034	138	12.27	11.217	12.53	11.214
J-7	BASE	100yr-72hr	60.71	5.904	4.400	-0.0065	137	60.79	9.038	60.63	9.145
J-7	BASE	10yr-24hr	12.54	5.417	4.400	0.0085	137	12.73	10.272	12.74	10.292
J-7	BASE	1hr_calibrate	0.89	4.820	4.400	0.0086	137	0.99	9.219	1.00	9.264
J-7	BASE	25yr-72hr	60.63	5.730	4.400	0.0059	137	60.67	8.740	60.52	8.767
J-7	BASE	5yr-24hr	12.41	5.142	4.400	0.0075	137	12.67	9.804	12.67	9.853
J-8	BASE	100yr-72hr	60.51	5.460	4.860	-0.0100	132	61.81	5.156	62.05	6.861
J-8	BASE	10yr-24hr	12.35	4.785	4.860	0.0100	132	13.27	6.495	13.22	7.896
J-8	BASE	1hr_calibrate	0.83	4.253	4.860	-0.0099	132	1.21	5.634	0.46	8.189
J-8	BASE	25yr-72hr	60.47	5.294	4.860	0.0100	132	61.62	4.937	61.82	6.110
J-8	BASE	5yr-24hr	12.30	4.524	4.860	-0.0100	132	12.98	6.133	12.87	8.248
J-9	BASE	100yr-72hr	60.66	5.597	4.000	0.0060	130	62.53	4.472	62.30	4.544
J-9	BASE	10yr-24hr	12.50	4.999	4.000	-0.0058	130	13.22	5.941	13.25	6.015
J-9	BASE	1hr_calibrate	0.90	4.460	4.000	-0.0084	130	1.19	5.007	1.21	5.123
J-9	BASE	25yr-72hr	60.62	5.420	4.000	0.0060	130	62.23	4.328	61.85	4.377
J-9	BASE	5yr-24hr	12.40	4.743	4.000	-0.0072	130	12.93	5.466	12.93	5.573
WATERWAY	BASE	100yr-72hr	0.00	3.800	2.600	1.2000	56	60.27	46.750	0.00	0.000
WATERWAY	BASE	10yr-24hr	0.00	2.600	2.600	0.0000	56	12.29	53.103	0.00	0.000
WATERWAY	BASE	1hr_calibrate	0.00	2.600	2.600	0.0000	56	0.82	45.433	0.00	0.000

Mary Brickell Village Drainage Improvements  
Node Maximum Comparison Report  
Pre Mitigation Condition

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
WATERWAY	BASE	25yr-72hr	0.00	3.800	2.600	1.2000	56	60.26	44.124	0.00	0.000
WATERWAY	BASE	5yr-24hr	0.00	2.600	2.600	0.0000	56	12.25	49.446	0.00	0.000

Mary Brickell Village Drainage Improvements  
 Link Maximum Comparison Report  
 Pre Mitigation Condition

Name	Group	Simulation	Max Time Flow hrs	Max Flow cfs	Max Delta Q cfs	Max Time US Stage hrs	Max US Stage ft	Max Time DS Stage hrs	Max DS Stage ft
B1-J2	BASE	100yr-72hr	60.82	38.658	8.122	60.50	5.171	60.27	4.812
B1-J2	BASE	10yr-24hr	12.53	44.565	9.656	12.34	4.419	12.29	3.906
B1-J2	BASE	1hr_calibrate	0.87	39.454	9.398	0.83	3.969	0.82	3.556
B1-J2	BASE	25yr-72hr	60.75	36.784	8.126	60.45	5.032	60.26	4.702
B1-J2	BASE	5yr-24hr	12.39	42.134	-11.522	12.30	4.199	12.25	3.732
B10-J7	BASE	100yr-72hr	62.66	2.518	0.551	60.85	5.920	60.71	5.904
B10-J7	BASE	10yr-24hr	13.55	3.545	1.103	12.65	5.449	12.54	5.417
B10-J7	BASE	1hr_calibrate	1.26	2.893	-1.077	0.95	4.856	0.89	4.820
B10-J7	BASE	25yr-72hr	62.22	2.392	0.389	60.75	5.747	60.63	5.730
B10-J7	BASE	5yr-24hr	13.14	3.286	1.103	12.52	5.178	12.41	5.142
B11-J7	BASE	100yr-72hr	62.66	2.450	0.445	60.85	5.935	60.71	5.904
B11-J7	BASE	10yr-24hr	13.44	3.366	-0.256	12.66	5.474	12.54	5.417
B11-J7	BASE	1hr_calibrate	1.28	2.889	-0.343	0.96	4.886	0.89	4.820
B11-J7	BASE	25yr-72hr	62.13	2.316	0.366	60.75	5.762	60.63	5.730
B11-J7	BASE	5yr-24hr	13.13	3.133	-0.427	12.53	5.207	12.41	5.142
B12-J7	BASE	100yr-72hr	60.12	9.983	2.789	60.60	6.046	60.71	5.904
B12-J7	BASE	10yr-24hr	12.11	9.364	0.540	12.49	5.572	12.54	5.417
B12-J7	BASE	1hr_calibrate	0.74	7.621	0.610	0.87	4.934	0.89	4.820
B12-J7	BASE	25yr-72hr	60.10	9.486	2.080	60.56	5.857	60.63	5.730
B12-J7	BASE	5yr-24hr	12.15	8.638	0.897	12.38	5.279	12.41	5.142
B13-B12	BASE	100yr-72hr	60.05	8.053	0.966	60.44	6.287	60.60	6.046
B13-B12	BASE	10yr-24hr	12.05	7.754	0.328	12.39	5.799	12.49	5.572
B13-B12	BASE	1hr_calibrate	0.68	6.263	-0.385	0.83	5.084	0.87	4.934
B13-B12	BASE	25yr-72hr	60.03	7.806	0.966	60.35	6.075	60.56	5.857
B13-B12	BASE	5yr-24hr	12.06	7.273	-0.855	12.32	5.469	12.38	5.279
B14-B13	BASE	100yr-72hr	60.12	7.143	0.428	60.30	6.690	60.44	6.287
B14-B13	BASE	10yr-24hr	12.05	6.890	-0.311	12.33	6.161	12.39	5.799
B14-B13	BASE	1hr_calibrate	0.68	5.756	0.237	0.78	5.330	0.83	5.084
B14-B13	BASE	25yr-72hr	60.10	6.879	0.428	60.25	6.448	60.35	6.075
B14-B13	BASE	5yr-24hr	12.05	6.601	-0.417	12.23	5.776	12.32	5.469
B15-B14	BASE	100yr-72hr	59.70	1.931	0.046	60.38	6.808	60.30	6.690
B15-B14	BASE	10yr-24hr	11.90	1.945	-0.113	12.35	6.296	12.33	6.161
B15-B14	BASE	1hr_calibrate	0.68	1.570	-0.153	0.76	5.440	0.78	5.330
B15-B14	BASE	25yr-72hr	59.73	1.895	0.046	60.30	6.568	60.25	6.448
B15-B14	BASE	5yr-24hr	11.99	1.885	-0.240	12.20	5.915	12.23	5.776
B16-B14	BASE	100yr-72hr	60.18	3.530	0.020	60.22	7.754	60.30	6.690
B16-B14	BASE	10yr-24hr	12.23	3.048	0.051	12.29	6.954	12.33	6.161
B16-B14	BASE	1hr_calibrate	0.75	2.397	-0.054	0.77	5.826	0.78	5.330
B16-B14	BASE	25yr-72hr	60.16	3.272	0.020	60.19	7.367	60.25	6.448
B16-B14	BASE	5yr-24hr	12.19	2.709	0.060	12.20	6.411	12.23	5.776
B17-B16	BASE	100yr-72hr	60.19	1.672	0.021	60.22	7.916	60.22	7.754
B17-B16	BASE	10yr-24hr	12.24	1.444	0.273	12.29	7.074	12.29	6.954
B17-B16	BASE	1hr_calibrate	0.76	1.134	0.277	0.77	5.900	0.77	5.826

Mary Brickell Village Drainage Improvements  
 Link Maximum Comparison Report  
 Pre Mitigation Condition

Name	Group	Simulation	Max Flow hrs	Max Flow cfs	Max Delta Q cfs	Max US Stage hrs	Max US Stage ft	Max DS Stage hrs	Max DS Stage ft
B17-B16	BASE	25yr-72hr	60.17	1.550	0.021	60.19	7.506	60.19	7.367
B17-B16	BASE	5yr-24hr	12.20	1.282	0.277	12.20	6.506	12.20	6.411
B18-B1	BASE	100yr-72hr	60.51	19.269	4.049	60.51	5.453	60.50	5.171
B18-B1	BASE	10yr-24hr	12.36	21.626	5.510	12.34	4.774	12.34	4.419
B18-B1	BASE	1hr_calibrate	0.81	19.040	5.087	0.84	4.243	0.83	3.969
B18-B1	BASE	25yr-72hr	60.38	18.328	-4.023	60.44	5.286	60.45	5.032
B18-B1	BASE	5yr-24hr	12.28	20.336	5.444	12.30	4.513	12.30	4.199
B19-J8	BASE	100yr-72hr	59.67	1.167	0.609	60.53	5.504	60.51	5.460
B19-J8	BASE	10yr-24hr	11.94	1.498	0.591	12.33	4.871	12.35	4.785
B19-J8	BASE	1hr_calibrate	0.70	1.146	0.608	0.81	4.307	0.83	4.253
B19-J8	BASE	25yr-72hr	59.69	1.157	0.599	60.45	5.334	60.47	5.294
B19-J8	BASE	5yr-24hr	12.01	1.428	0.621	12.25	4.591	12.30	4.524
B2-J3	BASE	100yr-72hr	60.31	3.248	0.599	60.41	5.732	60.54	5.228
B2-J3	BASE	10yr-24hr	12.44	3.316	0.395	12.38	5.038	12.36	4.499
B2-J3	BASE	1hr_calibrate	0.87	2.753	0.625	0.85	4.412	0.84	4.039
B2-J3	BASE	25yr-72hr	60.28	2.967	0.594	60.37	5.505	60.49	5.083
B2-J3	BASE	5yr-24hr	12.36	3.033	0.394	12.33	4.728	12.32	4.276
B20-J9	BASE	100yr-72hr	62.05	2.271	-1.117	60.69	5.618	60.66	5.597
B20-J9	BASE	10yr-24hr	13.22	2.906	0.937	12.54	5.037	12.50	4.999
B20-J9	BASE	1hr_calibrate	1.31	2.816	-1.112	0.91	4.493	0.90	4.460
B20-J9	BASE	25yr-72hr	61.82	2.165	-1.117	60.64	5.440	60.62	5.420
B20-J9	BASE	5yr-24hr	12.87	2.649	0.879	12.43	4.780	12.40	4.743
B21-J9	BASE	100yr-72hr	62.69	2.255	-0.860	60.68	5.624	60.66	5.597
B21-J9	BASE	10yr-24hr	13.27	3.051	1.275	12.54	5.044	12.50	4.999
B21-J9	BASE	1hr_calibrate	1.20	2.585	-1.386	0.92	4.499	0.90	4.460
B21-J9	BASE	25yr-72hr	62.28	2.195	-0.860	60.64	5.445	60.62	5.420
B21-J9	BASE	5yr-24hr	12.96	2.844	1.083	12.44	4.786	12.40	4.743
B22-B18	BASE	100yr-72hr	60.06	16.944	4.639	60.37	5.679	60.51	5.453
B22-B18	BASE	10yr-24hr	12.08	15.811	2.859	12.32	5.024	12.34	4.774
B22-B18	BASE	1hr_calibrate	1.32	14.012	2.829	0.82	4.429	0.84	4.243
B22-B18	BASE	25yr-72hr	60.05	15.822	4.640	60.32	5.491	60.44	5.286
B22-B18	BASE	5yr-24hr	12.08	14.439	2.712	12.28	4.727	12.30	4.513
B23-J11	BASE	100yr-72hr	59.91	1.782	0.601	60.33	5.873	60.43	5.847
B23-J11	BASE	10yr-24hr	12.07	1.604	0.744	12.32	5.240	12.34	5.210
B23-J11	BASE	1hr_calibrate	0.67	1.044	-0.023	0.83	4.595	0.83	4.586
B23-J11	BASE	25yr-72hr	59.95	1.657	0.606	60.29	5.666	60.36	5.643
B23-J11	BASE	5yr-24hr	12.07	1.299	-0.242	12.29	4.919	12.30	4.898
B24-J12	BASE	100yr-72hr	61.93	1.981	0.109	60.67	6.213	60.59	6.101
B24-J12	BASE	10yr-24hr	13.66	2.627	-0.818	12.57	5.635	12.47	5.486
B24-J12	BASE	1hr_calibrate	1.21	2.160	-0.652	0.93	4.979	0.89	4.843
B24-J12	BASE	25yr-72hr	61.66	1.890	0.109	60.62	5.982	60.56	5.877
B24-J12	BASE	5yr-24hr	13.23	2.367	-0.816	12.48	5.310	12.39	5.169



Mary Brickell Village Drainage Improvements  
 Link Maximum Comparison Report  
 Pre Mitigation Condition

Name	Group	Simulation	Max Time Flow hrs	Max Flow cfs	Max Delta Q cfs	Max Time US Stage hrs	Max US Stage ft	Max Time DS Stage hrs	Max DS Stage ft
B25-J12	BASE	100yr-72hr	62.74	2.889	0.104	60.69	6.426	60.59	6.101
B25-J12	BASE	10yr-24hr	13.81	4.912	-0.380	12.62	5.863	12.47	5.486
B25-J12	BASE	1hr_calibrate	1.41	4.608	-0.092	0.97	5.149	0.89	4.843
B25-J12	BASE	25yr-72hr	62.33	2.780	0.104	60.64	6.177	60.56	5.877
B25-J12	BASE	5yr-24hr	13.36	4.719	-0.381	12.54	5.518	12.39	5.169
B26-J13	BASE	100yr-72hr	60.03	2.141	-0.419	60.09	6.746	60.26	6.539
B26-J13	BASE	10yr-24hr	12.05	1.697	-0.136	12.05	5.926	12.33	5.840
B26-J13	BASE	1hr_calibrate	0.65	1.065	0.008	0.66	5.719	0.65	4.756
B26-J13	BASE	25yr-72hr	60.03	1.828	-0.384	60.10	6.414	60.25	6.279
B26-J13	BASE	5yr-24hr	12.05	1.351	-0.003	12.05	5.815	12.29	5.433
B27-J14	BASE	100yr-72hr	61.22	3.867	-0.086	60.55	7.705	60.42	7.161
B27-J14	BASE	10yr-24hr	13.01	4.545	-0.699	12.51	6.938	12.39	6.431
B27-J14	BASE	1hr_calibrate	1.16	3.793	-0.716	0.91	5.843	0.83	5.460
B27-J14	BASE	25yr-72hr	61.41	3.751	-0.069	60.49	7.355	60.35	6.856
B27-J14	BASE	5yr-24hr	12.84	4.204	-0.723	12.43	6.379	12.33	5.949
B28-J14	BASE	100yr-72hr	59.68	3.127	-0.063	60.37	7.542	60.42	7.161
B28-J14	BASE	10yr-24hr	11.87	3.103	-0.333	12.36	6.817	12.39	6.431
B28-J14	BASE	1hr_calibrate	0.67	2.703	-0.394	0.77	5.769	0.83	5.460
B28-J14	BASE	25yr-72hr	59.71	3.060	-0.063	60.30	7.215	60.35	6.856
B28-J14	BASE	5yr-24hr	11.95	3.038	-0.345	12.26	6.299	12.33	5.949
B3-J3	BASE	100yr-72hr	61.91	1.530	0.542	60.65	5.282	60.54	5.228
B3-J3	BASE	10yr-24hr	12.81	1.706	0.570	12.43	4.627	12.36	4.499
B3-J3	BASE	1hr_calibrate	0.59	1.674	0.554	0.86	4.151	0.84	4.039
B3-J3	BASE	25yr-72hr	61.58	1.476	0.537	60.61	5.133	60.49	5.083
B3-J3	BASE	5yr-24hr	11.87	1.647	0.576	12.35	4.399	12.32	4.276
B4-J4	BASE	100yr-72hr	62.63	2.070	0.418	60.76	5.479	60.65	5.453
B4-J4	BASE	10yr-24hr	13.23	2.645	0.281	12.56	4.879	12.45	4.823
B4-J4	BASE	1hr_calibrate	1.20	2.131	-0.346	0.92	4.380	0.87	4.327
B4-J4	BASE	25yr-72hr	62.22	2.011	0.417	60.70	5.324	60.61	5.300
B4-J4	BASE	5yr-24hr	12.94	2.328	-0.325	12.45	4.650	12.37	4.592
B5-J4	BASE	100yr-72hr	62.76	2.269	0.377	60.78	5.508	60.65	5.453
B5-J4	BASE	10yr-24hr	13.31	2.948	0.382	12.59	4.933	12.45	4.823
B5-J4	BASE	1hr_calibrate	1.27	2.543	-0.448	0.94	4.429	0.87	4.327
B5-J4	BASE	25yr-72hr	62.35	2.209	0.377	60.72	5.350	60.61	5.300
B5-J4	BASE	5yr-24hr	13.02	2.722	-0.483	12.49	4.703	12.37	4.592
B6-J5	BASE	100yr-72hr	59.74	1.459	0.603	60.65	5.705	60.63	5.693
B6-J5	BASE	10yr-24hr	12.00	1.534	0.145	12.44	5.176	12.48	5.149
B6-J5	BASE	1hr_calibrate	0.67	0.979	0.324	0.86	4.626	0.87	4.602
B6-J5	BASE	25yr-72hr	59.78	1.377	0.599	60.60	5.542	60.62	5.529
B6-J5	BASE	5yr-24hr	12.05	1.257	-0.392	12.35	4.924	12.38	4.898
B7-J5	BASE	100yr-72hr	59.93	0.814	0.482	60.68	5.699	60.63	5.693
B7-J5	BASE	10yr-24hr	12.09	0.736	0.156	12.47	5.166	12.48	5.149
B7-J5	BASE	1hr_calibrate	0.89	0.497	-0.345	0.87	4.617	0.87	4.602

Mary Brickell Village Drainage Improvements  
 Link Maximum Comparison Report  
 Pre Mitigation Condition

Name	Group	Simulation	Max Time Flow hrs	Max Flow cfs	Max Delta Q cfs	Max Time US Stage hrs	Max US Stage ft	Max Time DS Stage hrs	Max DS Stage ft
B7-J5	BASE	25yr-72hr	60.00	0.760	0.483	60.62	5.536	60.62	5.529
B7-J5	BASE	5yr-24hr	12.13	0.597	-0.237	12.37	4.914	12.38	4.898
B8-J6	BASE	100yr-72hr	59.72	1.484	0.612	60.68	5.791	60.69	5.775
B8-J6	BASE	10yr-24hr	11.96	1.558	0.156	12.48	5.291	12.50	5.258
B8-J6	BASE	1hr_calibrate	0.66	1.059	0.168	0.85	4.726	0.87	4.693
B8-J6	BASE	25yr-72hr	59.76	1.414	0.605	60.62	5.624	60.63	5.608
B8-J6	BASE	5yr-24hr	12.06	1.366	0.189	12.37	5.032	12.39	4.998
B9-J6	BASE	100yr-72hr	59.71	1.391	0.563	60.72	5.789	60.69	5.775
B9-J6	BASE	10yr-24hr	11.95	1.475	0.144	12.51	5.291	12.50	5.258
B9-J6	BASE	1hr_calibrate	0.66	1.029	0.156	0.85	4.729	0.87	4.693
B9-J6	BASE	25yr-72hr	59.75	1.332	0.563	60.65	5.623	60.63	5.608
B9-J6	BASE	5yr-24hr	12.05	1.332	0.175	12.39	5.034	12.39	4.998
J1-WW	BASE	100yr-72hr	60.27	46.750	-69.873	60.27	4.337	0.00	3.800
J1-WW	BASE	10yr-24hr	12.29	53.103	7.754	12.29	3.293	0.00	2.600
J1-WW	BASE	1hr_calibrate	0.82	45.433	7.575	0.82	3.107	0.00	2.600
J1-WW	BASE	25yr-72hr	60.26	44.124	-69.873	60.26	4.279	0.00	3.800
J1-WW	BASE	5yr-24hr	12.25	49.446	7.755	12.25	3.201	0.00	2.600
J10-B22	BASE	100yr-72hr	60.54	11.725	7.706	60.38	5.747	60.37	5.679
J10-B22	BASE	10yr-24hr	12.71	12.224	4.995	12.32	5.094	12.32	5.024
J10-B22	BASE	1hr_calibrate	1.32	11.125	3.877	0.82	4.485	0.82	4.429
J10-B22	BASE	25yr-72hr	60.46	11.188	7.740	60.33	5.553	60.32	5.491
J10-B22	BASE	5yr-24hr	12.52	11.507	3.300	12.29	4.790	12.28	4.727
J11-J10	BASE	100yr-72hr	61.93	5.122	2.054	60.43	5.847	60.38	5.747
J11-J10	BASE	10yr-24hr	13.67	7.026	-2.169	12.34	5.210	12.32	5.094
J11-J10	BASE	1hr_calibrate	1.34	6.116	1.166	0.83	4.586	0.82	4.485
J11-J10	BASE	25yr-72hr	62.41	4.984	2.055	60.36	5.643	60.33	5.553
J11-J10	BASE	5yr-24hr	13.25	6.664	0.573	12.30	4.898	12.29	4.790
J12-J11	BASE	100yr-72hr	62.47	4.861	-0.354	60.59	6.101	60.43	5.847
J12-J11	BASE	10yr-24hr	13.69	6.674	0.793	12.47	5.486	12.34	5.210
J12-J11	BASE	1hr_calibrate	1.34	5.522	0.820	0.89	4.843	0.83	4.586
J12-J11	BASE	25yr-72hr	62.33	4.682	-0.354	60.56	5.877	60.36	5.643
J12-J11	BASE	5yr-24hr	13.26	6.232	0.759	12.39	5.169	12.30	4.898
J13-J10	BASE	100yr-72hr	60.11	7.203	0.749	60.26	6.539	60.38	5.747
J13-J10	BASE	10yr-24hr	12.37	6.868	-1.059	12.33	5.840	12.32	5.094
J13-J10	BASE	1hr_calibrate	0.81	5.860	0.614	0.82	5.029	0.82	4.485
J13-J10	BASE	25yr-72hr	60.14	6.832	0.752	60.25	6.279	60.33	5.553
J13-J10	BASE	5yr-24hr	12.32	6.375	0.389	12.29	5.433	12.29	4.790
J14-J13	BASE	100yr-72hr	60.70	6.189	-0.296	60.42	7.161	60.26	6.539
J14-J13	BASE	10yr-24hr	12.65	6.106	-0.275	12.39	6.431	12.33	5.840
J14-J13	BASE	1hr_calibrate	0.88	5.016	-0.308	0.83	5.460	0.82	5.029
J14-J13	BASE	25yr-72hr	60.61	5.892	-0.296	60.35	6.856	60.25	6.279
J14-J13	BASE	5yr-24hr	12.47	5.586	-0.286	12.33	5.949	12.29	5.433

Mary Brickell Village Drainage Improvements  
 Link Maximum Comparison Report  
 Pre Mitigation Condition

Name	Group	Simulation	Max Flow hrs	Max Flow cfs	Max Delta Q cfs	Max US Stage hrs	Max US Stage ft	Max DS Stage hrs	Max DS Stage ft
J2-J1	BASE	100yr-72hr	60.27	46.750	-9.877	60.27	4.812	60.27	4.337
J2-J1	BASE	10yr-24hr	12.29	53.104	12.299	12.29	3.906	12.29	3.293
J2-J1	BASE	1hr_calibrate	0.82	45.433	12.046	0.82	3.556	0.82	3.107
J2-J1	BASE	25yr-72hr	60.26	44.124	-9.877	60.26	4.702	60.26	4.279
J2-J1	BASE	5yr-24hr	12.25	49.446	12.297	12.25	3.732	12.25	3.201
J3-B1	BASE	100yr-72hr	61.13	17.372	8.605	60.54	5.228	60.50	5.171
J3-B1	BASE	10yr-24hr	12.83	21.372	14.822	12.36	4.499	12.34	4.419
J3-B1	BASE	1hr_calibrate	1.35	19.881	-15.855	0.84	4.039	0.83	3.969
J3-B1	BASE	25yr-72hr	60.98	16.616	8.496	60.49	5.083	60.45	5.032
J3-B1	BASE	5yr-24hr	12.62	20.101	13.787	12.32	4.276	12.30	4.199
J4-J3	BASE	100yr-72hr	61.36	13.814	4.064	60.65	5.453	60.54	5.228
J4-J3	BASE	10yr-24hr	12.92	16.741	2.984	12.45	4.823	12.36	4.499
J4-J3	BASE	1hr_calibrate	1.09	15.048	2.934	0.87	4.327	0.84	4.039
J4-J3	BASE	25yr-72hr	61.07	13.143	4.001	60.61	5.300	60.49	5.083
J4-J3	BASE	5yr-24hr	12.87	15.896	-3.835	12.37	4.592	12.32	4.276
J5-J4	BASE	100yr-72hr	60.08	11.086	2.869	60.63	5.693	60.65	5.453
J5-J4	BASE	10yr-24hr	12.71	12.874	1.424	12.48	5.149	12.45	4.823
J5-J4	BASE	1hr_calibrate	0.85	11.686	1.688	0.87	4.602	0.87	4.327
J5-J4	BASE	25yr-72hr	60.08	10.838	2.866	60.62	5.529	60.61	5.300
J5-J4	BASE	5yr-24hr	12.45	12.331	1.512	12.38	4.898	12.37	4.592
J6-J5	BASE	100yr-72hr	60.91	10.144	6.090	60.69	5.775	60.63	5.693
J6-J5	BASE	10yr-24hr	12.76	11.865	1.901	12.50	5.258	12.48	5.149
J6-J5	BASE	1hr_calibrate	0.91	10.476	0.884	0.87	4.693	0.87	4.602
J6-J5	BASE	25yr-72hr	60.74	9.828	4.164	60.63	5.608	60.62	5.529
J6-J5	BASE	5yr-24hr	12.53	11.214	1.903	12.39	4.998	12.38	4.898
J7-J6	BASE	100yr-72hr	60.63	9.145	3.133	60.71	5.904	60.69	5.775
J7-J6	BASE	10yr-24hr	12.74	10.292	1.440	12.54	5.417	12.50	5.258
J7-J6	BASE	1hr_calibrate	1.00	9.264	1.511	0.89	4.820	0.87	4.693
J7-J6	BASE	25yr-72hr	60.52	8.767	4.385	60.63	5.730	60.63	5.608
J7-J6	BASE	5yr-24hr	12.67	9.853	1.573	12.41	5.142	12.39	4.998
J8-B18	BASE	100yr-72hr	62.05	6.861	-7.968	60.51	5.460	60.51	5.453
J8-B18	BASE	10yr-24hr	13.22	7.896	7.935	12.35	4.785	12.34	4.774
J8-B18	BASE	1hr_calibrate	0.46	8.189	6.108	0.83	4.253	0.84	4.243
J8-B18	BASE	25yr-72hr	61.82	6.110	-7.968	60.47	5.294	60.44	5.286
J8-B18	BASE	5yr-24hr	12.87	8.248	8.183	12.30	4.524	12.30	4.513
J9-J8	BASE	100yr-72hr	62.30	4.544	1.306	60.66	5.597	60.51	5.460
J9-J8	BASE	10yr-24hr	13.25	6.015	-1.305	12.50	4.999	12.35	4.785
J9-J8	BASE	1hr_calibrate	1.21	5.123	-0.877	0.90	4.460	0.83	4.253
J9-J8	BASE	25yr-72hr	61.85	4.377	1.303	60.62	5.420	60.47	5.294
J9-J8	BASE	5yr-24hr	12.93	5.573	1.172	12.40	4.743	12.30	4.524

## **APPENDIX G – ICPR POST-DEVELOPMENT MODEL**

- NODE-LINK DIAGRAM
- COMPLETE INPUT REPORT
- NODE MAXIMUM CONDITIONS REPORT
- LINK MAXIMUM CONDITIONS REPORT

Mary Brickell Village Drainage Improvements  
 Final Design  
 Node-Link Diagram

Nodes

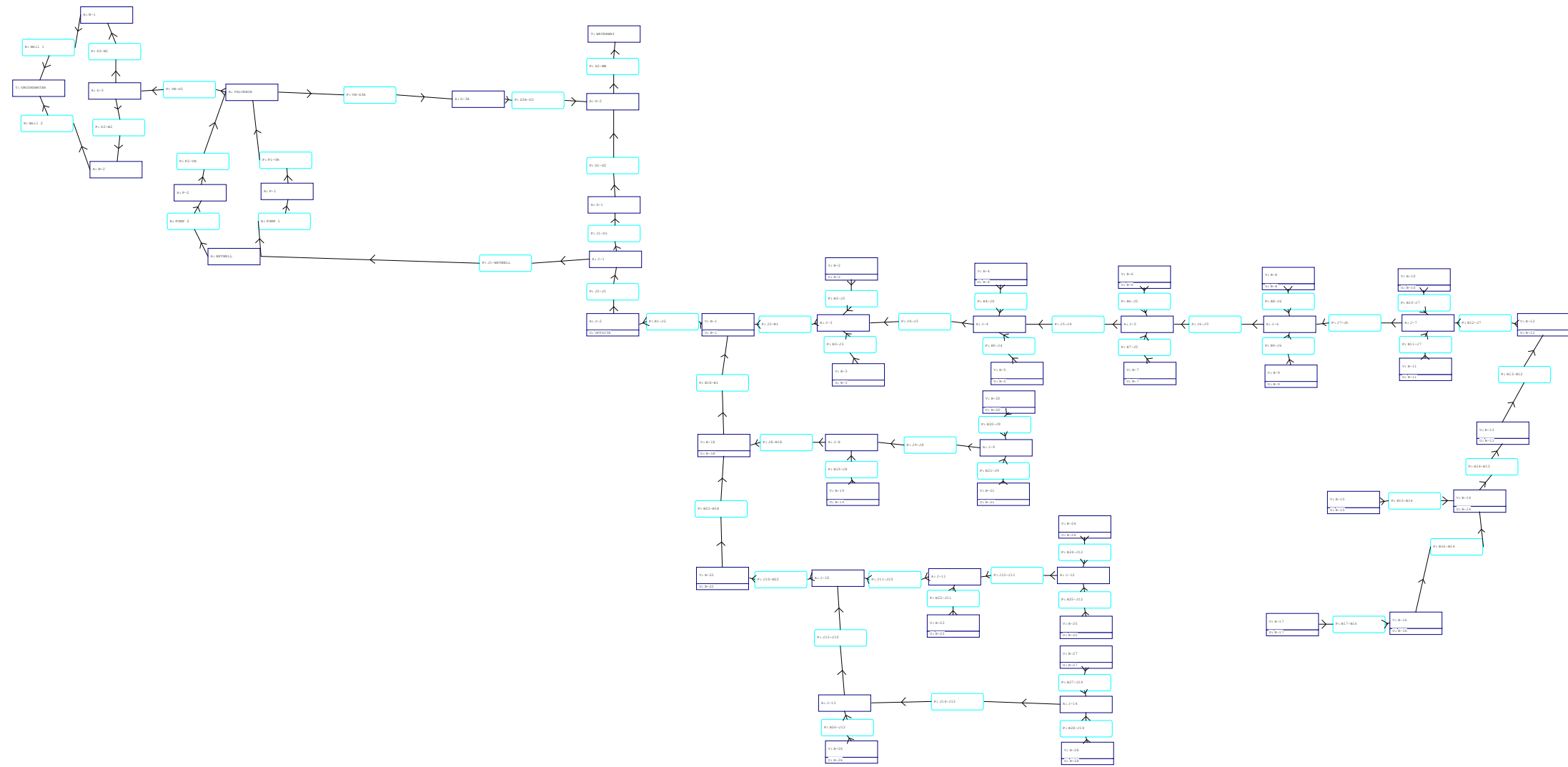
- A Stage/Area
- V Stage/Volume
- T Time/Stage
- M Manhole

Basins

- O Overland Flow
- U SCS Unit CN
- S SBUH CN
- Y SCS Unit GA
- Z SBUH GA

Links

- P Pipe
- W Weir
- C Channel
- D Drop Structure
- B Bridge
- R Rating Curve
- H Breach
- E Percolation
- F Filter
- X Exfil Trench







---

Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.560	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-16	Node: B-16	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.490	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-17	Node: B-17	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.440	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-18	Node: B-18	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.600	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-19	Node: B-19	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 0.400	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-2	Node: b-2	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 1.250	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

---

Name: B-20	Node: B-20	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	

Unit Hydrograph: Uh256	Peaking Factor: 256.0
Rainfall File:	Storm Duration(hrs): 0.00
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00
Area(ac): 1.130	Time Shift(hrs): 0.00
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000
DCIA(%): 0.00	

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---

Name: B-21	Node: B-21	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh256	Peaking Factor: 256.0	
Rainfall File:	Storm Duration(hrs): 0.00	
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00	
Area(ac): 1.120	Time Shift(hrs): 0.00	
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000	
DCIA(%): 0.00		

---

Name: B-22	Node: B-22	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh256	Peaking Factor: 256.0	
Rainfall File:	Storm Duration(hrs): 0.00	
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00	
Area(ac): 1.090	Time Shift(hrs): 0.00	
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000	
DCIA(%): 0.00		

---

Name: B-23	Node: B-23	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh256	Peaking Factor: 256.0	
Rainfall File:	Storm Duration(hrs): 0.00	
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00	
Area(ac): 0.390	Time Shift(hrs): 0.00	
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000	
DCIA(%): 0.00		

---

Name: B-24	Node: B-24	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh256	Peaking Factor: 256.0	
Rainfall File:	Storm Duration(hrs): 0.00	
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00	
Area(ac): 1.060	Time Shift(hrs): 0.00	
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000	
DCIA(%): 0.00		

---

Name: B-25	Node: B-25	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh256	Peaking Factor: 256.0	
Rainfall File:	Storm Duration(hrs): 0.00	
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00	
Area(ac): 1.770	Time Shift(hrs): 0.00	
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000	
DCIA(%): 0.00		

---

Name: B-26	Node: B-26	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh256	Peaking Factor: 256.0	
Rainfall File:	Storm Duration(hrs): 0.00	
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00	
Area(ac): 0.360	Time Shift(hrs): 0.00	
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000	
DCIA(%): 0.00		

---

Name: B-27	Node: B-27	Status: Onsite
Group: BASE	Type: SCS Unit Hydrograph CN	
Unit Hydrograph: Uh256	Peaking Factor: 256.0	
Rainfall File:	Storm Duration(hrs): 0.00	
Rainfall Amount(in): 0.000	Time of Conc(min): 10.00	
Area(ac): 1.750	Time Shift(hrs): 0.00	
Curve Number: 98.00	Max Allowable Q(cfs): 999999.000	
DCIA(%): 0.00		

---



Rainfall Amount(in): 0.000                      Time of Conc(min): 10.00  
 Area(ac): 0.380                                      Time Shift(hrs): 0.00  
 Curve Number: 98.00                                Max Allowable Q(cfs): 999999.000  
 DCIA(%): 0.00

-----  
 Name: B-9    Node: B-9    Status: Onsite  
 Group: BASE    Type: SCS Unit Hydrograph CN  
  
 Unit Hydrograph: Uh256    Peaking Factor: 256.0  
 Rainfall File:    Storm Duration(hrs): 0.00  
 Rainfall Amount(in): 0.000                                      Time of Conc(min): 10.00  
 Area(ac): 0.370    Time Shift(hrs): 0.00  
 Curve Number: 98.00                                      Max Allowable Q(cfs): 999999.000  
 DCIA(%): 0.00

-----  
 Name: OFFSITE    Node: J-2    Status: Onsite  
 Group: BASE    Type: SCS Unit Hydrograph CN  
  
 Unit Hydrograph: Uh256    Peaking Factor: 256.0  
 Rainfall File:    Storm Duration(hrs): 0.00  
 Rainfall Amount(in): 0.000                                      Time of Conc(min): 21.00  
 Area(ac): 2.960    Time Shift(hrs): 0.00  
 Curve Number: 98.00                                      Max Allowable Q(cfs): 999999.000  
 DCIA(%): 0.00

For Tc calculation see Offisite basin Tc calculations spreadsheet.

=====  
 --- Nodes ---  
 =====

Name: B-1    Base Flow(cfs): 0.000    Init Stage(ft): 0.000  
 Group: BASE    Warn Stage(ft): 3.800  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
3.800	0.0013
4.000	0.0031
4.500	0.0387
5.000	0.1734
6.000	0.7710
7.000	1.5717
8.000	2.4696
9.000	3.4703
10.500	5.0287
12.000	6.5871

Name: B-10    Base Flow(cfs): 0.000    Init Stage(ft): 0.000  
 Group: BASE    Warn Stage(ft): 4.110  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
4.110	0.0014
4.500	0.0050
5.000	0.0546
6.000	0.3749
7.000	0.9191
8.000	1.6202
9.000	2.3451
10.500	3.4326
12.000	4.5200

Name: B-11    Base Flow(cfs): 0.000    Init Stage(ft): 0.000  
 Group: BASE    Warn Stage(ft): 4.060  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000



Mary Brickell Village Drainage Improvements  
 Final Design  
 Input Report

4.060	0.0014
4.500	0.0084
5.000	0.0546
6.000	0.3151
7.000	0.8961
8.000	2.0271
9.000	3.4190
10.500	5.5068
12.000	7.5946

Name: B-12                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.150  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
4.150	0.0015
4.500	0.0039
5.000	0.0304
6.000	0.1711
7.000	0.4770
8.000	0.9524
9.000	1.5624
10.500	2.6467
12.000	3.7310

Name: B-13                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.870  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
5.870	0.0025
6.000	0.0026
7.000	0.0224
8.000	0.0686
9.000	0.1424
10.500	0.3642
12.000	0.6021

Name: B-14                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.700  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
5.700	0.0024
6.000	0.0032
7.000	0.0515
8.000	0.1856
9.000	0.4534
10.500	1.1248
12.000	1.9320

Name: B-15                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.660  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
5.660	0.0023
6.000	0.0033
7.000	0.0798
8.000	0.3051
9.000	0.6773
10.500	1.4554
12.000	2.2945

Name: B-16                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 8.130

Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
8.130	0.0037
9.000	0.0740
10.500	0.5881
12.000	1.2283

Name: B-17                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 8.150  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
8.150	0.0038
9.000	0.0596
10.500	0.6260
12.000	1.3156

Name: B-18                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.030  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
4.030	0.0014
4.500	0.0064
5.000	0.0359
6.000	0.2829
7.000	0.8156
8.000	1.3831
9.000	1.9506
10.500	2.8019
12.000	3.6532

Name: B-19                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.370  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
4.370	0.0016
4.500	0.0017
5.000	0.0073
6.000	0.1121
7.000	0.3848
8.000	0.7395
9.000	1.1411
10.500	1.7434
12.000	2.3458

Name: B-2                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 3.960  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
3.960	0.0014
4.500	0.0200
5.000	0.0808
6.000	0.2586
7.000	0.5060
8.000	0.7940
9.000	1.1270
10.500	1.6521
12.000	2.1918

-----  
 Name: B-20                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 3.670  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
3.670	0.0012
4.000	0.0031
4.500	0.0347
5.000	0.1211
6.000	0.4812
7.000	1.0491
8.000	1.8381
9.000	2.6272
10.500	3.8107
12.000	4.9943

-----  
 Name: B-21                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 3.830  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
3.830	0.0013
4.000	0.0016
4.500	0.0307
5.000	0.1330
6.000	0.4696
7.000	0.9242
8.000	1.4315
9.000	2.1144
10.500	3.1559
12.000	4.1974

-----  
 Name: B-22                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.310  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
5.310	0.0021
6.000	0.0197
7.000	0.1241
8.000	0.3267
9.000	0.6524
10.500	1.3352
12.000	2.2350

-----  
 Name: B-23                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.340  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
5.340	0.0021
6.000	0.0172
7.000	0.0886
8.000	0.2126
9.000	0.3729
10.500	0.7495
12.000	1.2461

-----  
 Name: B-24                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.200  
 Type: Stage/Volume

Stage(ft)	Volume(af)
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Mary Brickell Village Drainage Improvements  
 Final Design  
 Input Report

0.000	0.0000
4.200	0.0015
4.500	0.0020
5.000	0.0251
6.000	0.2376
7.000	0.5373
8.000	0.8959
9.000	1.3047
10.500	1.9634
12.000	2.8260

Name: B-25                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.200  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
4.200	0.0015
4.500	0.0035
5.000	0.0453
6.000	0.3025
7.000	0.6905
8.000	1.2048
9.000	1.7916
10.500	2.7538
12.000	3.8005

Name: B-26                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 9.940  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
9.940	0.0048
10.500	0.0099
12.000	0.0891

Name: B-27                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.900  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
5.900	0.0025
6.000	0.0222
7.000	0.1041
8.000	0.3342
9.000	0.7004
10.500	1.4681
12.000	2.3786

Name: B-28                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.800  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
5.800	0.0024
6.000	0.0025
7.000	0.0395
8.000	0.1565
9.000	0.3610
10.500	0.8406
12.000	1.4000

Name: B-3                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 3.960  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
3.960	0.0013
4.000	0.0014
4.500	0.0278
5.000	0.1191
6.000	0.4511
7.000	0.8571
8.000	1.3610
9.000	1.8650
10.500	2.6209
12.000	3.3768

Name: B-4                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 3.120  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
3.120	0.0009
3.500	0.0013
4.000	0.0092
4.500	0.0446
5.000	0.1445
6.000	0.5415
7.000	0.9754
8.000	1.4128
9.000	1.8534
10.500	2.5198
12.000	3.1921

Name: B-5                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 3.690  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
3.690	0.0012
4.000	0.0030
4.500	0.0429
5.000	0.1588
6.000	0.5515
7.000	1.0384
8.000	1.7077
9.000	2.3797
10.500	3.3877
12.000	4.3958

Name: B-6                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.870  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
4.870	0.0019
5.000	0.0024
6.000	0.0311
7.000	0.1475
8.000	0.3786
9.000	0.6798
10.500	1.2133
12.000	1.7468

Name: B-7                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.220  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000



5.220	0.0012
6.000	0.0403
7.000	0.2176
8.000	0.4601
9.000	0.7026
10.500	1.0663
12.000	1.4301

Name: B-8                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.900  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
4.900	0.0019
5.000	0.0024
6.000	0.0444
7.000	0.2148
8.000	0.5568
9.000	0.9400
10.500	1.5148
12.000	2.0896

Name: B-9                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.860  
 Type: Stage/Volume

Stage(ft)	Volume(af)
0.000	0.0000
4.860	0.0019
5.000	0.0020
6.000	0.0762
7.000	0.3260
8.000	0.6753
9.000	1.0444
10.500	1.5980
12.000	2.1516

Name: D-1                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 6.500  
 Type: Stage/Area

EMERGENCY OVERFLOW CONTROL STRUCTURE W/ GATE VALVE, DOWNSTREAM LINK MODELED AS POSITIVE TO SIMULATE A CHECK VALVE ON THE DOWNSTR

Stage(ft)	Area(ac)
0.000	0.0006
6.500	0.0006

Name: D-2                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 6.500  
 Type: Stage/Area

FORCE MAIN RETURN STRUCTURE INSTALLED ALONG EXISTING CULVERT

Stage(ft)	Area(ac)
0.000	0.0006
6.500	0.0006

Name: D-3                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 6.500  
 Type: Stage/Area

JUNCTURE BOX TO MODEL DIVERSION TEE ALONG FORCE MAIN TO DIVERT FLOWS TO WELLS

Stage(ft)	Area(ac)
0.000	0.0001
6.500	0.0001

Name: D-3A                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 6.500  
 Type: Stage/Area

DUMMY NODE TO MODEL REDUCER

Stage(ft)	Area(ac)
0.000	0.0001
6.500	0.0001

Name: GROUNDWATER      Base Flow(cfs): 0.000      Init Stage(ft): 2.250  
 Group: BASE              Warn Stage(ft): 0.000  
 Type: Time/Stage

This node represents the downstream discharge of the Well or the Goundwater table which was determined to be approximately 2.00'

Time(hrs)	Stage(ft)
0.00	2.250
200.00	2.250

Name: J-1                      Base Flow(cfs): 0.000      Init Stage(ft): 0.000  
 Group: BASE                  Warn Stage(ft): 5.800  
 Type: Stage/Area

DIVERSION STRUCTURE INSTALLED ALONG EXISTING CULVERT

Stage(ft)	Area(ac)
0.000	0.0006
5.800	0.0006

Name: J-10                      Base Flow(cfs): 0.000      Init Stage(ft): 0.000  
 Group: BASE                  Warn Stage(ft): 5.860  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
5.860	0.0006

Name: J-11                      Base Flow(cfs): 0.000      Init Stage(ft): 0.000  
 Group: BASE                  Warn Stage(ft): 5.950  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
5.950	0.0006

Name: J-12                      Base Flow(cfs): 0.000      Init Stage(ft): 0.000  
 Group: BASE                  Warn Stage(ft): 4.650  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
4.650	0.0006

Name: J-13                      Base Flow(cfs): 0.000      Init Stage(ft): 0.000  
 Group: BASE                  Warn Stage(ft): 10.080  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
10.080	0.0006

Name: J-14                      Base Flow(cfs): 0.000      Init Stage(ft): 0.000  
 Group: BASE                  Warn Stage(ft): 6.500  
 Type: Stage/Area

Stage(ft)	Area(ac)
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0.000      0.0006  
 6.500      0.0006

Name: J-2                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.000  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
5.000	0.0006

Name: J-3                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.200  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
4.200	0.0006

Name: J-4                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.600  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
4.600	0.0006

Name: J-5                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.300  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
5.300	0.0006

Name: J-6                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 5.200  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
5.200	0.0006

Name: J-7                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.400  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
4.400	0.0006

Name: J-8                      Base Flow(cfs): 0.000              Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.860  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
4.860	0.0006

Name: J-9                      Base Flow(cfs): 0.000                      Init Stage(ft): 0.000  
 Group: BASE                      Warn Stage(ft): 4.000  
 Type: Stage/Area

Stage(ft)	Area(ac)
0.000	0.0006
4.000	0.0006

Name: P-1                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 6.500  
 Type: Stage/Area

Stage(ft)	Area(ac)
2.600	0.0001
6.500	0.0001

Name: P-2                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 6.500  
 Type: Stage/Area

Stage(ft)	Area(ac)
2.600	0.0001
6.500	0.0001

Name: VALVEBOX                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 6.500  
 Type: Stage/Area

Stage(ft)	Area(ac)
2.600	0.0001
6.500	0.0001

Name: W-1                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 8.000  
 Type: Stage/Area

JUNCTURE BOX TO MODEL WELL STRUCTURE

Stage(ft)	Area(ac)
0.000	0.0001
6.500	0.0001

Name: W-2                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 8.000  
 Type: Stage/Area

JUNCTURE BOX TO MODEL WELL STRUCTURE

Stage(ft)	Area(ac)
0.000	0.0001
6.500	0.0001

Name: WATERWAY                      Base Flow(cfs): 0.000                      Init Stage(ft): 2.600  
 Group: BASE                      Warn Stage(ft): 2.600  
 Type: Time/Stage

Outfall Discharge to Miami River,  
 Tidal Data at Miami Marina NOAA Station used to determine mean high-high water.  
 MHHW determined to be 2.6' City of Miami Datum

Time(hrs)	Stage(ft)
0.00	2.600
100.00	2.600





Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B11-J7	From Node: B-11	Length(ft): 19.00
Group: BASE	To Node: J-7	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Circular	Circular	Entrance Loss Coef: 0.50
Span(in): 18.00	18.00	Exit Loss Coef: 0.00
Rise(in): 18.00	18.00	Bend Loss Coef: 0.70
Invert(ft): 2.010	1.550	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	Stabilizer Option: None
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B12-J7	From Node: B-12	Length(ft): 61.00
Group: BASE	To Node: J-7	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Rectangular	Rectangular	Entrance Loss Coef: 0.50
Span(in): 30.00	30.00	Exit Loss Coef: 0.00
Rise(in): 19.00	19.00	Bend Loss Coef: 0.00
Invert(ft): 1.800	1.800	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	Stabilizer Option: None
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: B13-B12	From Node: B-13	Length(ft): 320.00
Group: BASE	To Node: B-12	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Rectangular	Rectangular	Entrance Loss Coef: 0.50
Span(in): 30.00	30.00	Exit Loss Coef: 0.00
Rise(in): 19.00	19.00	Bend Loss Coef: 0.70
Invert(ft): 1.320	0.360	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	Stabilizer Option: None
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: B14-B13	From Node: B-14	Length(ft): 78.00
Group: BASE	To Node: B-13	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Rectangular	Rectangular	Entrance Loss Coef: 0.50
Span(in): 23.00	23.00	Exit Loss Coef: 0.00
Rise(in): 14.00	14.00	Bend Loss Coef: 0.00
Invert(ft): 1.750	1.770	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	

Bot Clip(in): 0.000                      0.000                      Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: B15-B14	From Node: B-15	Length(ft): 22.00
Group: BASE	To Node: B-14	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 12.00	12.00	Flow: Both
Rise(in): 12.00	12.00	Entrance Loss Coef: 0.50
Invert(ft): 1.950	1.770	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.55
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B16-B14	From Node: B-16	Length(ft): 349.00
Group: BASE	To Node: B-14	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 15.00	15.00	Flow: None
Rise(in): 15.00	15.00	Entrance Loss Coef: 0.50
Invert(ft): 2.550	1.800	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B17-B16	From Node: B-17	Length(ft): 30.00
Group: BASE	To Node: B-16	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 12.00	12.00	Flow: Both
Rise(in): 12.00	12.00	Entrance Loss Coef: 0.50
Invert(ft): 2.800	2.480	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.55
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B18-B1	From Node: B-18	Length(ft): 350.00
Group: BASE	To Node: B-1	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Rectangular	Rectangular	Solution Algorithm: Most Restrictive
		Flow: Both

Span(in): 42.00	42.00	Entrance Loss Coef: 0.50
Rise(in): 30.00	30.00	Exit Loss Coef: 0.00
Invert(ft): 0.590	0.150	Bend Loss Coef: 0.70
Manning's N: 0.012000	0.012000	Outlet Ctrl Spec: Use dc or tw
Top Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
Bot Clip(in): 0.000	0.000	Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: B19-J8	From Node: B-19	Length(ft): 32.00
Group: BASE	To Node: J-8	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 18.00	18.00	Flow: Both
Rise(in): 18.00	18.00	Entrance Loss Coef: 0.50
Invert(ft): 2.110	1.950	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B2-J3	From Node: B-2	Length(ft): 17.00
Group: BASE	To Node: J-3	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 18.00	18.00	Flow: Both
Rise(in): 18.00	18.00	Entrance Loss Coef: 0.50
Invert(ft): 0.510	0.270	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B20-J9	From Node: B-20	Length(ft): 12.00
Group: BASE	To Node: J-9	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 18.00	18.00	Flow: Both
Rise(in): 18.00	18.00	Entrance Loss Coef: 0.50
Invert(ft): 1.800	1.800	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B21-J9	From Node: B-21	Length(ft): 40.00
Group: BASE	To Node: J-9	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 18.00	18.00	Flow: Both
Rise(in): 18.00	18.00	Entrance Loss Coef: 0.50
Invert(ft): 1.500	1.500	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B22-B18	From Node: B-22	Length(ft): 346.00
Group: BASE	To Node: B-18	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Rectangular	Rectangular	Solution Algorithm: Most Restrictive
Span(in): 36.00	36.00	Flow: Both
Rise(in): 30.00	30.00	Entrance Loss Coef: 0.50
Invert(ft): 1.110	0.590	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: B23-J11	From Node: B-23	Length(ft): 31.00
Group: BASE	To Node: J-11	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 15.00	15.00	Flow: Both
Rise(in): 15.00	15.00	Entrance Loss Coef: 0.50
Invert(ft): 3.400	3.250	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B24-J12	From Node: B-24	Length(ft): 13.00
Group: BASE	To Node: J-12	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 18.00	18.00	Flow: Both
Rise(in): 18.00	18.00	Entrance Loss Coef: 0.50
Invert(ft): 2.500	2.100	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:

Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B25-J12	From Node: B-25	Length(ft): 21.00
Group: BASE	To Node: J-12	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 18.00	18.00	Flow: Both
Rise(in): 18.00	18.00	Entrance Loss Coef: 0.50
Invert(ft): 2.410	2.120	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B26-J13	From Node: B-26	Length(ft): 41.00
Group: BASE	To Node: J-13	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 12.00	12.00	Flow: Both
Rise(in): 12.00	12.00	Entrance Loss Coef: 0.50
Invert(ft): 5.110	4.440	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B27-J14	From Node: B-27	Length(ft): 9.00
Group: BASE	To Node: J-14	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 18.00	18.00	Flow: Both
Rise(in): 18.00	18.00	Entrance Loss Coef: 0.50
Invert(ft): 2.770	2.500	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B28-J14	From Node: B-28	Length(ft): 26.00
Group: BASE	To Node: J-14	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 18.00	18.00	Flow: Both
Rise(in): 18.00	18.00	Entrance Loss Coef: 0.50
Invert(ft): 2.800	2.500	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None



Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B3-J3	From Node: B-3	Length(ft): 37.00
Group: BASE	To Node: J-3	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 18.00	18.00	Flow: Both
Rise(in): 18.00	18.00	Entrance Loss Coef: 0.50
Invert(ft): 0.870	1.350	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B4-J4	From Node: B-4	Length(ft): 6.00
Group: BASE	To Node: J-4	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 24.00	24.00	Flow: Both
Rise(in): 24.00	24.00	Entrance Loss Coef: 0.50
Invert(ft): 1.370	1.000	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 24"

Name: B5-J4	From Node: B-5	Length(ft): 18.00
Group: BASE	To Node: J-4	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 18.00	18.00	Flow: Both
Rise(in): 18.00	18.00	Entrance Loss Coef: 0.50
Invert(ft): 1.640	1.000	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Cross Drain size increased to 18"

Name: B6-J5	From Node: B-6	Length(ft): 9.00
Group: BASE	To Node: J-5	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 12.00	12.00	Flow: Both
Rise(in): 12.00	12.00	Entrance Loss Coef: 0.50
Invert(ft): 1.820	1.470	Exit Loss Coef: 0.00
		Bend Loss Coef: 0.70

Manning's N: 0.012000	0.012000	Outlet Ctrl Spec: Use dc or tw
Top Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
Bot Clip(in): 0.000	0.000	Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B7-J5	From Node: B-7	Length(ft): 33.00
Group: BASE	To Node: J-5	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Circular	Circular	Entrance Loss Coef: 0.50
Span(in): 12.00	12.00	Exit Loss Coef: 0.00
Rise(in): 12.00	12.00	Bend Loss Coef: 0.70
Invert(ft): 0.970	0.590	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	Stabilizer Option: None
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B8-J6	From Node: B-8	Length(ft): 20.00
Group: BASE	To Node: J-6	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Circular	Circular	Entrance Loss Coef: 0.50
Span(in): 12.00	12.00	Exit Loss Coef: 0.00
Rise(in): 12.00	12.00	Bend Loss Coef: 0.70
Invert(ft): 1.390	0.800	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	Stabilizer Option: None
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: B9-J6	From Node: B-9	Length(ft): 32.00
Group: BASE	To Node: J-6	Count: 1
		Friction Equation: Automatic
		Solution Algorithm: Most Restrictive
UPSTREAM	DOWNSTREAM	Flow: Both
Geometry: Circular	Circular	Entrance Loss Coef: 0.50
Span(in): 12.00	12.00	Exit Loss Coef: 0.00
Rise(in): 12.00	12.00	Bend Loss Coef: 0.70
Invert(ft): 1.460	0.450	Outlet Ctrl Spec: Use dc or tw
Manning's N: 0.012000	0.012000	Inlet Ctrl Spec: Use dc
Top Clip(in): 0.000	0.000	Stabilizer Option: None
Bot Clip(in): 0.000	0.000	

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: D1-D2	From Node: D-1	Length(ft): 50.00
Group: BASE	To Node: D-2	Count: 1
		Friction Equation: Automatic

UPSTREAM	DOWNSTREAM	Solution Algorithm: Most Restrictive
Geometry: Rectangular	Rectangular	Flow: Positive
Span(in): 60.00	60.00	Entrance Loss Coef: 0.50
Rise(in): 36.00	36.00	Exit Loss Coef: 0.00
Invert(ft): -0.750	-0.750	Bend Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Outlet Ctrl Spec: Use dc or tw
Top Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
Bot Clip(in): 0.000	0.000	Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

FLOW IS POSITIVE TO SIMULATE A CHECK VALVE ON THE DOWNSTREAM STRUCTURE TO NOT ALLOW FOR RECIRCULATION OF THE PUMPED WATERS.

Name: D2-WW	From Node: D-2	Length(ft): 975.00
Group: BASE	To Node: WATERWAY	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Rectangular	Rectangular	Solution Algorithm: Most Restrictive
Span(in): 60.00	60.00	Flow: Both
Rise(in): 36.00	36.00	Entrance Loss Coef: 0.50
Invert(ft): -0.750	-0.800	Exit Loss Coef: 1.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: D3-W1	From Node: D-3	Length(ft): 50.00
Group: BASE	To Node: W-1	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 24.86	24.86	Flow: Both
Rise(in): 24.86	24.86	Entrance Loss Coef: 0.00
Invert(ft): 0.500	0.500	Exit Loss Coef: 1.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.50
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

This pipe represents the force main stub-out to well 1

Name: D3-W2	From Node: D-3	Length(ft): 50.00
Group: BASE	To Node: W-2	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 24.86	24.86	Flow: Both
Rise(in): 24.86	24.86	Entrance Loss Coef: 0.00
Invert(ft): 0.500	0.500	Exit Loss Coef: 1.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.50
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

This pipe represents the force main stub-out to well 2

```

-----
Name: D3A-D3          From Node: D-3A          Length(ft): 0.50
Group: BASE          To Node: D-2              Count: 1
                                Friction Equation: Automatic
                                Solution Algorithm: Most Restrictive
                                Flow: Both
UPSTREAM          DOWNSTREAM
Geometry: Circular          Circular
Span(in): 43.00          32.40
Rise(in): 43.00          32.40
Invert(ft): 0.000          0.000
Manning's N: 0.012000      0.012000
Top Clip(in): 0.000          0.000
Bot Clip(in): 0.000          0.000
Entrance Loss Coef: 0.00
Exit Loss Coef: 1.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

PIPE REPRESENTS 32.4" CONTROL ORIFACE INSTALLED IN PIPE FLANGE CONNECTOR

```

-----
Name: J1-D1          From Node: J-1          Length(ft): 25.00
Group: BASE          To Node: D-1              Count: 1
                                Friction Equation: Automatic
                                Solution Algorithm: Most Restrictive
                                Flow: Both
UPSTREAM          DOWNSTREAM
Geometry: Rectangular      Rectangular
Span(in): 60.00          60.00
Rise(in): 36.00          36.00
Invert(ft): -0.680          -0.750
Manning's N: 0.012000      0.012000
Top Clip(in): 0.000          0.000
Bot Clip(in): 0.000          0.000
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

```

-----
Name: J1-WETWELL     From Node: J-1          Length(ft): 30.00
Group: BASE          To Node: WETWELL        Count: 1
                                Friction Equation: Automatic
                                Solution Algorithm: Most Restrictive
                                Flow: Both
UPSTREAM          DOWNSTREAM
Geometry: Circular          Circular
Span(in): 84.00          84.00
Rise(in): 84.00          84.00
Invert(ft): -1.000          -1.000
Manning's N: 0.012000      0.012000
Top Clip(in): 0.000          0.000
Bot Clip(in): 0.000          0.000
Entrance Loss Coef: 0.50
Exit Loss Coef: 1.00
Bend Loss Coef: 0.00
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

```

-----
Name: J10-B22        From Node: J-10         Length(ft): 45.00
Group: BASE          To Node: B-22           Count: 1
                                Friction Equation: Automatic
                                Solution Algorithm: Most Restrictive
                                Flow: Both
UPSTREAM          DOWNSTREAM
Geometry: Rectangular      Rectangular
Span(in): 36.00          36.00
Rise(in): 30.00          30.00
Invert(ft): 1.200          1.110
Manning's N: 0.012000      0.012000
Top Clip(in): 0.000          0.000
Bot Clip(in): 0.000          0.000
Entrance Loss Coef: 0.50
Exit Loss Coef: 0.00
Bend Loss Coef: 0.70
Outlet Ctrl Spec: Use dc or tw
Inlet Ctrl Spec: Use dc
Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: J11-J10	From Node: J-11	Length(ft): 22.00
Group: BASE	To Node: J-10	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 30.00	30.00	Flow: Both
Rise(in): 30.00	30.00	Entrance Loss Coef: 0.50
Invert(ft): 1.280	1.200	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Pipe run size increased to 30" circular

Name: J12-J11	From Node: J-12	Length(ft): 351.00
Group: BASE	To Node: J-11	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 30.00	30.00	Flow: Both
Rise(in): 30.00	30.00	Entrance Loss Coef: 0.50
Invert(ft): 1.950	1.280	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Pipe run size increased to 30" circular

Name: J13-J10	From Node: J-13	Length(ft): 348.00
Group: BASE	To Node: J-10	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 21.00	21.00	Flow: Both
Rise(in): 21.00	21.00	Entrance Loss Coef: 0.50
Invert(ft): 1.160	0.780	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: J14-J13	From Node: J-14	Length(ft): 392.00
Group: BASE	To Node: J-13	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 21.00	21.00	Flow: None
Rise(in): 21.00	21.00	Entrance Loss Coef: 0.50
Invert(ft): 2.000	1.060	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None



Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Name: J2-J1	From Node: J-2	Length(ft): 50.00
Group: BASE	To Node: J-1	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Rectangular	Rectangular	Solution Algorithm: Most Restrictive
Span(in): 60.00	60.00	Flow: Both
Rise(in): 36.00	36.00	Entrance Loss Coef: 0.50
Invert(ft): -0.250	-0.680	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: J3-B1	From Node: J-3	Length(ft): 48.00
Group: BASE	To Node: B-1	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 48.00	48.00	Flow: Both
Rise(in): 48.00	48.00	Entrance Loss Coef: 0.50
Invert(ft): 0.250	0.000	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Pipe run modified to 48" circular

Name: J4-J3	From Node: J-4	Length(ft): 230.00
Group: BASE	To Node: J-3	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 48.00	48.00	Flow: Both
Rise(in): 48.00	48.00	Entrance Loss Coef: 0.50
Invert(ft): 0.500	0.500	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Pipe run modified to 48"Circular

Name: J5-J4	From Node: J-5	Length(ft): 383.00
Group: BASE	To Node: J-4	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 36.00	42.00	Flow: Both
		Entrance Loss Coef: 0.50

Rise(in): 36.00	42.00	Exit Loss Coef: 0.00
Invert(ft): 1.000	0.500	Bend Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Outlet Ctrl Spec: Use dc or tw
Top Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
Bot Clip(in): 0.000	0.000	Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Upsize to 42" circular pipe at downstream side. Intermediate manhole will be added with 36" upstream pipe

Name: J6-J5	From Node: J-6	Length(ft): 50.00
Group: BASE	To Node: J-5	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Rectangular	Rectangular	Solution Algorithm: Most Restrictive
Span(in): 36.00	36.00	Flow: Both
Rise(in): 24.00	24.00	Entrance Loss Coef: 0.50
Invert(ft): -1.050	-1.120	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: J7-J6	From Node: J-7	Length(ft): 264.00
Group: BASE	To Node: J-6	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Rectangular	Rectangular	Solution Algorithm: Most Restrictive
Span(in): 36.00	36.00	Flow: Both
Rise(in): 24.00	24.00	Entrance Loss Coef: 0.50
Invert(ft): 1.560	1.330	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: J8-B18	From Node: J-8	Length(ft): 53.00
Group: BASE	To Node: B-18	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Rectangular	Rectangular	Solution Algorithm: Most Restrictive
Span(in): 36.00	36.00	Flow: Both
Rise(in): 30.00	30.00	Entrance Loss Coef: 0.50
Invert(ft): 0.810	0.650	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Downstream FHWA Inlet Edge Description:  
 Rectangular Box: 30° to 75° wingwall flares

Name: J9-J8	From Node: J-9	Length(ft): 294.00
-------------	----------------	--------------------

Group: BASE	To Node: J-8	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 30.00	30.00	Flow: Both
Rise(in): 30.00	30.00	Entrance Loss Coef: 0.50
Invert(ft): 0.500	0.500	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Pipe run size increased to 30" circular

Name: P1-VB	From Node: P-1	Length(ft): 454.00
Group: BASE	To Node: VALVEBOX	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 24.92	24.92	Flow: Positive
Rise(in): 24.92	24.92	Entrance Loss Coef: 0.00
Invert(ft): 0.500	0.500	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

This pipe represents the run between the pump outlet, through the valve box fixtures and out to the force main connection. Length is a hydraulic equivalent length including pipes, fittings, and bends. This pipe is shown with only positive flow in order to model a one-way check valve installed in the discharge pipe to avoid reci

Name: P2-VB	From Node: P-2	Length(ft): 454.00
Group: BASE	To Node: VALVEBOX	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 24.92	24.92	Flow: Positive
Rise(in): 24.92	24.92	Entrance Loss Coef: 0.00
Invert(ft): 0.500	0.500	Exit Loss Coef: 0.00
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.70
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

This pipe represents the run between the pump outlet, through the valve box fixtures and out to the force main connection. Length is a hydraulic equivalent length including pipes, fittings, and bends. This pipe is shown with only positive flow in order to model a one-way check valve installed in the discharge pipe to avoid reci

Name: VB-D3	From Node: VALVEBOX	Length(ft): 5.00
Group: BASE	To Node: d-3	Count: 1
UPSTREAM	DOWNSTREAM	Friction Equation: Automatic
Geometry: Circular	Circular	Solution Algorithm: Most Restrictive
Span(in): 43.00	43.00	Flow: Both
Rise(in): 43.00	43.00	Entrance Loss Coef: 0.00
Invert(ft): 0.000	0.000	Exit Loss Coef: 0.70
Manning's N: 0.012000	0.012000	Bend Loss Coef: 0.00
Top Clip(in): 0.000	0.000	Outlet Ctrl Spec: Use dc or tw
Bot Clip(in): 0.000	0.000	Inlet Ctrl Spec: Use dc
		Stabilizer Option: None

Upstream FHWA Inlet Edge Description:

Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

```

-----
Name: VB-D3A           From Node: VALVEBOX           Length(ft): 250.00
Group: BASE           To Node: d-3A                 Count: 1
                                     Friction Equation: Automatic
                                     Solution Algorithm: Most Restrictive
UPSTREAM              DOWNSTREAM
Geometry: Circular    Circular
Span(in): 43.00       43.00
Rise(in): 43.00       43.00
Invert(ft): 0.000     0.000
Manning's N: 0.012000 0.012000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
                                     Entrance Loss Coef: 0.00
                                     Exit Loss Coef: 0.50
                                     Bend Loss Coef: 0.00
                                     Outlet Ctrl Spec: Use dc or tw
                                     Inlet Ctrl Spec: Use dc
                                     Stabilizer Option: None
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

This pipe represents the force main connecting back to the bypassed gravity outfall, included equivalent lengths for fittings (i

==== Channels =====

```

-----
Name:                   From Node:           Length(ft): 0.00
Group: BASE            To Node:             Count: 1
                                     Friction Equation: Automatic
                                     Solution Algorithm: Automatic
UPSTREAM              DOWNSTREAM
Geometry: Trapezoidal Trapezoidal
Invert(ft): 0.000     0.000
TClpInitZ(ft): 9999.000 9999.000
Manning's N: 0.000000 0.000000
Top Clip(ft): 0.000   0.000
Bot Clip(ft): 0.000   0.000
Main XSec:            Outlet Ctrl Spec: Use dc or tw
AuxElev1(ft):         Inlet Ctrl Spec: Use dc
Aux XSec1:            Stabilizer Option: None
AuxElev2(ft):
Aux XSec2:
Top Width(ft):
Depth(ft):
Bot Width(ft): 0.000   0.000
LtSdSlp(h/v): 0.00    0.00
RtSdSlp(h/v): 0.00    0.00
  
```

==== Drop Structures =====

```

-----
Name:                   From Node:           Length(ft): 0.00
Group: BASE            To Node:             Count: 1
                                     Friction Equation: Automatic
                                     Solution Algorithm: Most Restrictive
UPSTREAM              DOWNSTREAM
Geometry: Circular    Circular
Span(in): 0.00        0.00
Rise(in): 0.00        0.00
Invert(ft): 0.000     0.000
Manning's N: 0.000000 0.000000
Top Clip(in): 0.000   0.000
Bot Clip(in): 0.000   0.000
                                     Entrance Loss Coef: 0.000
                                     Exit Loss Coef: 1.000
                                     Outlet Ctrl Spec: Use dc or tw
                                     Inlet Ctrl Spec: Use dc
                                     Solution Incs: 10
  
```

Upstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

Downstream FHWA Inlet Edge Description:  
 Circular Concrete: Square edge w/ headwall

==== Bridges =====

```

-----
Name:                   From Node:           Flow: Both
  
```

Group: BASE	To Node:	Run WSPRO: No				
XSEC TYPE	NAME	INV(ft)	STAT(ft)	SKEW(deg)	EXPAN	CONTRAC
Exit		0.000	0.00	0.000	0.500	0.000
Full Valley		0.000	0.00	0.000	0.500	0.000
Approach		0.000	0.00	0.000	0.500	0.000
Roadway		0.000	0.00	0.000		

Road Surface Material: Paved  
 Road Embankment Top Width(ft): 0.00  
 Road Unsubmerged Weir Q Coef: 0.000

RATING CURVE CONTROL

TW(ft)	QMin(cfs)	QMax(cfs)	QInc(cfs)
0.000	0.000	0.000	0.000

==== Rating Curves =====

Name: PUMP 1                      From Node: WETWELL                      Count: 1  
 Group: BASE                        To Node: P-1                              Flow: Both

TABLE	ELEV ON(ft)	ELEV OFF(ft)
#1: pump	1.600	-8.000
#2:	0.000	0.000
#3:	0.000	0.000
#4:	0.000	0.000

Name: PUMP 2                      From Node: WETWELL                      Count: 1  
 Group: BASE                        To Node: P-2                              Flow: Both

TABLE	ELEV ON(ft)	ELEV OFF(ft)
#1: pump	2.100	-8.000
#2:	0.000	0.000
#3:	0.000	0.000
#4:	0.000	0.000

Name: Well 1                        From Node: W-1                            Count: 1  
 Group: BASE                        To Node: GROUNDWATER                    Flow: Both

TABLE	ELEV ON(ft)	ELEV OFF(ft)
#1: well	2.250	2.250
#2:	0.000	0.000
#3:	0.000	0.000
#4:	0.000	0.000

Discharge to Well

Name: Well 2                        From Node: W-2                            Count: 1  
 Group: BASE                        To Node: GROUNDWATER                    Flow: Both

TABLE	ELEV ON(ft)	ELEV OFF(ft)
#1: well	2.250	2.250
#2:	0.000	0.000
#3:	0.000	0.000
#4:	0.000	0.000

Discharge to Well

==== Exfiltration Trenches =====

Name:                                      From Node:                                      Flow: Both  
 Group: BASE                                To Node:                                        Count: 1

Aquifer Base Elev(ft): 0.000	Trench Bot Elev(ft): 0.000
Water Table Elev(ft): 0.000	Trench Width(ft): 0.000
*****0.000	Trench Length(ft): 0.000
Horiz Conductivity(ft/day): 0.000	Trench Height(ft): 0.000
Vert Conductivity(ft/day): 0.000	Gravel Porosity(dec): 0.000
Effective Porosity(dec): 0.000	Pipe Diameter(in): 0.000
Suction Head(in): 0.000	Pipe Invert Elev(ft): 0.000
	End Treatment: Exclude
	Cell Spacing(ft): 0.000



Num Cells: 0

==== Hydrology Simulations =====

Name: 100yr-72hr  
Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\post results final design\100yr-72hr.R32  
Override Defaults: Yes  
Storm Duration(hrs): 72.00  
Rainfall File: Sfwmd72  
Rainfall Amount(in): 14.00

Time(hrs)	Print Inc(min)
48.000	15.00
56.000	5.00
64.000	1.00
72.000	5.00
72.330	5.00

Name: 10yr-24hr  
Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\post results final design\10yr-24hr.R32  
Override Defaults: Yes  
Storm Duration(hrs): 24.00  
Rainfall File: Flmod  
Rainfall Amount(in): 7.90

Time(hrs)	Print Inc(min)
8.000	15.00
10.000	5.00
14.000	1.00
16.000	5.00
24.000	15.00
24.330	5.00

Name: 25yr-72hr  
Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\post results final design\25yr-72hr.R32  
Override Defaults: Yes  
Storm Duration(hrs): 72.00  
Rainfall File: Sfwmd72  
Rainfall Amount(in): 12.00

Time(hrs)	Print Inc(min)
48.000	15.00
56.000	5.00
64.000	1.00
72.000	5.00
72.330	5.00

Name: 5yr-24hr  
Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\post results final design\5yr-24hr.R32  
Override Defaults: Yes  
Storm Duration(hrs): 24.00  
Rainfall File: Flmod  
Rainfall Amount(in): 6.30

Time(hrs)	Print Inc(min)
8.000	15.00
10.000	5.00
14.000	1.00
16.000	5.00
24.000	15.00
24.330	5.00

==== Routing Simulations =====

Name: 100yr-72hr                    Hydrology Sim: 100yr-72hr  
Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\post results final design\100yr-72hr.I32  
Execute: Yes                    Restart: No                    Patch: No  
Alternative: No

---

Max Delta Z(ft): 1.00                      Delta Z Factor: 0.01000  
Time Step Optimizer: 10.000  
Start Time(hrs): 0.000                      End Time(hrs): 96.00  
Min Calc Time(sec): 0.0500                Max Calc Time(sec): 60.0000  
Boundary Stages: 25/100yr Tailwa        Boundary Flows:

Time(hrs)            Print Inc(min)  
-----  
48.000                15.000  
56.000                5.000  
64.000                1.000  
72.000                5.000  
96.000                15.000

Group                Run  
-----  
BASE                 Yes

---

Name: 10yr-24hr                      Hydrology Sim: 10yr-24hr  
Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\post results final design\10yr-24hr.I32

Execute: Yes                      Restart: No                      Patch: No  
Alternative: No

Max Delta Z(ft): 1.00                      Delta Z Factor: 0.01000  
Time Step Optimizer: 10.000  
Start Time(hrs): 0.000                      End Time(hrs): 48.00  
Min Calc Time(sec): 0.0500                Max Calc Time(sec): 60.0000  
Boundary Stages:                      Boundary Flows:

Time(hrs)            Print Inc(min)  
-----  
8.000                  5.000  
16.000                1.000  
24.000                5.000  
48.000                15.000

Group                Run  
-----  
BASE                 Yes

---

Name: 25yr-72hr                      Hydrology Sim: 25yr-72hr  
Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\post results final design\25yr-72hr.I32

Execute: No                      Restart: No                      Patch: No  
Alternative: No

Max Delta Z(ft): 1.00                      Delta Z Factor: 0.01000  
Time Step Optimizer: 10.000  
Start Time(hrs): 0.000                      End Time(hrs): 96.00  
Min Calc Time(sec): 0.0500                Max Calc Time(sec): 60.0000  
Boundary Stages: 25/100yr Tailwa        Boundary Flows:

Time(hrs)            Print Inc(min)  
-----  
48.000                15.000  
56.000                5.000  
64.000                1.000  
72.000                5.000  
96.000                15.000

Group                Run  
-----  
BASE                 Yes

---

Name: 5yr-24hr                      Hydrology Sim: 5yr-24hr  
Filename: K:\Projects\550860.15\_CM Mary Brickell Village\docs\drainage report\icpr\post results final design\5yr-24hr.I32

Execute: Yes                      Restart: No                      Patch: No  
Alternative: No

Max Delta Z(ft): 1.00                      Delta Z Factor: 0.01000  
Time Step Optimizer: 10.000  
Start Time(hrs): 0.000                      End Time(hrs): 48.00

---

Min Calc Time(sec): 0.0500  
Boundary Stages:

Max Calc Time(sec): 60.0000  
Boundary Flows:

Time(hrs)	Print Inc(min)
8.000	5.000
16.000	1.000
24.000	5.000
48.000	15.000

Group	Run
-----	-----
BASE	Yes

=====  
=== Boundary Conditions ===  
=====

Name: 25/100yr Tailwa      Node: WATERWAY      Type: Stage

Time(hrs)	Stage(ft)
-----	-----
0.000	3.800
1000.000	3.800

Mary Brickell Village Drainage Improvements  
Final Design  
Node Maximum Conditions Report

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
B-1	BASE	100yr-72hr	60.26	4.529	3.800	0.0026	8137	60.76	62.015	59.96	61.361
B-1	BASE	10yr-24hr	12.28	4.038	3.800	0.0055	2238	12.00	58.020	12.00	57.618
B-1	BASE	25yr-72hr	60.22	4.242	3.800	0.0047	4535	60.08	61.443	60.08	61.842
B-1	BASE	5yr-24hr	12.15	3.357	3.800	0.0053	276	12.14	56.016	12.14	55.991
B-10	BASE	100yr-72hr	60.41	5.295	4.110	-0.0045	11997	60.02	4.597	61.00	6.124
B-10	BASE	10yr-24hr	12.33	4.779	4.110	0.0026	6146	12.03	3.493	11.85	4.255
B-10	BASE	25yr-72hr	60.29	5.014	4.110	0.0033	9269	60.02	3.939	60.68	4.893
B-10	BASE	5yr-24hr	12.15	4.177	4.110	0.0026	581	12.03	2.782	11.92	4.248
B-11	BASE	100yr-72hr	60.41	5.311	4.060	-0.0034	11001	60.02	5.528	60.99	5.611
B-11	BASE	10yr-24hr	12.33	4.802	4.060	0.0018	5582	12.03	4.201	12.63	4.318
B-11	BASE	25yr-72hr	60.28	5.034	4.060	-0.0021	8051	60.02	4.738	60.73	4.984
B-11	BASE	5yr-24hr	12.15	4.202	4.060	-0.0020	1000	12.03	3.345	11.88	3.837
B-12	BASE	100yr-72hr	60.28	5.424	4.150	-0.0020	6580	60.00	13.414	60.05	10.187
B-12	BASE	10yr-24hr	12.28	4.876	4.150	0.0016	3520	12.05	10.844	12.03	9.024
B-12	BASE	25yr-72hr	60.20	5.146	4.150	0.0014	5047	60.02	12.064	60.06	9.668
B-12	BASE	5yr-24hr	12.14	4.261	4.150	0.0016	544	12.07	8.290	12.07	8.056
B-13	BASE	100yr-72hr	60.17	5.601	5.870	-0.0021	137	59.98	7.505	59.99	7.411
B-13	BASE	10yr-24hr	12.20	4.997	5.870	0.0011	137	12.06	6.406	12.07	6.292
B-13	BASE	25yr-72hr	60.13	5.318	5.870	0.0015	137	60.00	6.991	60.01	6.902
B-13	BASE	5yr-24hr	12.13	4.369	5.870	0.0012	137	12.08	4.889	12.10	4.784
B-14	BASE	100yr-72hr	60.11	5.882	5.700	0.0022	704	60.02	6.408	59.98	6.279
B-14	BASE	10yr-24hr	12.13	5.198	5.700	0.0011	117	12.05	5.577	12.06	5.469
B-14	BASE	25yr-72hr	60.09	5.581	5.700	0.0015	117	59.94	6.024	60.00	5.929
B-14	BASE	5yr-24hr	12.13	4.509	5.700	0.0010	117	12.07	4.320	12.09	4.166
B-15	BASE	100yr-72hr	60.15	6.218	5.660	-0.0021	2786	60.02	3.479	59.85	2.804
B-15	BASE	10yr-24hr	12.10	5.509	5.660	0.0011	114	12.03	2.644	12.07	2.525
B-15	BASE	25yr-72hr	60.10	5.924	5.660	0.0016	1359	60.02	2.981	59.94	2.700
B-15	BASE	5yr-24hr	12.12	4.697	5.660	0.0010	114	12.03	2.105	12.09	1.922
B-16	BASE	100yr-72hr	72.33	10.166	8.130	0.0001	15083	60.02	2.803	0.00	0.000
B-16	BASE	10yr-24hr	24.33	9.414	8.130	0.0003	11308	12.03	2.193	0.00	0.000
B-16	BASE	25yr-72hr	72.33	9.943	8.130	0.0001	13961	60.02	2.407	0.00	0.000
B-16	BASE	5yr-24hr	24.33	9.170	8.130	0.0002	10077	12.03	1.800	0.00	0.000
B-17	BASE	100yr-72hr	72.33	10.166	8.150	0.0001	16326	60.02	2.733	7.16	0.038
B-17	BASE	10yr-24hr	24.33	9.414	8.150	0.0003	12026	12.03	2.077	11.70	0.090
B-17	BASE	25yr-72hr	72.33	9.943	8.150	0.0001	15049	60.02	2.342	8.15	0.024
B-17	BASE	5yr-24hr	24.33	9.170	8.150	0.0002	10625	12.03	1.654	11.92	0.123
B-18	BASE	100yr-72hr	60.27	4.912	4.030	0.0042	5820	61.10	31.929	61.13	29.299
B-18	BASE	10yr-24hr	12.29	4.423	4.030	0.0041	1367	12.72	30.400	12.73	27.604
B-18	BASE	25yr-72hr	60.21	4.634	4.030	0.0039	2952	60.80	31.160	60.81	28.803
B-18	BASE	5yr-24hr	12.16	3.792	4.030	0.0039	273	12.36	25.898	12.42	24.635
B-19	BASE	100yr-72hr	60.28	4.950	4.370	0.0024	2301	60.02	2.485	59.89	2.175
B-19	BASE	10yr-24hr	12.29	4.465	4.370	-0.0019	198	12.03	1.888	12.06	1.769
B-19	BASE	25yr-72hr	60.21	4.675	4.370	0.0021	1055	60.02	2.129	59.97	2.005
B-19	BASE	5yr-24hr	12.16	3.840	4.370	0.0020	114	12.03	1.504	12.32	1.538
B-2	BASE	100yr-72hr	60.24	4.820	3.960	0.0026	5396	60.02	7.765	59.96	5.554
B-2	BASE	10yr-24hr	12.26	4.250	3.960	0.0019	2178	12.03	5.901	12.03	4.811
B-2	BASE	25yr-72hr	60.20	4.493	3.960	0.0013	3363	60.02	6.654	60.08	5.403
B-2	BASE	5yr-24hr	12.14	3.560	3.960	0.0018	609	12.03	4.699	12.12	4.100

Mary Brickell Village Drainage Improvements  
Final Design  
Node Maximum Conditions Report

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
B-20	BASE	100yr-72hr	60.40	5.070	3.670	-0.0056	12211	60.02	7.019	61.03	5.796
B-20	BASE	10yr-24hr	12.36	4.615	3.670	-0.0051	6627	12.03	5.334	12.68	4.926
B-20	BASE	25yr-72hr	60.29	4.812	3.670	-0.0057	9179	60.02	6.015	60.76	5.347
B-20	BASE	5yr-24hr	12.18	4.033	3.670	0.0016	1740	12.03	4.248	12.03	3.874
B-21	BASE	100yr-72hr	60.42	5.081	3.830	-0.0045	12228	60.02	6.957	61.12	6.910
B-21	BASE	10yr-24hr	12.37	4.626	3.830	-0.0082	7252	12.03	5.287	12.70	5.324
B-21	BASE	25yr-72hr	60.31	4.822	3.830	-0.0091	9633	60.02	5.962	60.80	5.901
B-21	BASE	5yr-24hr	12.18	4.055	3.830	0.0012	1794	12.03	4.210	12.04	4.060
B-22	BASE	100yr-72hr	60.20	5.137	5.310	0.0034	558	59.73	16.964	61.10	18.610
B-22	BASE	10yr-24hr	12.29	4.622	5.310	-0.0021	452	12.72	15.901	12.72	19.000
B-22	BASE	25yr-72hr	60.17	4.850	5.310	0.0030	499	60.80	16.626	60.83	19.268
B-22	BASE	5yr-24hr	12.16	4.009	5.310	0.0024	326	12.35	15.836	12.36	17.709
B-23	BASE	100yr-72hr	60.16	5.336	5.340	-0.0009	507	60.02	2.423	60.05	2.095
B-23	BASE	10yr-24hr	12.29	4.792	5.340	-0.0008	407	12.03	1.841	11.97	1.660
B-23	BASE	25yr-72hr	60.15	5.036	5.340	-0.0009	452	60.02	2.076	60.05	1.817
B-23	BASE	5yr-24hr	12.17	4.189	5.340	-0.0004	314	12.03	1.466	12.06	1.457
B-24	BASE	100yr-72hr	60.33	5.529	4.200	0.0036	8553	60.02	6.584	59.74	4.727
B-24	BASE	10yr-24hr	12.35	4.995	4.200	-0.0037	5593	12.03	5.004	11.85	4.485
B-24	BASE	25yr-72hr	60.27	5.230	4.200	-0.0034	6906	60.02	5.643	60.76	4.570
B-24	BASE	5yr-24hr	12.17	4.397	4.200	0.0054	700	12.03	3.984	11.93	4.476
B-25	BASE	100yr-72hr	60.35	5.675	4.200	-0.0098	11898	60.02	10.995	61.10	8.992
B-25	BASE	10yr-24hr	12.37	5.129	4.200	-0.0085	8281	12.03	8.356	12.72	8.301
B-25	BASE	25yr-72hr	60.28	5.370	4.200	-0.0095	9876	60.02	9.422	60.81	8.929
B-25	BASE	5yr-24hr	12.19	4.553	4.200	-0.0037	2549	12.03	6.653	12.02	6.580
B-26	BASE	100yr-72hr	60.02	6.096	9.940	0.0003	122	60.02	2.236	60.02	2.232
B-26	BASE	10yr-24hr	12.05	5.926	9.940	0.0002	130	12.03	1.699	12.05	1.697
B-26	BASE	25yr-72hr	60.02	5.995	9.940	0.0003	128	60.02	1.916	60.02	1.913
B-26	BASE	5yr-24hr	12.05	5.815	9.940	0.0002	132	12.03	1.353	12.05	1.351
B-27	BASE	100yr-72hr	72.33	11.091	5.900	-0.0002	26001	60.02	10.870	4.77	1.495
B-27	BASE	10yr-24hr	24.33	9.530	5.900	0.0009	20977	12.03	8.261	3.04	1.185
B-27	BASE	25yr-72hr	72.33	10.614	5.900	-0.0002	24684	60.02	9.316	5.52	1.209
B-27	BASE	5yr-24hr	24.33	9.047	5.900	0.0008	19286	12.03	6.578	3.66	1.106
B-28	BASE	100yr-72hr	72.49	11.091	5.800	0.0003	16000	60.02	5.901	7.16	0.381
B-28	BASE	10yr-24hr	48.00	9.530	5.800	0.0010	12715	12.03	4.485	4.29	0.564
B-28	BASE	25yr-72hr	72.49	10.614	5.800	0.0002	15264	60.02	5.057	8.16	0.343
B-28	BASE	5yr-24hr	48.00	9.047	5.800	0.0009	11533	12.03	3.571	5.10	0.554
B-3	BASE	100yr-72hr	60.33	4.678	3.960	-0.0029	7289	60.02	3.851	60.76	3.289
B-3	BASE	10yr-24hr	12.29	4.134	3.960	0.0014	2258	12.03	2.927	12.07	2.783
B-3	BASE	25yr-72hr	60.25	4.370	3.960	-0.0013	4107	60.02	3.300	59.92	2.998
B-3	BASE	5yr-24hr	12.15	3.458	3.960	0.0013	114	12.03	2.331	12.00	2.234
B-4	BASE	100yr-72hr	60.32	4.730	3.120	-0.0092	9158	60.02	4.410	59.69	6.388
B-4	BASE	10yr-24hr	12.29	4.173	3.120	-0.0063	3272	12.03	3.352	11.81	5.981
B-4	BASE	25yr-72hr	60.24	4.408	3.120	-0.0039	5153	60.02	3.780	59.71	6.306
B-4	BASE	5yr-24hr	12.15	3.533	3.120	-0.0063	468	12.03	2.669	11.89	6.038
B-5	BASE	100yr-72hr	60.37	4.775	3.690	0.0034	10540	60.02	5.963	60.90	5.029
B-5	BASE	10yr-24hr	12.30	4.241	3.690	-0.0037	4242	12.03	4.532	11.82	4.273
B-5	BASE	25yr-72hr	60.27	4.460	3.690	0.0040	6394	60.02	5.110	59.72	4.608
B-5	BASE	5yr-24hr	12.14	3.605	3.690	0.0033	129	12.03	3.609	11.91	4.335

Mary Brickell Village Drainage Improvements  
Final Design  
Node Maximum Conditions Report

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
B-6	BASE	100yr-72hr	60.24	4.946	4.870	0.0019	454	60.02	2.174	60.02	2.091
B-6	BASE	10yr-24hr	12.26	4.376	4.870	-0.0011	113	12.03	1.652	12.04	1.549
B-6	BASE	25yr-72hr	60.18	4.633	4.870	0.0008	113	60.02	1.863	60.02	1.793
B-6	BASE	5yr-24hr	12.15	3.723	4.870	-0.0012	113	12.03	1.316	11.82	1.426
B-7	BASE	100yr-72hr	60.29	4.920	5.220	0.0012	973	60.02	1.491	60.89	1.053
B-7	BASE	10yr-24hr	12.29	4.353	5.220	-0.0007	737	12.03	1.133	12.66	1.174
B-7	BASE	25yr-72hr	60.23	4.607	5.220	-0.0009	843	60.02	1.278	60.75	1.109
B-7	BASE	5yr-24hr	12.16	3.702	5.220	0.0004	465	12.03	0.902	12.28	0.881
B-8	BASE	100yr-72hr	60.25	5.133	4.900	0.0014	1504	60.02	2.360	59.97	2.220
B-8	BASE	10yr-24hr	12.26	4.581	4.900	-0.0008	114	12.03	1.794	12.04	1.676
B-8	BASE	25yr-72hr	60.15	4.843	4.900	0.0009	115	60.02	2.023	60.02	1.953
B-8	BASE	5yr-24hr	12.14	3.940	4.900	-0.0008	114	12.03	1.428	12.01	1.310
B-9	BASE	100yr-72hr	60.29	5.133	4.860	0.0014	2355	60.02	2.298	59.95	2.115
B-9	BASE	10yr-24hr	12.25	4.590	4.860	-0.0007	114	12.03	1.747	12.04	1.626
B-9	BASE	25yr-72hr	60.14	4.855	4.860	0.0009	114	60.02	1.970	60.03	1.899
B-9	BASE	5yr-24hr	12.14	3.948	4.860	0.0005	114	12.03	1.391	12.01	1.265
D-1	BASE	100yr-72hr	60.20	3.333	6.500	0.0070	122	59.76	14.398	0.00	0.000
D-1	BASE	10yr-24hr	12.26	2.766	6.500	-0.0063	122	11.99	12.837	0.00	0.000
D-1	BASE	25yr-72hr	60.19	3.006	6.500	0.0058	122	59.80	14.286	0.00	0.000
D-1	BASE	5yr-24hr	12.09	2.396	6.500	-0.0042	122	12.02	14.031	0.00	0.000
D-2	BASE	100yr-72hr	60.96	4.941	6.500	0.0097	360	60.96	52.648	60.96	52.648
D-2	BASE	10yr-24hr	12.77	3.837	6.500	0.0024	360	12.77	54.813	12.77	54.813
D-2	BASE	25yr-72hr	60.84	4.941	6.500	0.0097	360	60.84	52.648	60.84	52.648
D-2	BASE	5yr-24hr	12.46	3.837	6.500	0.0023	360	12.46	54.812	12.46	54.812
D-3	BASE	100yr-72hr	60.96	8.066	6.500	-0.0099	119	59.72	11.717	60.94	11.352
D-3	BASE	10yr-24hr	12.77	7.233	6.500	-0.0082	119	11.51	10.078	12.77	9.187
D-3	BASE	25yr-72hr	60.84	8.066	6.500	-0.0100	119	59.74	11.694	60.82	11.352
D-3	BASE	5yr-24hr	12.46	7.233	6.500	-0.0078	119	11.70	10.078	12.46	9.187
D-3A	BASE	100yr-72hr	60.96	7.148	6.500	0.0057	135	60.95	52.648	60.96	52.648
D-3A	BASE	10yr-24hr	12.77	6.229	6.500	-0.0035	135	12.77	54.813	12.77	54.813
D-3A	BASE	25yr-72hr	60.84	7.148	6.500	0.0057	135	60.84	52.648	60.84	52.648
D-3A	BASE	5yr-24hr	12.46	6.229	6.500	-0.0034	135	12.46	54.812	12.46	54.812
GROUNDWATER	BASE	100yr-72hr	0.00	2.250	0.000	0.0000	0	60.96	11.352	0.00	0.000
GROUNDWATER	BASE	10yr-24hr	0.00	2.250	0.000	0.0000	0	12.77	9.187	0.00	0.000
GROUNDWATER	BASE	25yr-72hr	0.00	2.250	0.000	0.0000	0	60.84	11.352	0.00	0.000
GROUNDWATER	BASE	5yr-24hr	0.00	2.250	0.000	0.0000	0	12.46	9.187	0.00	0.000
J-1	BASE	100yr-72hr	60.20	3.325	5.800	0.0070	225	59.95	74.277	59.83	77.056
J-1	BASE	10yr-24hr	12.26	2.759	5.800	0.0100	227	12.61	71.947	11.99	77.581
J-1	BASE	25yr-72hr	60.19	2.999	5.800	0.0069	226	60.07	74.242	59.89	77.034
J-1	BASE	5yr-24hr	12.09	2.396	5.800	-0.0062	257	12.16	64.417	12.06	72.668
J-10	BASE	100yr-72hr	60.21	5.192	5.860	-0.0029	133	61.06	13.655	61.09	14.794
J-10	BASE	10yr-24hr	12.29	4.672	5.860	-0.0028	133	12.74	13.537	12.72	14.573
J-10	BASE	25yr-72hr	60.17	4.903	5.860	-0.0037	133	60.83	13.988	60.80	15.576
J-10	BASE	5yr-24hr	12.16	4.067	5.860	0.0026	133	12.35	12.098	12.35	13.346
J-11	BASE	100yr-72hr	60.23	5.279	5.950	0.0019	137	61.05	14.025	61.06	13.184
J-11	BASE	10yr-24hr	12.30	4.757	5.950	-0.0017	137	12.66	12.884	12.74	12.648
J-11	BASE	25yr-72hr	60.18	4.988	5.950	0.0018	137	60.75	13.742	60.78	13.232
J-11	BASE	5yr-24hr	12.17	4.167	5.950	0.0012	199	11.97	10.968	12.35	11.012



Mary Brickell Village Drainage Improvements  
Final Design  
Node Maximum Conditions Report

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
J-12	BASE	100yr-72hr	60.30	5.447	4.650	-0.0029	136	59.74	12.578	61.05	13.252
J-12	BASE	10yr-24hr	12.33	4.918	4.650	-0.0024	136	11.93	11.156	12.66	11.981
J-12	BASE	25yr-72hr	60.24	5.151	4.650	-0.0026	136	60.76	11.825	60.75	12.914
J-12	BASE	5yr-24hr	12.17	4.306	4.650	-0.0017	273	11.95	10.357	11.97	9.640
J-13	BASE	100yr-72hr	60.15	5.231	10.080	0.0017	147	60.02	2.232	60.04	2.139
J-13	BASE	10yr-24hr	12.28	4.695	10.080	-0.0012	148	12.05	1.697	12.10	1.567
J-13	BASE	25yr-72hr	60.14	4.936	10.080	0.0014	148	60.02	1.913	60.04	1.830
J-13	BASE	5yr-24hr	12.16	4.088	10.080	0.0010	148	12.05	1.351	12.36	1.246
J-14	BASE	100yr-72hr	72.49	11.091	6.500	0.0009	114	4.77	1.570	0.00	0.000
J-14	BASE	10yr-24hr	48.00	9.530	6.500	0.0025	114	3.04	1.407	0.00	0.000
J-14	BASE	25yr-72hr	72.49	10.614	6.500	0.0010	114	5.52	1.302	0.00	0.000
J-14	BASE	5yr-24hr	48.00	9.046	6.500	0.0024	114	3.66	1.315	0.00	0.000
J-2	BASE	100yr-72hr	60.20	3.817	5.000	0.0097	133	59.96	73.823	59.95	74.277
J-2	BASE	10yr-24hr	12.26	3.251	5.000	0.0099	133	12.00	66.433	12.61	71.947
J-2	BASE	25yr-72hr	60.19	3.490	5.000	-0.0100	133	60.08	73.608	60.07	74.242
J-2	BASE	5yr-24hr	12.09	2.554	5.000	-0.0053	222	12.14	64.143	12.16	64.417
J-3	BASE	100yr-72hr	60.29	4.644	4.200	-0.0044	143	60.76	32.730	60.76	37.396
J-3	BASE	10yr-24hr	12.28	4.092	4.200	0.0017	417	12.00	29.715	12.49	29.381
J-3	BASE	25yr-72hr	60.23	4.336	4.200	-0.0042	293	60.08	31.736	60.38	35.626
J-3	BASE	5yr-24hr	12.15	3.417	4.200	0.0016	597	12.13	28.613	12.14	28.549
J-4	BASE	100yr-72hr	60.31	4.719	4.600	0.0017	169	60.88	27.534	60.89	27.031
J-4	BASE	10yr-24hr	12.29	4.160	4.600	0.0009	408	12.48	24.947	12.52	24.396
J-4	BASE	25yr-72hr	60.23	4.396	4.600	-0.0011	301	60.58	26.114	60.60	25.414
J-4	BASE	5yr-24hr	12.15	3.521	4.600	0.0009	949	12.13	22.626	12.15	22.538
J-5	BASE	100yr-72hr	60.30	4.884	5.300	-0.0022	148	60.98	18.603	60.92	19.446
J-5	BASE	10yr-24hr	12.28	4.316	5.300	0.0017	148	12.01	17.978	12.54	18.688
J-5	BASE	25yr-72hr	60.23	4.572	5.300	-0.0017	148	60.08	18.171	60.63	19.002
J-5	BASE	5yr-24hr	12.15	3.668	5.300	0.0005	503	12.13	17.240	12.15	17.211
J-6	BASE	100yr-72hr	60.32	5.049	5.200	-0.0016	138	59.78	17.037	60.98	17.128
J-6	BASE	10yr-24hr	12.29	4.498	5.200	-0.0025	138	11.97	16.435	11.97	16.180
J-6	BASE	25yr-72hr	60.22	4.748	5.200	-0.0016	138	59.82	16.624	60.63	16.342
J-6	BASE	5yr-24hr	12.15	3.863	5.200	-0.0028	138	12.07	15.646	12.08	15.488
J-7	BASE	100yr-72hr	60.35	5.270	4.400	0.0050	138	60.98	15.697	60.99	15.902
J-7	BASE	10yr-24hr	12.31	4.742	4.400	0.0054	138	11.96	14.008	12.53	14.081
J-7	BASE	25yr-72hr	60.24	4.986	4.400	0.0044	138	59.73	14.906	60.63	14.907
J-7	BASE	5yr-24hr	12.15	4.130	4.400	0.0049	138	11.92	13.797	12.07	13.156
J-8	BASE	100yr-72hr	60.29	4.933	4.860	0.0051	137	61.07	12.612	61.12	15.320
J-8	BASE	10yr-24hr	12.30	4.448	4.860	0.0033	137	12.69	11.260	12.69	11.282
J-8	BASE	25yr-72hr	60.22	4.657	4.860	-0.0038	137	60.77	11.962	60.82	12.747
J-8	BASE	5yr-24hr	12.16	3.825	4.860	-0.0035	137	12.04	8.987	12.04	9.002
J-9	BASE	100yr-72hr	60.34	5.000	4.000	-0.0024	133	61.05	11.929	61.05	12.081
J-9	BASE	10yr-24hr	12.33	4.532	4.000	-0.0029	133	12.69	10.192	12.69	10.381
J-9	BASE	25yr-72hr	60.25	4.735	4.000	-0.0028	133	60.76	11.074	60.76	11.244
J-9	BASE	5yr-24hr	12.17	3.935	4.000	0.0013	133	12.03	7.760	12.04	7.502
P-1	BASE	100yr-72hr	60.96	15.807	6.500	0.0117	137	7.05	32.000	60.96	32.000
P-1	BASE	10yr-24hr	12.77	14.967	6.500	-0.0117	137	4.29	32.000	12.77	32.000
P-1	BASE	25yr-72hr	60.84	15.807	6.500	0.0117	137	8.16	32.000	60.84	32.000
P-1	BASE	5yr-24hr	12.46	14.967	6.500	-0.0117	137	5.10	32.000	11.92	32.003

Mary Brickell Village Drainage Improvements  
Final Design  
Node Maximum Conditions Report

Name	Group	Simulation	Max Time Stage hrs	Max Stage ft	Warning Stage ft	Max Delta Stage ft	Max Surf Area ft2	Max Time Inflow hrs	Max Inflow cfs	Max Time Outflow hrs	Max Outflow cfs
P-2	BASE	100yr-72hr	60.96	15.807	6.500	0.0117	137	59.70	32.000	60.96	32.000
P-2	BASE	10yr-24hr	12.77	14.967	6.500	0.0117	137	11.82	32.000	12.77	32.000
P-2	BASE	25yr-72hr	60.84	15.807	6.500	0.0117	137	59.72	32.000	60.84	32.000
P-2	BASE	5yr-24hr	12.46	14.967	6.500	0.0117	137	11.92	32.000	12.46	32.000
VALVEBOX	BASE	100yr-72hr	60.96	8.086	6.500	-0.0077	183	60.96	64.000	60.95	64.000
VALVEBOX	BASE	10yr-24hr	12.77	7.246	6.500	-0.0039	183	12.77	64.000	12.77	64.000
VALVEBOX	BASE	25yr-72hr	60.84	8.086	6.500	-0.0073	183	60.84	64.000	60.84	64.000
VALVEBOX	BASE	5yr-24hr	12.46	7.246	6.500	-0.0039	183	12.46	63.999	12.46	63.999
W-1	BASE	100yr-72hr	60.96	8.000	8.000	-0.0038	116	60.94	5.676	60.96	5.676
W-1	BASE	10yr-24hr	12.77	7.190	8.000	-0.0039	116	12.77	4.594	12.77	4.594
W-1	BASE	25yr-72hr	60.84	8.000	8.000	-0.0038	116	60.82	5.676	60.84	5.676
W-1	BASE	5yr-24hr	12.46	7.189	8.000	-0.0039	116	12.46	4.594	12.46	4.594
W-2	BASE	100yr-72hr	60.96	8.000	8.000	-0.0038	116	60.94	5.676	60.96	5.676
W-2	BASE	10yr-24hr	12.77	7.190	8.000	-0.0039	116	12.77	4.594	12.77	4.594
W-2	BASE	25yr-72hr	60.84	8.000	8.000	-0.0038	116	60.82	5.676	60.84	5.676
W-2	BASE	5yr-24hr	12.46	7.189	8.000	-0.0039	116	12.46	4.594	12.46	4.594
WATERWAY	BASE	100yr-72hr	0.00	3.800	2.600	1.2000	122	60.96	52.648	0.00	0.000
WATERWAY	BASE	10yr-24hr	0.00	2.600	2.600	0.0000	122	12.77	54.813	0.00	0.000
WATERWAY	BASE	25yr-72hr	0.00	3.800	2.600	1.2000	122	60.84	52.648	0.00	0.000
WATERWAY	BASE	5yr-24hr	0.00	2.600	2.600	0.0000	122	12.46	54.812	0.00	0.000
WETWELL	BASE	100yr-72hr	60.20	3.147	6.500	-0.0100	495	59.96	75.036	59.70	64.000
WETWELL	BASE	10yr-24hr	12.26	2.473	6.500	-0.0092	497	12.00	65.672	11.82	64.000
WETWELL	BASE	25yr-72hr	60.19	2.770	6.500	-0.0100	497	60.08	75.034	59.72	64.000
WETWELL	BASE	5yr-24hr	12.08	2.101	6.500	-0.0100	497	12.08	66.853	11.92	64.000

Mary Brickell Village Drainage Improvements  
Final Design  
Link Maximum Conditions Report

Name	Group	Simulation	Max Time Flow hrs	Max Flow cfs	Max Delta Q cfs	Max Time US Stage hrs	Max US Stage ft	Max Time DS Stage hrs	Max DS Stage ft
B1-J2	BASE	100yr-72hr	59.96	61.361	9.526	60.26	4.529	60.20	3.817
B1-J2	BASE	10yr-24hr	12.00	57.618	9.526	12.28	4.038	12.26	3.251
B1-J2	BASE	25yr-72hr	60.08	61.842	9.525	60.22	4.242	60.19	3.490
B1-J2	BASE	5yr-24hr	12.14	55.991	9.525	12.15	3.357	12.09	2.554
B10-J7	BASE	100yr-72hr	61.00	6.124	-3.224	60.41	5.295	60.35	5.270
B10-J7	BASE	10yr-24hr	11.85	4.255	1.992	12.33	4.779	12.31	4.742
B10-J7	BASE	25yr-72hr	60.68	4.893	3.580	60.29	5.014	60.24	4.986
B10-J7	BASE	5yr-24hr	11.92	4.248	-3.025	12.15	4.177	12.15	4.130
B11-J7	BASE	100yr-72hr	60.99	5.611	-1.938	60.41	5.311	60.35	5.270
B11-J7	BASE	10yr-24hr	12.63	4.318	-1.939	12.33	4.802	12.31	4.742
B11-J7	BASE	25yr-72hr	60.73	4.984	-1.936	60.28	5.034	60.24	4.986
B11-J7	BASE	5yr-24hr	11.88	3.837	-1.981	12.15	4.202	12.15	4.130
B12-J7	BASE	100yr-72hr	60.05	10.187	-0.630	60.28	5.424	60.35	5.270
B12-J7	BASE	10yr-24hr	12.03	9.024	-0.530	12.28	4.876	12.31	4.742
B12-J7	BASE	25yr-72hr	60.06	9.668	-0.603	60.20	5.146	60.24	4.986
B12-J7	BASE	5yr-24hr	12.07	8.056	-0.556	12.14	4.261	12.15	4.130
B13-B12	BASE	100yr-72hr	59.99	7.411	-0.549	60.17	5.601	60.28	5.424
B13-B12	BASE	10yr-24hr	12.07	6.292	-0.540	12.20	4.997	12.28	4.876
B13-B12	BASE	25yr-72hr	60.01	6.902	-0.544	60.13	5.318	60.20	5.146
B13-B12	BASE	5yr-24hr	12.10	4.784	0.541	12.13	4.369	12.14	4.261
B14-B13	BASE	100yr-72hr	59.98	6.279	-0.286	60.11	5.882	60.17	5.601
B14-B13	BASE	10yr-24hr	12.06	5.469	-0.244	12.13	5.198	12.20	4.997
B14-B13	BASE	25yr-72hr	60.00	5.929	-0.278	60.09	5.581	60.13	5.318
B14-B13	BASE	5yr-24hr	12.09	4.166	-0.255	12.13	4.509	12.13	4.369
B15-B14	BASE	100yr-72hr	59.85	2.804	-0.408	60.15	6.218	60.11	5.882
B15-B14	BASE	10yr-24hr	12.07	2.525	-0.363	12.10	5.509	12.13	5.198
B15-B14	BASE	25yr-72hr	59.94	2.700	-0.405	60.10	5.924	60.09	5.581
B15-B14	BASE	5yr-24hr	12.09	1.922	-0.362	12.12	4.697	12.13	4.509
B16-B14	BASE	100yr-72hr	0.00	0.000	0.000	0.00	0.000	0.00	0.000
B16-B14	BASE	10yr-24hr	0.00	0.000	0.000	0.00	0.000	0.00	0.000
B16-B14	BASE	25yr-72hr	0.00	0.000	0.000	0.00	0.000	0.00	0.000
B16-B14	BASE	5yr-24hr	0.00	0.000	0.000	0.00	0.000	0.00	0.000
B17-B16	BASE	100yr-72hr	7.16	0.038	-0.037	72.33	10.166	72.33	10.166
B17-B16	BASE	10yr-24hr	11.70	0.090	0.037	24.33	9.414	24.33	9.414
B17-B16	BASE	25yr-72hr	8.15	0.024	0.028	72.33	9.943	72.33	9.943
B17-B16	BASE	5yr-24hr	11.92	0.123	0.035	24.33	9.170	24.33	9.170
B18-B1	BASE	100yr-72hr	61.13	29.299	-4.179	60.27	4.912	60.26	4.529
B18-B1	BASE	10yr-24hr	12.73	27.604	-4.160	12.29	4.423	12.28	4.038
B18-B1	BASE	25yr-72hr	60.81	28.803	-4.272	60.21	4.634	60.22	4.242
B18-B1	BASE	5yr-24hr	12.42	24.635	-4.273	12.16	3.792	12.15	3.357
B19-J8	BASE	100yr-72hr	59.89	2.175	0.439	60.28	4.950	60.29	4.933
B19-J8	BASE	10yr-24hr	12.06	1.769	-0.390	12.29	4.465	12.30	4.448
B19-J8	BASE	25yr-72hr	59.97	2.005	-0.387	60.21	4.675	60.22	4.657
B19-J8	BASE	5yr-24hr	12.32	1.538	0.448	12.16	3.840	12.16	3.825
B2-J3	BASE	100yr-72hr	59.96	5.554	-1.240	60.24	4.820	60.29	4.644
B2-J3	BASE	10yr-24hr	12.03	4.811	-0.975	12.26	4.250	12.28	4.092
B2-J3	BASE	25yr-72hr	60.08	5.403	-1.204	60.20	4.493	60.23	4.336
B2-J3	BASE	5yr-24hr	12.12	4.100	-0.925	12.14	3.560	12.15	3.417

Mary Brickell Village Drainage Improvements  
 Final Design  
 Link Maximum Conditions Report

Name	Group	Simulation	Max Time Flow hrs	Max Flow cfs	Max Delta Q cfs	Max Time US Stage hrs	Max US Stage ft	Max Time DS Stage hrs	Max DS Stage ft
B20-J9	BASE	100yr-72hr	61.03	5.796	-0.065	60.40	5.070	60.34	5.000
B20-J9	BASE	10yr-24hr	12.68	4.926	-0.041	12.36	4.615	12.33	4.532
B20-J9	BASE	25yr-72hr	60.76	5.347	-0.067	60.29	4.812	60.25	4.735
B20-J9	BASE	5yr-24hr	12.03	3.874	-0.017	12.18	4.033	12.17	3.935
B21-J9	BASE	100yr-72hr	61.12	6.910	-0.021	60.42	5.081	60.34	5.000
B21-J9	BASE	10yr-24hr	12.70	5.324	-0.073	12.37	4.626	12.33	4.532
B21-J9	BASE	25yr-72hr	60.80	5.901	-0.062	60.31	4.822	60.25	4.735
B21-J9	BASE	5yr-24hr	12.04	4.060	-0.007	12.18	4.055	12.17	3.935
B22-B18	BASE	100yr-72hr	61.10	18.610	3.742	60.20	5.137	60.27	4.912
B22-B18	BASE	10yr-24hr	12.72	19.000	3.823	12.29	4.622	12.29	4.423
B22-B18	BASE	25yr-72hr	60.83	19.268	3.716	60.17	4.850	60.21	4.634
B22-B18	BASE	5yr-24hr	12.36	17.709	3.505	12.16	4.009	12.16	3.792
B23-J11	BASE	100yr-72hr	60.05	2.095	-0.443	60.16	5.336	60.23	5.279
B23-J11	BASE	10yr-24hr	11.97	1.660	-0.401	12.29	4.792	12.30	4.757
B23-J11	BASE	25yr-72hr	60.05	1.817	-0.422	60.15	5.036	60.18	4.988
B23-J11	BASE	5yr-24hr	12.06	1.457	-0.001	12.17	4.189	12.17	4.167
B24-J12	BASE	100yr-72hr	59.74	4.727	1.669	60.33	5.529	60.30	5.447
B24-J12	BASE	10yr-24hr	11.85	4.485	-1.536	12.35	4.995	12.33	4.918
B24-J12	BASE	25yr-72hr	60.76	4.570	-1.485	60.27	5.230	60.24	5.151
B24-J12	BASE	5yr-24hr	11.93	4.476	1.467	12.17	4.397	12.17	4.306
B25-J12	BASE	100yr-72hr	61.10	8.992	-0.926	60.35	5.675	60.30	5.447
B25-J12	BASE	10yr-24hr	12.72	8.301	-0.983	12.37	5.129	12.33	4.918
B25-J12	BASE	25yr-72hr	60.81	8.929	-0.962	60.28	5.370	60.24	5.151
B25-J12	BASE	5yr-24hr	12.02	6.580	1.881	12.19	4.553	12.17	4.306
B26-J13	BASE	100yr-72hr	60.02	2.232	0.001	60.02	6.096	60.02	4.912
B26-J13	BASE	10yr-24hr	12.05	1.697	-0.001	12.05	5.926	12.05	4.844
B26-J13	BASE	25yr-72hr	60.02	1.913	0.001	60.02	5.995	60.02	4.872
B26-J13	BASE	5yr-24hr	12.05	1.351	0.001	12.05	5.815	12.05	4.798
B27-J14	BASE	100yr-72hr	4.77	1.495	-1.686	72.33	11.091	72.49	11.091
B27-J14	BASE	10yr-24hr	3.04	1.185	-1.411	24.33	9.530	48.00	9.530
B27-J14	BASE	25yr-72hr	5.52	1.209	-1.380	72.33	10.614	72.49	10.614
B27-J14	BASE	5yr-24hr	3.66	1.106	-1.322	24.33	9.047	48.00	9.046
B28-J14	BASE	100yr-72hr	7.16	0.381	0.599	72.49	11.091	72.49	11.091
B28-J14	BASE	10yr-24hr	4.29	0.564	0.449	48.00	9.530	48.00	9.530
B28-J14	BASE	25yr-72hr	8.16	0.343	0.339	72.49	10.614	72.49	10.614
B28-J14	BASE	5yr-24hr	5.10	0.554	0.480	48.00	9.047	48.00	9.046
B3-J3	BASE	100yr-72hr	60.76	3.289	-0.126	60.33	4.678	60.29	4.644
B3-J3	BASE	10yr-24hr	12.07	2.783	-0.034	12.29	4.134	12.28	4.092
B3-J3	BASE	25yr-72hr	59.92	2.998	-0.125	60.25	4.370	60.23	4.336
B3-J3	BASE	5yr-24hr	12.00	2.234	-0.036	12.15	3.458	12.15	3.417
B4-J4	BASE	100yr-72hr	59.69	6.388	-4.902	60.32	4.730	60.31	4.719
B4-J4	BASE	10yr-24hr	11.81	5.981	4.197	12.29	4.173	12.29	4.160
B4-J4	BASE	25yr-72hr	59.71	6.306	-4.891	60.24	4.408	60.23	4.396
B4-J4	BASE	5yr-24hr	11.89	6.038	4.782	12.15	3.533	12.15	3.521
B5-J4	BASE	100yr-72hr	60.90	5.029	-2.666	60.37	4.775	60.31	4.719
B5-J4	BASE	10yr-24hr	11.82	4.273	-1.894	12.30	4.241	12.29	4.160
B5-J4	BASE	25yr-72hr	59.72	4.608	2.757	60.27	4.460	60.23	4.396
B5-J4	BASE	5yr-24hr	11.91	4.335	-2.720	12.14	3.605	12.15	3.521

Mary Brickell Village Drainage Improvements  
Final Design  
Link Maximum Conditions Report

Name	Group	Simulation	Max Time Flow hrs	Max Flow cfs	Max Delta Q cfs	Max Time US Stage hrs	Max US Stage ft	Max Time DS Stage hrs	Max DS Stage ft
B6-J5	BASE	100yr-72hr	60.02	2.091	-0.936	60.24	4.946	60.30	4.884
B6-J5	BASE	10yr-24hr	12.04	1.549	-0.935	12.26	4.376	12.28	4.316
B6-J5	BASE	25yr-72hr	60.02	1.793	-0.935	60.18	4.633	60.23	4.572
B6-J5	BASE	5yr-24hr	11.82	1.426	-0.934	12.15	3.723	12.15	3.668
B7-J5	BASE	100yr-72hr	60.89	1.053	0.063	60.29	4.920	60.30	4.884
B7-J5	BASE	10yr-24hr	12.66	1.174	0.066	12.29	4.353	12.28	4.316
B7-J5	BASE	25yr-72hr	60.75	1.109	-0.069	60.23	4.607	60.23	4.572
B7-J5	BASE	5yr-24hr	12.28	0.881	-0.066	12.16	3.702	12.15	3.668
B8-J6	BASE	100yr-72hr	59.97	2.220	0.598	60.25	5.133	60.32	5.049
B8-J6	BASE	10yr-24hr	12.04	1.676	0.589	12.26	4.581	12.29	4.498
B8-J6	BASE	25yr-72hr	60.02	1.953	0.600	60.15	4.843	60.22	4.748
B8-J6	BASE	5yr-24hr	12.01	1.310	0.582	12.14	3.940	12.15	3.863
B9-J6	BASE	100yr-72hr	59.95	2.115	-0.206	60.29	5.133	60.32	5.049
B9-J6	BASE	10yr-24hr	12.04	1.626	-0.175	12.25	4.590	12.29	4.498
B9-J6	BASE	25yr-72hr	60.03	1.899	-0.201	60.14	4.855	60.22	4.748
B9-J6	BASE	5yr-24hr	12.01	1.265	-0.170	12.14	3.948	12.15	3.863
D1-D2	BASE	100yr-72hr	0.00	0.000	0.000	60.20	3.333	60.20	3.333
D1-D2	BASE	10yr-24hr	0.00	0.000	0.000	12.26	2.766	12.26	2.766
D1-D2	BASE	25yr-72hr	0.00	0.000	0.000	60.19	3.006	60.19	3.006
D1-D2	BASE	5yr-24hr	0.00	0.000	0.000	12.09	2.396	12.09	2.396
D2-WW	BASE	100yr-72hr	60.96	52.648	-53.993	60.96	4.941	0.00	3.800
D2-WW	BASE	10yr-24hr	12.77	54.813	3.120	12.77	3.837	0.00	2.600
D2-WW	BASE	25yr-72hr	60.84	52.648	-53.993	60.84	4.941	0.00	3.800
D2-WW	BASE	5yr-24hr	12.46	54.812	3.117	12.46	3.837	0.00	2.600
D3-W1	BASE	100yr-72hr	60.94	5.676	3.336	60.96	8.066	60.96	8.000
D3-W1	BASE	10yr-24hr	12.77	4.594	-2.806	12.77	7.233	12.77	7.190
D3-W1	BASE	25yr-72hr	60.82	5.676	3.342	60.84	8.066	60.84	8.000
D3-W1	BASE	5yr-24hr	12.46	4.594	-2.741	12.46	7.233	12.46	7.189
D3-W2	BASE	100yr-72hr	60.94	5.676	3.336	60.96	8.066	60.96	8.000
D3-W2	BASE	10yr-24hr	12.77	4.594	-2.806	12.77	7.233	12.77	7.190
D3-W2	BASE	25yr-72hr	60.82	5.676	3.342	60.84	8.066	60.84	8.000
D3-W2	BASE	5yr-24hr	12.46	4.594	-2.741	12.46	7.233	12.46	7.189
D3A-D3	BASE	100yr-72hr	60.96	52.648	22.164	60.96	7.148	60.96	4.941
D3A-D3	BASE	10yr-24hr	12.77	54.813	6.398	12.77	6.229	12.77	3.837
D3A-D3	BASE	25yr-72hr	60.84	52.648	22.164	60.84	7.148	60.84	4.941
D3A-D3	BASE	5yr-24hr	12.46	54.812	6.397	12.46	6.229	12.46	3.837
J1-D1	BASE	100yr-72hr	59.76	14.398	18.616	60.20	3.325	60.20	3.333
J1-D1	BASE	10yr-24hr	11.99	12.837	-11.056	12.26	2.759	12.26	2.766
J1-D1	BASE	25yr-72hr	59.80	14.286	18.764	60.19	2.999	60.19	3.006
J1-D1	BASE	5yr-24hr	12.02	14.031	-10.720	12.09	2.396	12.09	2.396
J1-WETWELL	BASE	100yr-72hr	59.96	75.036	8.329	60.20	3.325	60.20	3.147
J1-WETWELL	BASE	10yr-24hr	12.00	65.672	9.142	12.26	2.759	12.26	2.473
J1-WETWELL	BASE	25yr-72hr	60.08	75.034	8.328	60.19	2.999	60.19	2.770
J1-WETWELL	BASE	5yr-24hr	12.08	66.853	9.260	12.09	2.396	12.08	2.101
J10-B22	BASE	100yr-72hr	61.09	14.794	1.270	60.21	5.192	60.20	5.137
J10-B22	BASE	10yr-24hr	12.72	14.573	-1.545	12.29	4.672	12.29	4.622
J10-B22	BASE	25yr-72hr	60.80	15.576	1.782	60.17	4.903	60.17	4.850
J10-B22	BASE	5yr-24hr	12.35	13.346	1.850	12.16	4.067	12.16	4.009

Mary Brickell Village Drainage Improvements  
 Final Design  
 Link Maximum Conditions Report

Name	Group	Simulation	Max Time Flow hrs	Max Flow cfs	Max Delta Q cfs	Max Time US Stage hrs	Max US Stage ft	Max Time DS Stage hrs	Max DS Stage ft
J11-J10	BASE	100yr-72hr	61.06	13.184	-0.999	60.23	5.279	60.21	5.192
J11-J10	BASE	10yr-24hr	12.74	12.648	-1.000	12.30	4.757	12.29	4.672
J11-J10	BASE	25yr-72hr	60.78	13.232	-0.995	60.18	4.988	60.17	4.903
J11-J10	BASE	5yr-24hr	12.35	11.012	-0.864	12.17	4.167	12.16	4.067
J12-J11	BASE	100yr-72hr	61.05	13.252	1.663	60.30	5.447	60.23	5.279
J12-J11	BASE	10yr-24hr	12.66	11.981	1.476	12.33	4.918	12.30	4.757
J12-J11	BASE	25yr-72hr	60.75	12.914	1.596	60.24	5.151	60.18	4.988
J12-J11	BASE	5yr-24hr	11.97	9.640	-0.032	12.17	4.306	12.17	4.167
J13-J10	BASE	100yr-72hr	60.04	2.139	0.094	60.15	5.231	60.21	5.192
J13-J10	BASE	10yr-24hr	12.10	1.567	-0.082	12.28	4.695	12.29	4.672
J13-J10	BASE	25yr-72hr	60.04	1.830	0.111	60.14	4.936	60.17	4.903
J13-J10	BASE	5yr-24hr	12.36	1.246	-0.081	12.16	4.088	12.16	4.067
J14-J13	BASE	100yr-72hr	0.00	0.000	0.000	0.00	0.000	0.00	0.000
J14-J13	BASE	10yr-24hr	0.00	0.000	0.000	0.00	0.000	0.00	0.000
J14-J13	BASE	25yr-72hr	0.00	0.000	0.000	0.00	0.000	0.00	0.000
J14-J13	BASE	5yr-24hr	0.00	0.000	0.000	0.00	0.000	0.00	0.000
J2-J1	BASE	100yr-72hr	59.95	74.277	-20.477	60.20	3.817	60.20	3.325
J2-J1	BASE	10yr-24hr	12.61	71.947	-20.955	12.26	3.251	12.26	2.759
J2-J1	BASE	25yr-72hr	60.07	74.242	-20.844	60.19	3.490	60.19	2.999
J2-J1	BASE	5yr-24hr	12.16	64.417	-7.441	12.09	2.554	12.09	2.396
J3-B1	BASE	100yr-72hr	60.76	37.396	6.795	60.29	4.644	60.26	4.529
J3-B1	BASE	10yr-24hr	12.49	29.381	0.803	12.28	4.092	12.28	4.038
J3-B1	BASE	25yr-72hr	60.38	35.626	6.736	60.23	4.336	60.22	4.242
J3-B1	BASE	5yr-24hr	12.14	28.549	0.795	12.15	3.417	12.15	3.357
J4-J3	BASE	100yr-72hr	60.89	27.031	-0.581	60.31	4.719	60.29	4.644
J4-J3	BASE	10yr-24hr	12.52	24.396	0.187	12.29	4.160	12.28	4.092
J4-J3	BASE	25yr-72hr	60.60	25.414	0.581	60.23	4.396	60.23	4.336
J4-J3	BASE	5yr-24hr	12.15	22.538	-0.069	12.15	3.521	12.15	3.417
J5-J4	BASE	100yr-72hr	60.92	19.446	-1.755	60.30	4.884	60.31	4.719
J5-J4	BASE	10yr-24hr	12.54	18.688	-1.641	12.28	4.316	12.29	4.160
J5-J4	BASE	25yr-72hr	60.63	19.002	-1.688	60.23	4.572	60.23	4.396
J5-J4	BASE	5yr-24hr	12.15	17.211	-0.025	12.15	3.668	12.15	3.521
J6-J5	BASE	100yr-72hr	60.98	17.128	0.366	60.32	5.049	60.30	4.884
J6-J5	BASE	10yr-24hr	11.97	16.180	0.436	12.29	4.498	12.28	4.316
J6-J5	BASE	25yr-72hr	60.63	16.342	-0.222	60.22	4.748	60.23	4.572
J6-J5	BASE	5yr-24hr	12.08	15.488	0.502	12.15	3.863	12.15	3.668
J7-J6	BASE	100yr-72hr	60.99	15.902	1.756	60.35	5.270	60.32	5.049
J7-J6	BASE	10yr-24hr	12.53	14.081	-1.746	12.31	4.742	12.29	4.498
J7-J6	BASE	25yr-72hr	60.63	14.907	1.723	60.24	4.986	60.22	4.748
J7-J6	BASE	5yr-24hr	12.07	13.156	-1.761	12.15	4.130	12.15	3.863
J8-B18	BASE	100yr-72hr	61.12	15.320	3.249	60.29	4.933	60.27	4.912
J8-B18	BASE	10yr-24hr	12.69	11.282	1.639	12.30	4.448	12.29	4.423
J8-B18	BASE	25yr-72hr	60.82	12.747	2.920	60.22	4.657	60.21	4.634
J8-B18	BASE	5yr-24hr	12.04	9.002	2.243	12.16	3.825	12.16	3.792
J9-J8	BASE	100yr-72hr	61.05	12.081	-0.086	60.34	5.000	60.29	4.933
J9-J8	BASE	10yr-24hr	12.69	10.381	-0.056	12.33	4.532	12.30	4.448
J9-J8	BASE	25yr-72hr	60.76	11.244	-0.054	60.25	4.735	60.22	4.657
J9-J8	BASE	5yr-24hr	12.04	7.502	0.104	12.17	3.935	12.16	3.825



Mary Brickell Village Drainage Improvements  
 Final Design  
 Link Maximum Conditions Report

Name	Group	Simulation	Max Time Flow hrs	Max Flow cfs	Max Delta Q cfs	Max Time US Stage hrs	Max US Stage ft	Max Time DS Stage hrs	Max DS Stage ft
P1-VB	BASE	100yr-72hr	60.96	32.000	1.089	60.96	15.807	60.96	8.086
P1-VB	BASE	10yr-24hr	12.77	32.000	1.291	12.77	14.967	12.77	7.246
P1-VB	BASE	25yr-72hr	60.84	32.000	1.089	60.84	15.807	60.84	8.086
P1-VB	BASE	5yr-24hr	11.92	32.003	1.289	12.46	14.967	12.46	7.246
P2-VB	BASE	100yr-72hr	60.96	32.000	0.994	60.96	15.807	60.96	8.086
P2-VB	BASE	10yr-24hr	12.77	32.000	1.225	12.77	14.967	12.77	7.246
P2-VB	BASE	25yr-72hr	60.84	32.000	1.050	60.84	15.807	60.84	8.086
P2-VB	BASE	5yr-24hr	12.46	32.000	1.136	12.46	14.967	12.46	7.246
PUMP 1	BASE	100yr-72hr	7.05	32.000	32.000	60.20	3.147	60.96	15.807
PUMP 1	BASE	10yr-24hr	4.29	32.000	32.000	12.26	2.473	12.77	14.967
PUMP 1	BASE	25yr-72hr	8.16	32.000	32.000	60.19	2.770	60.84	15.807
PUMP 1	BASE	5yr-24hr	5.10	32.000	32.000	12.08	2.101	12.46	14.967
PUMP 2	BASE	100yr-72hr	59.70	32.000	32.000	60.20	3.147	60.96	15.807
PUMP 2	BASE	10yr-24hr	11.82	32.000	32.000	12.26	2.473	12.77	14.967
PUMP 2	BASE	25yr-72hr	59.72	32.000	32.000	60.19	2.770	60.84	15.807
PUMP 2	BASE	5yr-24hr	11.92	32.000	32.000	12.08	2.101	12.46	14.967
VB-D3	BASE	100yr-72hr	59.72	11.717	-10.621	60.96	8.086	60.96	8.066
VB-D3	BASE	10yr-24hr	11.51	10.078	-6.452	12.77	7.246	12.77	7.233
VB-D3	BASE	25yr-72hr	59.74	11.694	-10.641	60.84	8.086	60.84	8.066
VB-D3	BASE	5yr-24hr	11.70	10.078	-6.452	12.46	7.246	12.46	7.233
VB-D3A	BASE	100yr-72hr	60.95	52.648	-6.993	60.96	8.086	60.96	7.148
VB-D3A	BASE	10yr-24hr	12.77	54.813	1.947	12.77	7.246	12.77	6.229
VB-D3A	BASE	25yr-72hr	60.84	52.648	-6.993	60.84	8.086	60.84	7.148
VB-D3A	BASE	5yr-24hr	12.46	54.812	2.142	12.46	7.246	12.46	6.229
Well 1	BASE	100yr-72hr	60.96	5.676	-0.005	60.96	8.000	0.00	2.250
Well 1	BASE	10yr-24hr	12.77	4.594	-0.004	12.77	7.190	0.00	2.250
Well 1	BASE	25yr-72hr	60.84	5.676	-0.005	60.84	8.000	0.00	2.250
Well 1	BASE	5yr-24hr	12.46	4.594	0.004	12.46	7.189	0.00	2.250
Well 2	BASE	100yr-72hr	60.96	5.676	-0.005	60.96	8.000	0.00	2.250
Well 2	BASE	10yr-24hr	12.77	4.594	-0.004	12.77	7.190	0.00	2.250
Well 2	BASE	25yr-72hr	60.84	5.676	-0.005	60.84	8.000	0.00	2.250
Well 2	BASE	5yr-24hr	12.46	4.594	0.004	12.46	7.189	0.00	2.250

**APPENDIX H – GEOTECHNICAL ENGINEERING REPORTS**

PREPARED BY:

MACTEC ENGINEERING AND CONSULTING, INC.

**REPORT OF GEOTECHNICAL SUBSURFACE EXPLORATION –  
PAVEMENT CORING**

**MARY BRICKELL VILLAGE  
SW 8<sup>TH</sup> ST TO SW 12<sup>TH</sup> ST BETWEEN SW 2<sup>ND</sup> AVE AND SE 1<sup>ST</sup> AVE  
CITY OF MIAMI, MIAMI-DADE COUNTY, FL**

**-PREPARED FOR-**

**T.Y. LINN INTERNATIONAL  
201 ALHAMBRA CIRCLE, SUITE 900  
CORAL GABLES, FLORIDA 33134**

**-PREPARED BY-**

**AMEC ENVIRONMENT & INFRASTRUCTURE, INC. (AMEC)  
5845 NW 158<sup>TH</sup> STREET  
MIAMI LAKES, FLORIDA 33014**

**AMEC PROJECT No. 6785-10-2160 TASK 01**

**OCTOBER 12, 2011**





October 12, 2011

Mr. Francisco J. Alonso  
T.Y. Linn International  
201 Alhambra Circle  
Coral Gables, Florida 33134

Subject: **Report of Geotechnical Exploration**  
**Mary Brickell Village**  
SW 8<sup>th</sup> St to SW 12<sup>th</sup> St between SW 2<sup>nd</sup> Ave and SE 1<sup>st</sup> Ave  
Miami, Florida  
AMEC Project Number 6785-10-2160 T-01

Dear Mr. Alonso:

AMEC Environment & Infrastructure, Inc. (AMEC), formally MACTEC, has completed the geotechnical services for the above referenced project. Our services were provided in accordance with the scope of services contained in our Proposal Number Prop09Miam T-70a and 70b, dated December 16, 2009 and December 15, 2011. The authorization to proceed with the geotechnical services was granted by you on May 18, 2011.


The attached report presents our findings based on the results of the field services conducted for the subject project. Pavement cores will be stored for three months and then discarded unless other arrangements are made.

We have enjoyed assisting you and look forward to serving as your geotechnical consultant on the remainder of this project and on future projects. If you have any questions, please contact us at your earliest convenience.

Sincerely,

**AMEC ENVIRONMENTAL & INFRASTRUCTURE, INC.**  
**FORMALLY MACTEC ENGINEERING AND CONSULTING, INC.**  
Florida Board of Professional Engineers Authorization No. 6090

  
Oscar Rodriguez  
Project Engineer

  
G. Thomas McDaniel, P.E.  
Principal Geotechnical Engineer  
Florida Registration 26158



Distribution: Addressee (2)  
File (1)

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## TABLE OF CONTENTS

<b>1.0</b>	<b>INTRODUCTION .....</b>	<b>1-1</b>
<b>2.0</b>	<b>PROJECT INFORMATION .....</b>	<b>2-1</b>
<b>3.0</b>	<b>FIELD SERVICES AND PAVEMENT INFORMATION .....</b>	<b>3-1</b>
3.1	SAMPLE STORAGE .....	3-2
<b>APPENDIX:</b>	Site Location Map	
	Field Exploration Location Plan	
	Test Boring Records	
	Key classification and symbols	
	Percolation Test Results	
	Field Procedures	

## 1.0 INTRODUCTION

The purpose of this geotechnical exploration and pavement coring was to develop information concerning the site and subsurface conditions in order for T.Y. Linn International to evaluate site preparation requirements and paving alternatives for the planned repaving and reconstruction of the subject site. This report briefly describes the field activities and presents the findings.

The purpose of this investigation was:

- To investigate the general subsurface conditions at the site.
- To provide information on the thickness of asphaltic and base course material of the pavement cores extracted.
- To provide results for two soil boring test and two percolation test.

The soil test borings (B-1 and B-2) were drilled to a depth of 30 and 40 feet respectively, below site pavement grade. The borings locations can be seen in the field exploration plan in the appendix. The general surface elevations at the soil borings were not provided. This report represents an evaluation of site conditions based on traditional geotechnical procedures for site characterization. The recovered soil samples were not examined, either visually or analytically for environmental hazards.

Our exploration program involved various geotechnical studies and collection of subsurface data. Your office proposed and we conducted two soil test boring tests in the westbound lane of SW 10<sup>th</sup> street and at the pump station location on SW 2<sup>nd</sup> Ave. Also, we have extracted a total of 8 core samples of the planned 13 pavement core locations, from the existing pavement at the locations indicated in the attached field exploration plan. Five asphalt core locations, C-2, C-3, C-5, C-6, and C-8 could not be cored due to utility conflicts. Two pavement cores were taken at each block, except at SE 11<sup>th</sup> Street, which due to the block length only one was taken and were designated as C-1 through C-13. Thickness of asphaltic layer and base material are measured for each of these cores extracted.

AMEC also performed two South Florida Water Management District Constant Head Percolation test at location chosen by T.Y. Linn International, see attached Field Exploration Plan for locations. The results of the testing are presented in the appendix.



## 2.0 PROJECT INFORMATION

Project information has been provided by Mr. Francisco J. Alonso of T.Y. Linn Interantional. AMEC understands the project consists of design, and reconstruction of the subject site. The main purpose of the pavement cores is primarily to understand the existing pavement depth and pavement structure condition in order to determine where to mill and resurface, or to replace the full depth pavement. The percolation tests were performed to redesign the road to address drainage issues. We understand that the following information IS NOT required:

- Cross slope
- Crack Information
- Rut depth
- Pavement Condition

### 3.0 FIELD SERVICES AND PAVEMENT INFORMATION

Six-inch diameter pavement core samples (approximately), were drilled at 8 locations at the subject site. Each pavement core were drilled to a depth of approximately 14 inches below existing ground surface or to the end of the base layer. Please refer to the Boring Location Plan presented in the Appendix of this report for specific coring locations.

The locations of the pavement cores are shown on the attached Field Exploration Plan. The lengths of asphalt cores and the thicknesses of the underlying base and sub base layers are summarized in the table below:

SUMMARY OF PAVEMENT CORING			
Core	Asphalt (inches)	Base (inches)	Lane Location
C-1*	1.875	12.125	Westbound Lane
C-2	-	-	Utility Conflict
C-3	-	-	Utility Conflict
C-4*	1	13	Westbound Lane
C-5	-	-	Utility Conflict
C-6	-	-	Utility Conflict
C-7	2.25	5	Westbound Lane
C-8	-	-	Utility Conflict
C-9*	2.5	12	Westbound Lane
C-10	2.75	5.75	Westbound Lane
C-11	2.5		Westbound Lane
C-12	2	7.125	Westbound Lane
C-13	3.5	7.5	Chevron Area North of Eastbound Lane

\*Base material termination not encountered.

The scope of the field services included performing Maintenance of Traffic (M.O.T.) to facilitate the safe operation of pavement coring and drilling equipment and personnel within the travel lanes and right of way. The underlying soil samples were measured and recorded on our field logs. At the completion of core and soil boring, each core/boring location was backfilled with drill cuttings and tamped and then patched with asphaltic concrete cold patch and tamped.

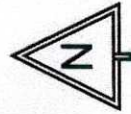
### **3.1 SAMPLE STORAGE**

The pavement cores, soil and rock samples retrieved during this exploration will be kept at our office for a period of three months from the date of this report. The samples are then discarded unless you request otherwise.

## **APPENDIX**

**Site location Map  
Field Exploration Location Plan  
Test boring records  
Key classification and symbols  
Percolation Test Results  
Field Procedures**





MACTEC Project No. 6785-10-2160 T-01

**SITE LOCATION MAP**

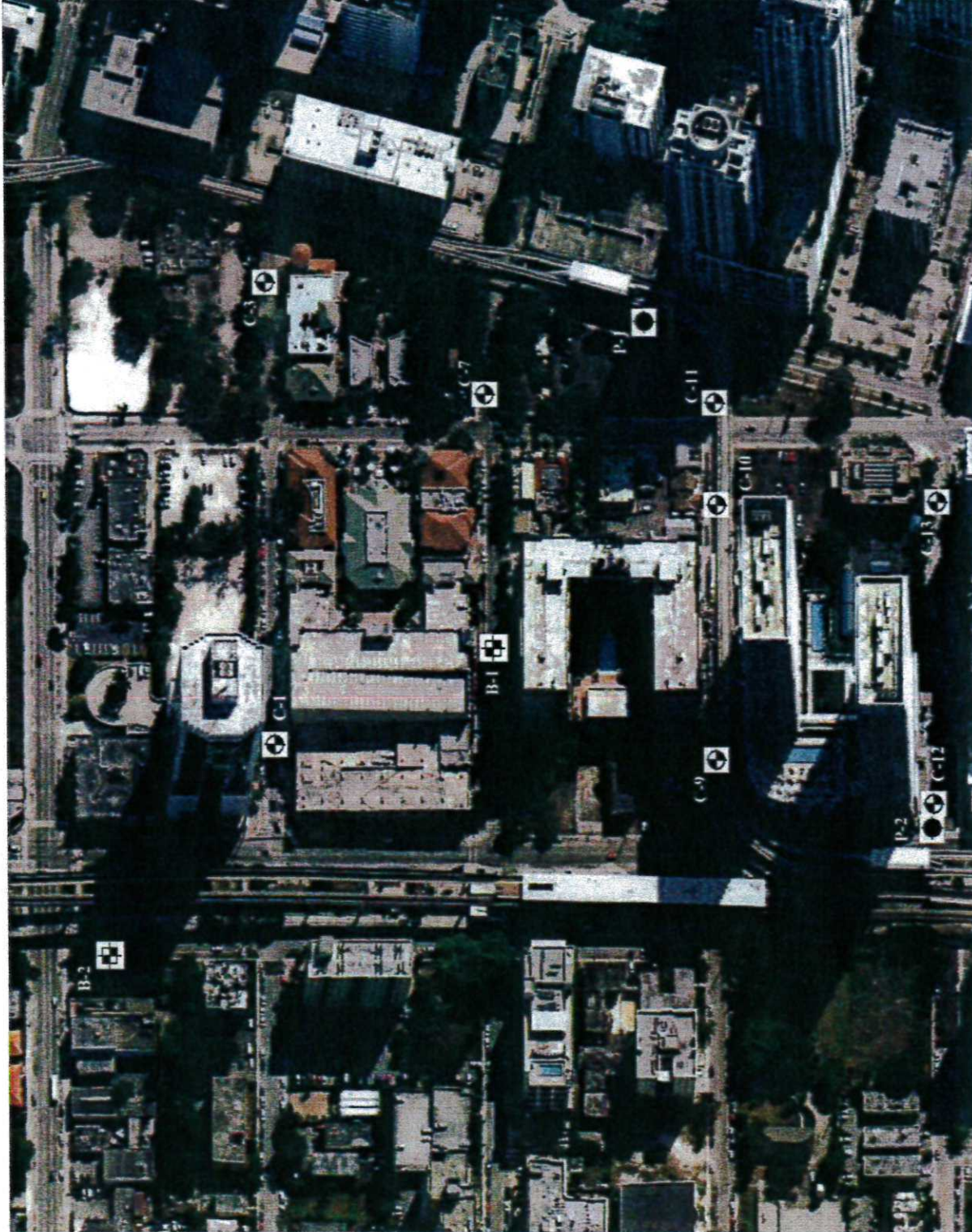
DRAWN BY: O.R. *[Signature]* DATE: 10/12/2011

CHECKED BY: *[Signature]* SCALE: NTS



**Mary Brickell Village**  
**SW 8th to 12th St, b/w SW 2nd and SE 1st Ave**  
**Miami, Florida**





**LEGEND**

- P-1 Approximate percolation test boring location and designation
- ⊕ C-1 Approximate asphalt coring location and designation
- ⊕ B-1 Approximate soil boring test location and designation

MACTEC Project No. 6785-10-2160 T-01

**Mary Brickell Village**  
**SW 8<sup>th</sup> to 12<sup>th</sup> St, b/w SW 2<sup>nd</sup> and SE 1<sup>st</sup> Ave**  
**Miami, Florida**



**FIELD EXPLORATION LOCATION PLAN**

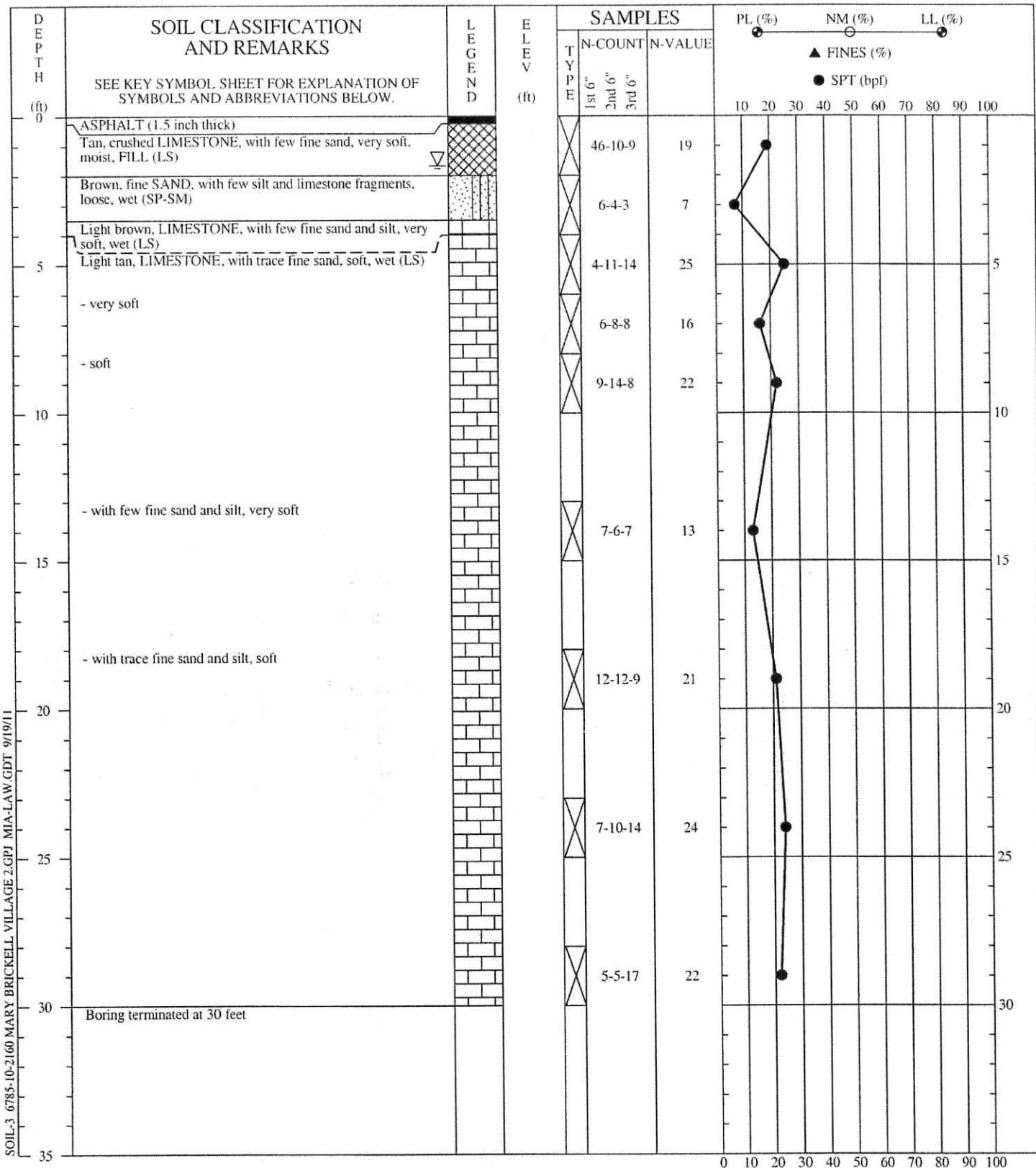
DRAWN BY: O.R.

DATE: 10/12/2011

CHECKED BY:

SCALE: NTS





SOIL-3 6785-10-2160 MARY BRICKELL VILLAGE 2.GPJ MIA-LAW GDT 9/19/11

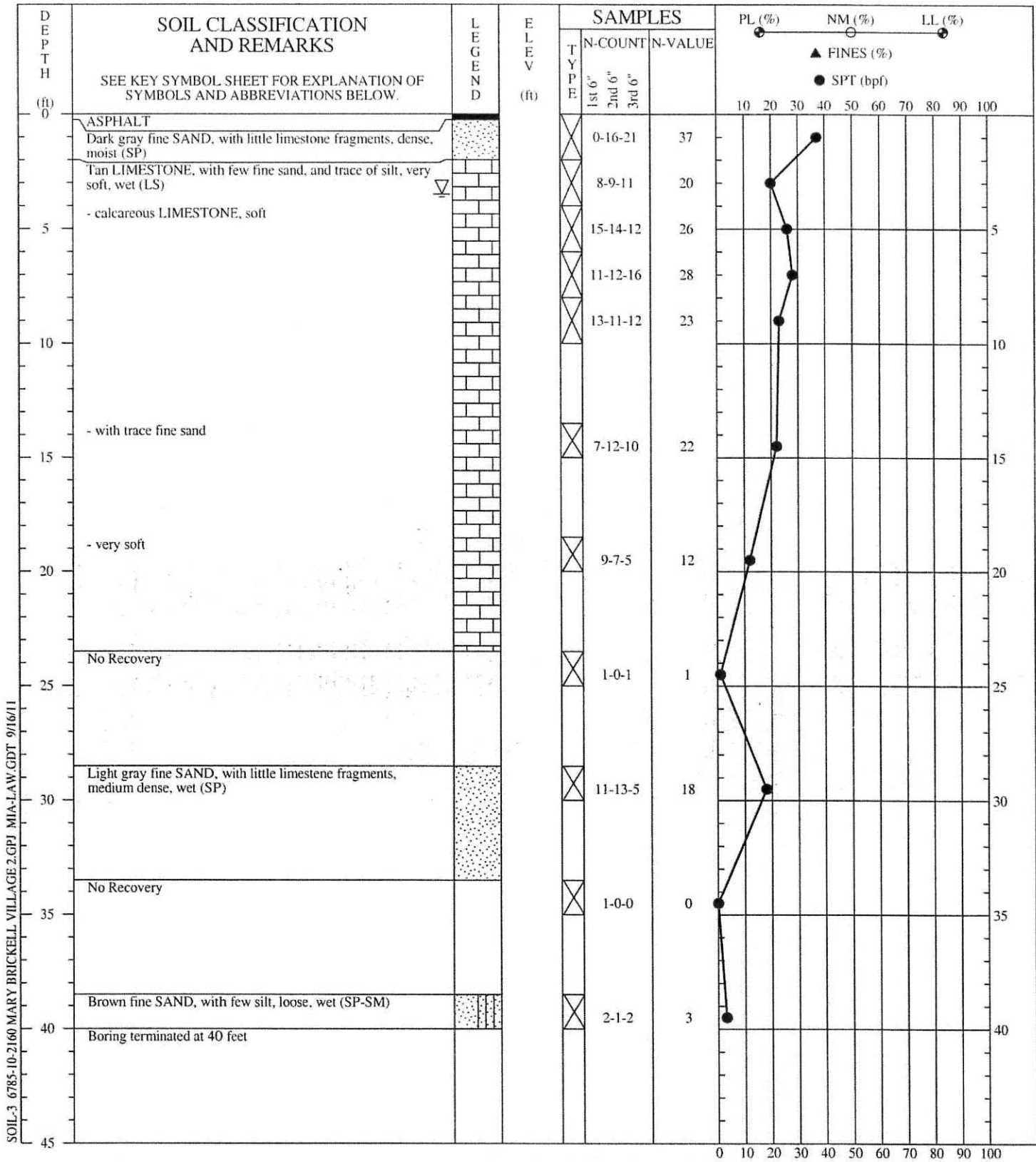
DRILLER: Helbert Avellanedo  
 EQUIPMENT: BK 66  
 METHOD: Standard Penetration Test  
 HOLE DIA.: 6-in  
 REMARKS:  
 ROTARY DRILLING:  
 GROUND WATER LEVEL: 1.67 feet  
 Checked By: *RA* Date: *10/12/11*

**PROJECT NAME:** Mary Brickell Village  
**PROJECT LOC.:** Miami, Florida  
**PROJECT No.:** 6785-10-2160  
**DRILLED:** 9/15/2011  
**BORING No.:** B-1

**PAGE 1 OF 1**

THIS RECORD IS A REASONABLE INTERPRETATION OF SUBSURFACE CONDITIONS AT THE EXPLORATION LOCATION. SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND AT OTHER TIMES MAY DIFFER. INTERFACES BETWEEN STRATA ARE APPROXIMATE. TRANSITIONS BETWEEN STRATA MAY BE GRADUAL.





SOIL-3 6785-10-2160 MARY BRICKELL VILLAGE 2.GPJ MIA-LAW.GDT 9/16/11

DRILLER: Robert Carrasco  
 EQUIPMENT: CME 55 Automatic Hammer  
 METHOD: Standard Penetration Test  
 HOLE DIA.: 6-in  
 REMARKS:  
 ROTARY DRILLING:  
 GROUND WATER LEVEL: 3.5 feet  
 Checked By: *[Signature]* Date: 10/12/11

**PROJECT NAME:** Mary Brickell Village  
**PROJECT LOC.:** Miami, Florida  
**PROJECT No.:** 6785-10-2160  
**DRILLED:** 7/5/2011  
**BORING No.:** B-2

**PAGE 1 OF 1**

THIS RECORD IS A REASONABLE INTERPRETATION OF SUBSURFACE CONDITIONS AT THE EXPLORATION LOCATION. SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND AT OTHER TIMES MAY DIFFER. INTERFACES BETWEEN STRATA ARE APPROXIMATE. TRANSITIONS BETWEEN STRATA MAY BE GRADUAL.



MAJOR DIVISIONS		GROUP SYMBOLS	TYPICAL NAMES	Undisturbed Sample (UD)	Auger Cuttings
COARSE GRAINED SOILS (More than 50% of material is LARGER than No. 200 sieve size)	GRAVELS (More than 50% of coarse fraction is LARGER than the No. 4 sieve size)	GW	Well graded gravels, gravel - sand mixtures, little or no fines.	Split Spoon Sample (SS)	Bulk Sample
	GRAVELS WITH FINES (Appreciable amount of fines)	GP	Poorly graded gravels or gravel - sand mixtures, little or no fines.	Rock Core (RC)	
SANDS (More than 50% of coarse fraction is SMALLER than the No. 4 Sieve Size)	CLEAN SANDS (Little or no fines)	GM	Silty gravels, gravel - sand - silt mixtures.	Water Table at time of drilling	Water Table after 24 hours
	CLEAN SANDS WITH FINES (Appreciable amount of fines)	GC	Clayey gravels, gravel - sand - clay mixtures.	WOH - Weight of Hammer	◀ 100% - Percent Loss of Drilling Fluid
FINE GRAINED SOILS (More than 50% of material is SMALLER than No. 200 sieve size)	SANDS (Liquid limit LESS than 50)	SW	Well graded sands, gravelly sands, little or no fines.	WOR - Weight of Drill Rods	c - cohesion estimated from pocket penetrometer
	SILTS AND CLAYS (Liquid limit LESS than 50)	SP	Poorly graded sands or gravelly sands, little or no fines.	SCP - Static Cone Penetrometer Tip Resistance (kg/sq. cm)	qu - unconfined compressive strength estimated from pocket penetrometer
SILTS AND CLAYS (Liquid limit GREATER than 50)	SANDS WITH FINES (Appreciable amount of fines)	SM	Silty sands, sand - silt mixtures	Correlation of Penetration Resistance (N) with Relative Density and Consistency	
	SANDS WITH FINES (Appreciable amount of fines)	SC	Clayey sands, sand - clay mixtures.		
SILTS AND CLAYS (Liquid limit GREATER than 50)	SANDS WITH FINES (Appreciable amount of fines)	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands or clayey silts and with slight plasticity.	No. of Blows	No. of Blows
	SANDS WITH FINES (Appreciable amount of fines)	CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays.	Very Loose	0 - 2
SILTS AND CLAYS (Liquid limit GREATER than 50)	SANDS WITH FINES (Appreciable amount of fines)	OL	Organic silts and organic silty clays of low plasticity.	Loose	3 - 4
	SANDS WITH FINES (Appreciable amount of fines)	MH	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts.	Firm	5 - 8
SILTS AND CLAYS (Liquid limit GREATER than 50)	SANDS WITH FINES (Appreciable amount of fines)	CH	Inorganic clays of high plasticity, fat clays	Very Firm	9 - 15
	SANDS WITH FINES (Appreciable amount of fines)	OH	Organic clays of medium to high plasticity, organic silts.	Dense	16 - 30
SILTS AND CLAYS (Liquid limit GREATER than 50)	SANDS WITH FINES (Appreciable amount of fines)	PT	Peat and other highly organic soils.	Very Dense	31 - 50
	SANDS WITH FINES (Appreciable amount of fines)			Over 50	Over 50
HIGHLY ORGANIC SOILS				Modifiers	
BOUNDARY CLASSIFICATIONS: Soils possessing characteristics of two groups are designated by combinations of group symbols.				These Modifiers Provide Our Estimate of The Amount of Fines (Silt or Clay Size Particles) in The Soil Sample	
SILT OR CLAY		SAND	GRAVEL	APPROX. FINES CONTENT	UNIFIED SOIL CLASSIFICATION SYMBOL
		Fine	Fine	5% TO 12%	WITH SILT OR WITH CLAY
		Medium	Coarse	12% TO 30%	SILTY OR CLAYEY
		Coarse	Coarse	30% TO 50%	VERY SILTY OR VERY CLAYEY
		No.200	No.10		SM OR SC
		No.40	No.4		SM OR SC
		No.10	3/4"		
		No.40	3"		
		No.100	12"		
U.S. STANDARD SIEVE SIZE		APPROXIMATE CONTENT, BY WEIGHT			
Reference: The Unified Soil Classification System, Corps of Engineers, U.S. Army Technical Memorandum No. 3-357, Vol. 1, March, 1953 (Revised April, 1960)		1% to 5%		MODIFIERS	
		5% to 12%		TRACE	
		12% to 30%		FEW	
		30% to 50%		SOME	
				MANY	
These Modifiers Provide Our Estimate of Shell, Rock Fragments, or Roots in The Soil Sample		ORGANIC CONTENT			
		1% TO 3%		TRACE	
		3% TO 5%		SLIGHTLY ORGANIC	
		5% TO 30%		ORGANIC	
		> 30%		PEAT	



KEY TO SYMBOLS AND DESCRIPTIONS

## KEY CLASSIFICATION AND SYMBOLS

### CORRELATION OF PENETRATION RESISTANCE WITH RELATIVE DENSITY AND CONSISTENCY

GRANULAR MATERIAL			SILTS AND CLAYS		
SPT N VALUE (BLOWS/FOOT)			SPT N VALUE (BLOWS/FOOT)		
RELATIVE DENSITY	SAFETY HAMMER	AUTOMATIC HAMMER	CONSISTENCY	SAFETY HAMMER	AUTOMATIC HAMMER
VERY LOOSE	0 - 4	0 - 3	VERY SOFT	0 - 2	0 - 1
LOOSE	5 - 10	4 - 8	SOFT	3 - 4	2 - 3
MEDIUM DENSE	11 - 30	9 - 24	FIRM	5 - 8	4 - 6
DENSE	31 - 50	25 - 40	STIFF	9 - 15	7 - 12
VERY DENSE	> 50	> 40	VERY STIFF	16 - 30	13 - 24
			HARD	> 30	> 24

ROCK HARDNESS DESCRIPTION		MODIFIERS	
VERY SOFT	Rock core crumbles when handled N < 20	APPROXIMATE PERCENTAGE	MODIFIERS
SOFT	Can break core easily with hands N = 21-30	0 to 5%	Trace
MEDIUM HARD	Can break core with hands N = 31-45	5% to 10%	Few
MODERATELY HARD	Thin edges of rock can be broken with fingers N = 46-60	15% to 25%	Little
HARD	Thin edges of rock cannot be broken with fingers N = 61-100	30% to 45%	Some
VERY HARD	Rock core rings when struck with a hammer (cherts) N > 50/2"	The modifiers provide our estimate of the percentages of gravel, sand, and fines (silt or clay size particles).	

SYMBOLS	DESCRIPTION
UD	Undisturbed sample (UD) recovered.
100/2"	N, Number of blows (100) to drive the support spoon or cone a number of inches (2").
NX, 4", 6"	Corel Barrel sizes which obtain cores 2-1/8", 3-7/8", and 5-7/8" diameter respectively.
65%	Percentage (65) of rock core and soil sample recovered
RQD	Rock Quality Design - Percent of rock core 4 or more inches long
▼	Water table at least 24 hours after drilling
△	Water table one hour or less after drilling
◀	Loss of drilling fluid



## SFWMD/DERM PERCOLATION TEST – CONSTANT HEAD

Percolation Test No.   P-1  

Date: 9/02/2011	Project Name: Mary Brickell Village
Project No. 6785-10-2160	Task No. 1
Crew: B. Carrasco	

### BOREHOLE GEOMETRY

Borehole Diameter: <u>  10.0  </u> (inches)	Solid Casing Depth: from <u>  NA  </u> (feet) to <u>  NA  </u> (feet)
Casing Diameter: <u>  4.5  </u> (inches)	Perforated Casing Depth: <u>  0  </u> (feet) to <u>  15  </u> (feet)
Borehole Depth: <u>  15  </u> (feet)	Groundwater Depth Measured from Ground Surface <u>  5'6"  </u> (feet-inches)

### PERCOLATION TEST DATA

Flushing Period: <u>  15  </u> minutes	Groundwater Depth during testing: <u>  0  </u> (feet-inches) (measured from ground surface)
--	--

### TEST RESULTS

Time (minutes)	Meter Reading		Time (minutes)	Meter Reading	
	Meter ** (Gallons)	Accumulated (Gallons)		Meter ** (Gallons)	Accumulated (Gallons)
Initial Reading	0	0	8	0.22	1.43
1	0.22	0.22	9	0.11	1.54
2	0.22	0.44	10	0.11	1.65
3	0.22	0.66	11	0.11	1.76
4	0.22	0.88	12	0.22	1.98
5	0.11	0.99	13	0.22	2.2
6	0.11	1.1	14	0.22	2.42
7	0.11	1.21	15	0.22	2.64

\*\* MEASURE WITH KNOWN VOLUME

### BORING INFORMATION

Sample No.	Depth (feet)		Soil/Rock Description
	From	To	
1	0	0.1	ASPHALT
2	0.1	1.5	Light gray, fine to coarse SAND with few limestone fragments.
3	1.5	5	Light tan, calcarious LIMESTONE.
4	5	15	Light tan to white, calcarious LIMESTONE with little fine sand and silt.

## SFWMD/DERM PERCOLATION TEST – CONSTANT HEAD

Percolation Test No.  P-2

Date: 9/16/2011		Project Name: Mary Brickell Village			
Project No. 6785-10-2160		Task No. 1			
Crew: H. Avellaneda					
<b>BOREHOLE GEOMETRY</b>					
Borehole Diameter: <u> 6.0 </u> (inches)		Solid Casing Depth: from <u> NA </u> (feet) to <u> NA </u> (feet)			
Casing Diameter: <u> 4.0 </u> (inches)		Perforated Casing Depth: <u> 0 </u> (feet) to <u> 15 </u> (feet)			
Borehole Depth: <u> 15 </u> (feet)		Groundwater Depth Measured from Ground Surface <u> 5' </u> (feet-inches)			
<b>PERCOLATION TEST DATA</b>					
Flushing Period: <u> 15 </u> minutes		Groundwater Depth during testing: <u> 0 </u> (feet-inches) (measured from ground surface)			
<b>TEST RESULTS</b>					
Time (minutes)	Meter Reading		Time (minutes)	Meter Reading	
	Meter (Gallons)	Accumulated (Gallons)		Meter ** (Gallons)	Accumulated (Gallons)
Initial Reading	0	0	8	32.14	32.14
1	4.38	4.38	9	35.68	35.68
2	8.99	8.99	10	39.04	39.04
3	13.42	13.42	11		
4	17.47	17.47	12		
5	21.34	21.34	13		
6	25.03	25.03	14		
7	28.69	28.69	15		
<b>BORING INFORMATION</b>					
Sample No.	Depth (feet)		Soil/Rock Description		
	From	To			
1	0	0.1	ASPHALT		
2	0.1	2	Light brown, LIMESTONE FILL		
3	2	15	Light brown, LIMESTONE with few fine sand.		



**SUMMARY OF PERCOLATION TEST RESULTS  
USUAL CONDITION TEST CONSTANT HEAD**

**Project Name: Mary Brickell Village**

Prepared by/Date: OR 09/19/2011

Checked by/Date: *YMM 9/16/11*

Date Performed

P-1 9/2/2011 & P-2 9/16/11

MACTEC PROJECT NO. 6785-10-2160 Task 01

Test No.	Depth to Grd. Water (ft)	Depth to Water during testing (ft)	(H2) (ft)	Borehole Depth (ft)	Borehole Diameter (inches)	Rate of Flow		k, Hydraulic Conductivity (cfs/ft <sup>2</sup> -ft. Head):
						(gpm)	(cfs)	
P-1	5.5	0.0	5.5	15	10.0	0.18	0.00039	<b>2.2E-06</b>
P-2	5.0	0.0	5.0	15	6.0	3.90	0.00869	<b>8.8E-05</b>

Note: Screen depth - from 0.0 ft to 15.0 ft below existing ground surface.

H 3= Depth of water during testing  
Dc = depth of perforations = 5 ft  
H2 = depth of water table

## FIELD PROCEDURES

**Test Borings** - The test borings were made in general accordance with ASTM-D-1586, "Penetration Test and Split-Barrel Sampling of Soils." The borings were advanced using a 3-inch ID casing (or a 6-inch ID casing in borings with rock coring) and a rotary drilling process. Water or bentonite drilling fluid was circulated in the boreholes to flush the cuttings. At regular intervals, the drilling tools were removed and soil samples were obtained with a standard 1.4-inch I.D., 2.0 inch O.D., split-tube sampler. The sampler was first seated six inches and then driven an additional foot with blows of a 140-pound hammer falling 30 inches. The number of hammer blows required to drive the sampler the final foot is designated the "Penetration Resistance". The penetration resistance, when properly interpreted, is an index to the soil strength and density.

Representative portions of the soil samples, obtained from the sampler, were placed in glass jars and transported to our laboratory. The samples were then examined by an engineer in order to confirm the field classifications.

**Percolation Testing** - The percolation test was performed in order to estimate the hydraulic conductivity of the materials encountered. The Constant Head method was used. The general procedures outlined in the South Florida Water Management District Permit Information Manual (Volume IV) were followed. Test was performed in a 5.5-inch diameter perforated PVC pipe installed in a 6.25-inch diameter hole pre-drilled to a depth of 15 feet below the existing ground surface, using a rock coring casing. The borehole was then filled with water and the water level maintained at the surface. Once the inflow stabilized or came into equilibrium with the outflow rate or seepage, the amount of water added for a period of 10 minutes was recorded and the percolation rate calculated and reported in units of CFS/FT<sup>2</sup>-FT of head.

**APPENDIX I – COST ESTIMATES**

**City of Miami Project B-30637**  
**Mary Brickell Drainage and Roadway Improvements Project - Phase I**  
**Engineer's Opinion of Probable Construction Cost**

100% Design Documents

PAY ITEM	PAY ITEM DESCRIPTION	UNIT	UNIT PRICE	PLAN QTY	FINAL QTY	COST
101-1	Mobilization	LS	\$27,786.46	1		\$27,786.46
102-1	Maintenance of Traffic	LS	\$27,786.46	1		\$27,786.46
110-1-1	Clearing and Grubbing	LS	\$27,786.46	1		\$27,786.46
285-706	Optional Base Group 06 (8" Limerock LBR 100)	SY	\$15.00	43		\$645.00
285-711	Optional Base Group 11 (12" Limerock LBR 100)	SY	\$20.00	2460		\$49,200.00
327-70-19	Milling Existing Asphalt Pavement (1" Average)	SY	\$3.00	10744		\$32,231.12
334-1-13	Superpave Asphaltic Concrete, Traffic C (110lbs/sy-in., 1" min., includes roadway and parking lanes)	TN	\$100.00	726		\$72,620.38
400-3-1	Concrete Class III, Culverts (36"x48" box culvert)	CY	\$500.00	11		\$5,500.00
415-1-6	Reinforcing Steel - Miscellaneous (36"x48" box culvert)	LB	\$1.00	700		\$700.00
425-1-351	Inlet, Curb Type P-5 , <10'	EA	\$3,500.00	2		\$7,000.00
425-1-361	Inlet, Curb Type P-6 , <10'	EA	\$4,000.00	2		\$8,000.00
425-1-521	Inlet, Ditch Bottom Type C , <10'	EA	\$3,000.00	1		\$3,000.00
425-1-905	Inlet Special, Partial (replace City of Miami Type F-3 curb inlet tops)	EA	\$1,500.00	3		\$4,500.00
425-2-61	Manholes, P-8, <10'	EA	\$3,500.00	9		\$31,500.00
425-2-71	Manholes, J-7, <10' (refer to plans for dimensions)	EA	\$6,000.00	6		\$36,000.00
430-175-112	Pipe Culvert, Optional Material, Round Shape 12" S/CD	LF	\$40.00	12		\$480.00
430-175-118	Pipe Culvert, Optional Material, Round Shape 18" S/CD	LF	\$50.00	77		\$3,850.00
430-175-124	Pipe Culvert, Optional Material, Round Shape 24" S/CD	LF	\$75.00	52		\$3,900.00
430-175-130	Pipe Culvert, Optional Material, Round Shape 30" S/CD	LF	\$90.00	625		\$56,250.00
430-175-136	Pipe Culvert, Optional Material, Round Shape 36" S/CD	LF	\$100.00	378		\$37,800.00
430-175-148	Pipe Culvert, Optional Material, Round Shape 48" S/CD	LF	\$150.00	215		\$32,250.00
430-94-1	Desilt Pipe	LF	\$4.00	3700		\$14,800.00
443-70-3	French Drain, 18" HDPE	LF	\$100.00	86		\$8,600.00
443-70-4	French Drain, 24" HDPE	LF	\$110.00	297		\$32,670.00
520-1-10	Concrete Curb Type "F"	LF	\$30.00	1440		\$43,200.00
522-1	Sidewalk Concrete, 4" Thick	SY	\$45.00	1264		\$56,880.00
527-1	Detectable Warning on Existing Walking Surface, Retrofit	EA	\$500.00	1		\$500.00
580-1-2	Landscaping Complete	LS	\$10,000.00	1		\$10,000.00
706-3	Retro-Reflective Pavement Markers	EA	\$5.00	75		\$375.00
711-11-121	Traffic Pavement Marking Thermoplastic, Solid, White, 6"	LF	\$0.50	3503		\$1,751.50
711-11-123	Traffic Pavement Marking Thermoplastic, Solid, White, 12"	LF	\$1.00	425		\$425.00
711-11-124	Traffic Pavement Marking Thermoplastic, Solid, White, 18"	LF	\$1.50	275		\$412.50
711-11-125	Traffic Pavement Marking Thermoplastic, Solid, White, 24"	LF	\$2.00	118		\$236.00
711-11-131	Traffic Pavement Marking Thermoplastic, Skip 10/30, White, 6"	GM	\$2,640.00	0.02		\$52.80
711-11-170	Traffic Pavement Marking Thermoplastic, Solid, White, Arrows	EA	\$50.00	8		\$400.00
711-11-221	Traffic Pavement Marking Thermoplastic, Solid, Yellow, 6"	LF	\$0.50	592		\$296.00
711-11-231	Traffic Pavement Marking Thermoplastic, Skip 10/30, Yellow, 6"	GM	\$2,640.00	0.21		\$554.40
	Contingency (Do Not Bid)	LS	\$80,000.00	1		\$70,000.00
<b>TOTAL:</b>						<b>\$709,939.09</b>

Mary Brickell Drainage and Roadway Improvements Project - Phase II Pump Station  
 Engineer's Opinion of Probable Construction Cost

PAY ITEM	PAY ITEM DESCRIPTION	UNIT	UNIT PRICE	PLAN QTY	FINAL QTY	COST
101-1	Mobilization	LS	\$59,070.35	1		\$59,070.35
102-1	Maintenance of Traffic	LS	\$35,442.21	1		\$35,442.21
110-1-1	Clearing and Grubbing	LS	\$35,442.21	1		\$35,442.21
285-711	Optional Base Group 11 (12" Limerock LBR 100)	SY	\$20.00	64		\$1,280.00
327-70-19	Milling Existing Asphalt Pavement (1" Average)	SY	\$3.00	920		\$2,760.00
334-1-13	Superpave Asphaltic Concrete, Traffic C (110lbs/sy-in., 1" min., includes roadway and parking lanes)	TN	\$100.00	54		\$5,412.00
400-3-1	Concrete Class III, Culverts (36"x60" box culvert)	CY	\$500.00	8		\$4,000.00
415-1-6	Reinforcing Steel - Miscellaneous (36"x60" box culvert)	LB	\$1.00	550		\$550.00
425-2-71	Manholes, J-7, <10' (refer to plans for dimensions)	EA	\$6,000.00	4		\$24,000.00
425-2-101	Manholes, Special <10' (includes structures S-1 and S-4)	EA	\$10,000.00	2		\$20,000.00
425-2-102	Manholes, Special >10' (includes BMP structure)	EA	\$50,000.00	1		\$50,000.00
430-175-124	Pipe Culvert, Optional Material, Round Shape 24" S/CD (D.I.P. for forcemain, includes fittings)	LF	\$150.00	103		\$15,450.00
430-175-130	Pipe Culvert, Optional Material, Round Shape 30" S/CD	LF	\$90.00	17		\$1,530.00
430-175-142	Pipe Culvert, Optional Material, Round Shape 42" S/CD (D.I.P. for forcemain, includes fittings)	LF	\$250.00	28		\$7,000.00
430-175-148	Pipe Culvert, Optional Material, Round Shape 48" S/CD	LF	\$150.00	30		\$4,500.00
444-70-11	Deep Well - Open Hole, 24"	LF	\$150.00	30		\$4,500.00
444-71-11	Deep Well - Casing, 24"	LF	\$200.00	160		\$32,000.00
448-73	Pumping Station	LS	\$1,000,000.00	1		\$1,000,000.00
520-1-10	Concrete Curb Type "F"	LF	\$20.00	130		\$2,600.00
522-1	Sidewalk Concrete, 4" Thick	SY	\$45.00	85		\$3,825.00
580-1-2	Landscaping Complete	LS	\$2,000.00	1		\$2,000.00
	Contingency (Do Not Bid)	LS	\$100,000.00	1		\$100,000.00
<b>TOTAL:</b>						<b>\$1,411,361.77</b>

5%  
3%  
3%

**APPENDIX J – CORRESPONDENCE**



CITY OF MIAMI, FLORIDA  
INTER-OFFICE MEMORANDUM

TO: Ola O. Aluko, Director,  
Capital Improvement Program

DATE: September 16, 2008

FILE:

SUBJECT: SW 10<sup>th</sup> Street Inadequate  
Drainage System Request for  
Improvement

FROM: *Francis Mitchell*  
Francis Mitchell, Assistant Director  
Public Works Department

REFERENCES:

ENCLOSURES:

The Public Works Department either thru the services of hired contractors or the capacity of its operations division has exhausted all options in dealing with the drainage deficiencies inherent to the SW 10<sup>th</sup> Street Drainage System. At high tide and during heavy storm events SW 10<sup>th</sup> Street gets flooded because the existing drainage system does not have enough capacity to adequately drain the storm generated runoff.

The problem facing this low lying area is compounded by the fact that private wells or drainage systems adjacent to this street are deficient and draining in the public right of way.

Therefore, in dealing with established 311 reporting procedure, our department is forwarding this memo to your attention for reference in the event a funded or unfunded project will be created to remediate at this problem.

cc: Stephanie N. Grindell, Director, Public Works Department  
Bill Anido, Assistant City Manager, City Manager's Office  
Vanessa Morales Balthazar, Special Projects Coordinator, CitiStat

# City of Miami



PEDRO G. HERNANDEZ, P.E.  
City Manager

June 16, 2009

Ms. Esther Calas  
Public Works Department  
Miami-Dade County  
111 NW 1 Street, Suite 1610  
Miami, FL 33128-1970

RE: **Inadequate Drainage System along SW 2<sup>nd</sup> Avenue and south Miami Avenue from SW 15<sup>th</sup> Road to SW 7<sup>th</sup> Street.**

The City is currently experiencing serious flooding along SW 10<sup>th</sup> Street from South Miami Avenue to SW 1<sup>st</sup> Avenue. We have extensively analyzed the gravity drainage system servicing this area and are planning some improvement to remediate at this situation. A mini pump station is currently under study.

We have conducted multiple field observation of this site and have observed that the flooding along SW 10<sup>th</sup> Street is also related to the upland areas drainage systems located along SW 2<sup>nd</sup> Avenue and South Miami Avenue. These systems are deficient and quickly overflow toward the low lying areas of SW 10 ST and SW 9 ST.

We have identified these intersections as trouble areas contributing to the increased runoff on SW 10 ST.

SW 2<sup>nd</sup> Avenue intersections (refer to attachments)

- SW 9<sup>th</sup> ST
- SW 10<sup>th</sup> ST
- SW 11<sup>th</sup> ST

} Com APW note

South Miami Avenue Intersections (refer to attachments)

- SE 10<sup>th</sup> ST
- SE 11<sup>th</sup> ST
- SE 12<sup>th</sup> ST

} Why is Com asking  
MD to fix these?

Our Department will initiate an emergency storm sewer construction project at the SW 2<sup>nd</sup> Avenue intersections. However, in order to maximize the reduction of upland runoff toward SW 10 Street we are hoping that your Department could initiate similar remedial action along the South Miami Avenue intersections.

I am transmitting some of the archived information that we have on file to help in further explaining the problem. Please advise our office of your decision.

Sincerely,

  
Francis Mitchell,  
Assistant Director

FM/cdt

cc: Stephanie N. Grindell, Director, Public Works  
Leonard Helmers, Professional Engineer IV, Public Works  
Pedro Lopez, Engineer I, Public Works  
Ricardo Castro, Project Manager, CIP

DEPARTMENT OF PUBLIC WORKS

444 S.W. 2nd Avenue / Miami, Florida 33130 / (305) 416-1200 / Fax: (305) 416-1278  
Mailing Address: P.O. Box 330708 Miami, FL 33233-0708

## Meeting Memorandum

**PROJECT:** City of Miami – Mary Brickell Village Drainage and Street Improvements

**TO:** **Ricardo Castro, PE**  
 444 S.W. 2nd Avenue  
 Miami, FL 33130

Phone: 305.416.1051

**FROM:** David Reynolds, P.E.

**DATE:** Wednesday, April 8, 2009, 2:00 PM

A meeting was held on this date at City of Miami Capital Improvements office to discuss the overview of the project. The following were in attendance:

Individual	Title	Company
Ricardo Castro	Project Manager	City of Miami, CIP
Francis Mitchell	Assistant Director	City of Miami, CIP
David Reynolds	Project Engineer	TY Lin International
Claudia Diaz	Project Engineer	TY Lin International

### Project Overview –

There are drainage, pavement, and roadside deficiencies along 9<sup>th</sup> and 10<sup>th</sup> Streets in the vicinity of Mary Brickell Village that need improvement plans to address. Project issues were discussed and a walk of project site was done to check the possible causes of drainage problems and to evaluate the condition of pavement on the subject streets.

1. **Drainage** – Minor recurring flooding/ponding is reported on SW 10<sup>th</sup> Street between 1<sup>st</sup> Ave. and S. Miami Ave. and at the intersection of SW 10<sup>th</sup> Street at S. Miami Ave. Ponding has appeared to be for only very brief periods of time during and following storm events. There is also reported ponding at the intersection of SW 9<sup>th</sup> Street and Brickell Plaza although this has not been confirmed. The existing drainage line along 10<sup>th</sup> St is a concrete trench (24" span, 18" rise). The existing drainage line along 1<sup>st</sup> Court is a concrete trench (60" span, 36" rise). The City has recently cleaned out the storm sewer systems in these areas. The City is considering installation of a small storm water pump station to completely drain the contributing storm sewers at these problem areas. Additionally, the existing storm sewer outfall at SW 1<sup>st</sup> Court at the Miami River has collapsed and requires a stable permanent headwall as well as a manatee barrier. This location is within the city Right-of-Way.
2. **Pavement Deterioration** – The road section of SW 9<sup>th</sup> and SW 10<sup>th</sup> Streets generally has adequate crown and cross slope and some segments have relatively new pavement from recent site development around Mary Brickell Village. However, significant pavement failures including map cracking, longitudinal cracking, and pot holes were evident in other segments. See the attached aerial map with pavement notations. Milling and resurfacing versus full-depth pavement reconstruction will depend on pavement core results for asphalt and base thickness.

3. **Sidewalk and Curb & Gutter** – Existing sidewalk and curb and gutters on the north side of SW 9<sup>th</sup> St from about 200ft east of SW 1<sup>st</sup> Ave to Brickell Plaza need reconstruction.

**Design Considerations** – Drainage design will be limited to Rational Method hydrology and the design of new inlet locations, storm sewer sizing, and pump station design. No additional hydraulic modeling of the storm network will be required. Drainage design will be based on the 5-year, 1-hour storm event (FDOT curves).

**Project Scope** – This project will require topographic survey within Right of Way, geotechnical investigations for pavement and base thickness and subsurface conditions at the storm drain outfall at the Miami River. Ricardo will obtain and forward copies of City utility atlas sheets and City DPW reports of flooding.

## Francisco Alonso

---

**From:** Francisco Alonso  
**Sent:** Tuesday, October 20, 2009 2:38 PM  
**To:** fmittchell@miamigov.com  
**Cc:** Jose Lago (jlago@miamigov.com); Jorge Garcia (jagarcia@miamigov.com); Claudia Diaz; Javier Gonzalez  
**Subject:** City of Miami Mary Brickell Village  
**Attachments:** PROJECT LAYOUT 3.PDF

Francis,

It seems we missed each other last Friday, I just wanted to follow up with you to finalize the scope for the subject project.

The following is my understanding of the scope the City wishes to pursue:

The Project limits are:

- SW 9<sup>th</sup> Street from SW 1<sup>st</sup> Avenue to SE 1<sup>st</sup> Avenue (Brickell Plaza Drive),
- SW 10<sup>th</sup> Street from SW 1<sup>st</sup> Avenue to SE 1<sup>st</sup> Avenue (Brickell Plaza Drive), and

The Project will involve:

- a. Construction of storm sewer improvements to alleviate recurring minor flooding/ponding. The City plans to utilize a small retrofit storm water pump station at the SW 10<sup>th</sup> Street / SW 1<sup>st</sup> Avenue intersection. Additional drainage improvements will include a new storm sewer connection for the isolated drainage system at SW 10<sup>th</sup> Street and S. Miami Avenue.
- b. Pavement milling and resurfacing and pavement marking. Generally, pavement work will be limited to the travel lanes, however, specific shoulder areas along the north side of SW 9<sup>th</sup> Street will be improved to address on-street parking. Milling/resurfacing versus full-depth pavement reconstruction will depend on pavement coring results for asphalt and base thickness.
- c. Reconstruction of existing sidewalk and curb and gutter along the north side of SW 9<sup>th</sup> Street as necessary to provide a uniform, closed-section roadway. Also include curb and gutter and sidewalk improvements on along 10<sup>th</sup> Street from S. Miami Avenue to SE 1<sup>st</sup> Avenue.
- d. Reconstruction of specific existing curb ramps to comply with ADA requirements.

It is also my understanding that the original proposal included the reconstruction of the existing concrete culvert outfall on SW 1<sup>st</sup> Court at the Miami River and to provide an end wall structure and manatee barrier. This portion of the scope is no longer included, as you had mentioned to me that the County was to perform improvements along that area in the future. I have also provided a sketch with the areas of the proposed improvements. Please respond to this email to concur with the presented scope items or to clarify any of the above items which may be incorrect. As soon as you can respond, we will provide Capital Improvements with the finalized proposal and get started asap on this project. Thank you for the opportunity.

Francisco J. Alonso, P.E.  
T.Y.Lin **International | H.J. Ross**  
201 Alhambra Circle  
Coral Gables, FL 33134  
(305)567-1888 ext. 267

## Francisco Alonso

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**From:** Lago, Jose [JLago@miamigov.com]  
**Sent:** Friday, December 04, 2009 11:10 AM  
**To:** Garcia, Jorge  
**Cc:** Francisco Alonso; Mitchell, Francis  
**Subject:** RE: Mary Brickell Sketch

Please arrange mtg with TYLIN. Time is of essence on this project (more then the norm).

Please insure that you understand the scope of work required. I have my notes. It may take the walking the site again. March 2010 is the design deadline. I believe it will require a DERM permit (Class II). Thx.

---

**From:** Francisco Alonso [Francisco.Alonso@tylin.com]  
**Sent:** Friday, December 04, 2009 9:13 AM  
**To:** Garcia, Jorge  
**Cc:** Lago, Jose  
**Subject:** RE: Mary Brickell Sketch

Gentlemen,

Before we proceed with the final proposal I need more specifics on the added scope. You are adding two more blocks of which I am not clear what the proposed improvements are, in addition I do not have any surveying planned for that area. I am requesting a meeting asap to go over the proposed plan in detail before finalizing the proposal. Please let me know

Thank you.

Francisco J. Alonso, P.E.  
T.Y.Lin International | H.J. Ross  
201 Alhambra Circle  
Coral Gables, FL 33134  
(305)567-1888 ext. 267

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**From:** Garcia, Jorge [mailto:jagarcia@miamigov.com]  
**Sent:** Thursday, December 03, 2009 4:06 PM  
**To:** Francisco Alonso  
**Cc:** Lago, Jose  
**Subject:** RE: Mary Brickell Sketch

Frank:

As we told you, the boundaries of the project changed, being now from the 9th Street to the 12th Street and between SE 1st Avenue and SW 1st Avenue. The storm water drainage should be analyzed inside those boundaries.

An important issue that you should consider is that S. Miami Avenue is a MDC street and is located inside the boundaries before mentioned, meaning that you have to coordinate with them the impact on that road due to this project.

Basically the scope of work is the same, but adding some aspects like the construction of bulb-outs, increases the sidewalk width all the way, some landscaping like small trees and finally if the cost estimate allows, considering to install pedestrian lightings.

The time is very important and the City needs to finish the design, including permitting and cost estimate on March, 2010, in order to start the construction on April, 2010, what I mean is that we should have your reviewed cost proposal not later than this Monday.



If you have any question, please do not hesitate to call me.

Thanks

Jorge Garcia  
Project Manager  
Department of Capital Improvements  
444 S.W. 2nd Avenue, 8th Floor  
Miami, FL 33130  
Office Phone: (305) 416-1219  
Fax: (305) 416-2153  
Cell: (786) 376-4391

From: Francisco Alonso [mailto:Francisco.Alonso@tylin.com]  
Sent: Wednesday, December 02, 2009 11:38 AM  
To: Garcia, Jorge  
Subject: Mary Brickell Sketch

Jorge,

Attached is the sketch for the Mary Brickell project scope. Let me know if this is adequate.

Thank you,

Francisco J. Alonso, P.E.  
T.Y.Lin International | H.J. Ross  
201 Alhambra Circle  
Coral Gables, FL 33134  
(305)567-1888 ext. 267

## Meeting Memorandum

**PROJECT:** Mary Brickell Village Drainage and Street Improvements B-30637

**TO: Jorge Garcia** Phone: 305.416.1219  
 444 S.W. 2nd Avenue  
 Miami, FL 33130

**FROM:** Francisco J. Alonso, P.E.

**DATE:** Wednesday, September 16, 2010, 1:15 PM

A meeting was held on this date at City of Miami Department of Capital Improvements office to discuss the subject Project. The following were in attendance:

Individual	Title	Company
Alice N. Bravo, P.E.	CIP Director	City of Miami, CIP
Albert Sosa, P.E.	CIP Assistant Director	City of Miami, CIP
Jose Lago, P.E.	CIP	City of Miami, CIP
Jorge Garcia	Project Manager, CIP	City of Miami, CIP
Francisco J. Alonso, P.E.	Project Manager	TY Lin International

The purpose of this meeting was to discuss concerns T.Y. Lin had over the current scope of the project, the following bullet points address the specific topics discussed:

- The meeting began with a brief history of the project and an explanation of the drainage problems currently experience throughout the various depressions in the site. A brief history of how the current scope was arrived at was also detailed.
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  - It will also be problematic for maintenance crews to access the pump station once it is operational and will require road closures to do so.
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- Mr. Sosa suggested a third alternative to construct a larger bypass pump station at the downstream end of the entire system near the outfall at NW 1<sup>st</sup> Avenue and the Miami River. Mr. Alonso concurred that this solution was really the “end all” solution to the flooding problems as it would address the entire area, but did involve a significantly larger station and cost. It was

mentioned that the costs of the larger station may be offset by not having to construction a new collection system and force main.

- It was also discussed that using CIPP (cured in place pipe) could be utilized to line the existing trunk lines further reducing restoration costs and construction time.
- It was finally agreed to model and study the three proposed scenarios: current scope, pump station at 10<sup>th</sup> Street Park, and pump station at outfall.
- T.Y. Lin would model and study the three scenarios as part of the ongoing technical memorandum to determine their effectiveness and feasibility as well as cost estimates for each in order to provide a basis for CIP to decide on a course of action for design.
- The remainder of the scope including milling and resurfacing, curb and gutter, and sidewalk improvements would remain the same. However T.Y. Lin would include estimates for bid options including milling and resurfacing of the remaining sections of roadway encompassed by the overall project area but not currently in the scope.
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- Mr. Garcia was to follow-up with the parks department to determine the feasibility of constructing the 10<sup>th</sup> Street park option and provide a response from PD.
- It was discussed that a meeting should be arranged with Lyn Helmers to determine the status of the agreements between the City and the private owners regarding decorative sidewalk treatments within the project limits.

## Memorandum

**PROJECT:** Mary Brickell Village Drainage and Street Improvements B-30637

**TO: Jorge Garcia**  
444 S.W. 2nd Avenue  
Miami, FL 33130

Phone: 305.416.1219

**FROM:** Francisco J. Alonso, P.E.

**DATE:** September 27, 2010

The purpose of this memo is to provide an update to the department of Capital Improvements Program on the subject project. The following is an outline of what has been completed to date. The technical memorandum presenting the drainage and roadway improvement options will be submitted October 18, 2010.

### Preliminary Engineering Services:

- Full Topographical Survey and GPR survey were completed as of September 15, 2010. Final signed and sealed copies were submitted to the City on September 22, 2010
- Geotechnical testing and report are currently being completed. There has been delay due to delays in the permitting of the field work, but we anticipate completion of the reporting prior to the Technical Memorandum submittal.
- Utility Coordination was initiated on August 12, 2010. The Sunshine state design ticket number is 224003469. Packages depicting preliminary surveys were mailed to all the utility companies listed on the design ticket on August 13, 2010. To date 5 of 14 of the utilities companies have responded in some form. Contact with all the utility companies is anticipated to be completed by the time of the Technical Memorandum submittal. Our Utility coordination matrix will be included with this memo.
- MD-WASD as-builts were acquired.
- City of Miami underground records were acquired from public works and incorporated into the project plans.

### Technical Memorandum:

- GIS maps of the project area are being developed to determine land use and soil types.
- FEMA Firm maps have acquired for the project area.
- The ICPR drainage model has been fully developed for the existing conditions including:
  - All basins and sub-basins (28) have been identified and incorporated into the model based on the topographic survey and as-built information.
  - All junction nodes, pipes, and culverts have been identified and incorporated into the model including sizes and inverts based on survey and as-built data.
  - Utilizing this information, a node-link diagram was developed.
  - "Stage vs. Storage" curves have been developed using the topographic survey and AutoCAD Civil 3D to create 3D surfaces to calculate below and above ground storage. This information was incorporated into the ICPR node information and is critical to determining accurate flood levels.
  - Boundary condition information has been identified based on available NOAA tidal data in the area. Said condition will serve as the project tail water elevation.

- Curve numbers based on percent impervious and existing soils have been estimated and incorporated into the model.
  - Times of concentration have been calculated and incorporated into the model.
  - Rainfall data for the area has been compiled and incorporated into the model.
  - All standard design storms have been modeled for the existing conditions per FDOT drainage design standards.
  - Levels of existing flooding have been identified and calibrated, and we now have a baseline from which to compare proposed improvement solutions.
- The ICPR drainage model for the proposed drainage alternatives is currently being developed. This model will be compared to the results of the existing conditions to determine the impact of the proposed improvements and serve as a basis for the final design.
  - The technical memorandum write-up outline has been prepared.
  - Field visits have been held to determine the extent of roadway improvements and to develop the typical sections that will be presented as part of the technical memorandum.

Attachments:

- ICPR node-link diagram for the existing system
- ICPR input report
- ICPR existing conditions node maximum results report
- Utility coordination Matrix



# **Pre Construction Conference Agenda**

**Miami Dade County  
Public Works Department  
September 1; 10:00 AM**

**Project Title: *Drainage Improvement Project for:  
Brickell Area.***

**Project No: *201000406***

## **1. Introduction.**

Introduction of attendees and opening comments by DCPW Head Construction Contract Management Section, Mr. Duane Kopp, P.E.

- Dade County Public Works Department
- Rock Power Paving Inc.
- Department of Business Development

## **2. Project Description**

**Total Contract Time : 240 Calendar Days**  
**Contract Amount : \$ 400,092.62**

## **3. Delineation of lines of Authority**

Dade County Public Works Department  
Esther Calas, P.E., Director.  
Antonio Cotarelo, P.E., Assistant Director.  
Bassam Moubayed, CFM, Chief Construction Division.  
Duane Kopp, P.E., Head Construction Contract Management Section.  
Otto Rojas P.E., Construction Coordinator.  
Ruben Arencibia, Project Manager.

Rock Power Paving Inc.  
Robert Delgado, President



All correspondence will be addressed to the project manager Ruben Arencibia who will coordinate the response. Names and emergency telephone numbers for the contractor, department and others should be provided before starting construction.

#### 4. Goals of the Project

- Timely completion of project
- Maintain project within contractual budget.
- Complete project with no reportable accidents

#### 5. Department of Business Development

Explanation by a representative

#### 6. Location of work.

The location of work to be performed shall be: South Miami Avenue from 10<sup>th</sup> Street to 14<sup>th</sup> Street and SW 2<sup>nd</sup> Avenue from SW 9<sup>th</sup> Street to 11 Street, Miami-Dade County, Florida. The exact location and limits of construction are shown in the Plans that accompanying the Contract.

#### 7. Scope of Work.

The work under the Contract includes furnishing of all supervision, labor, materials, tools, equipment, and performing all operations necessary for this project. Work includes but is not limited to the construction and installation of drainage structures, French Drains, miscellaneous drainage improvements, grading, sodding, and miscellaneous roadway restoration including construction of concrete curb and gutters, and sidewalks where needed in accordance with the construction plans and specifications contained in the contract.

#### 8. SPECIAL PROVISIONS

The following items of discussion are the most relevant, but not the only aspects that will be enforced following the wording of the contract documents.

##### 8.1. GENERAL.

###### **STANDARD REFERENCES. (SP-page 6, 2.02)**

The **Building Code** as set forth in **Charter 8** of the Code of Miami Dade County, the **Public Works Manual of Metropolitan Dade County**, and the **2008 Edition of FDOT Design Standards** (with July 1, 2009 modifications), Construction, Maintenance and Utility Operations on the State Highway System, as amended by the Contract Documents; all are incorporate by reference.

Unless otherwise specifically noted, the **2007 FDOT Standard Specification for Road and Bridge Construction**, as amended by the Contract Documents, is hereby incorporate by reference.

Miami-Dade County's Traffic Control Equipment Specifications and Standards for Metro Traffic Control System Miami Dade County with its supplements or addenda is incorporated herein by reference.

## 8.2 PLANS (SP-page 12, 3.03)

Engineering Drawings Plans are included in the Contract. Additional standards details are available in the Miami Dade Public Works Manual and FDOT's Standards for Design, Construction, Maintenance and Utility Operations on the State Highway System. The County shall have the right to modify the details and /or sketches, to supplement the sketches with additional information as work proceeds.

## 8.3 TIME FOR COMPLETION (SP-page 13, 3.05)

The terms of the Contract shall expire **240 calendar days** from the effective date of the "**Notice to proceed**", or until such time as the Contract amount has been expended, whichever occurs first.

The effective date of the "**Notice to Proceed**" will be established today .The effective date shall be as or later than 30 calendar days after the date of execution of the Contract Documents, unless a later date acceptable to both parties is agreed upon writing.

## 8.4 PERMITS AND LICENSES (SP- page 13, 3.06)

- The Contractor must obtain **all permits required** for the Project prior to commencing the work. This includes Permits required by other Municipalities and agencies, Permits to work in the Right-of-Way, and those required for tree removals and/or relocation.
- Permit to perform work within the County's Right-of-Way are issue by Public Work Department's Construction Division
- The Contractor shall give due and adequate notices to those in control of all properties that may be affected by the construction activities.
- The actual amount paid for the permits, will be reimbursed to the Contractor from a dedicated allowance established by the County. Original receipts must be presented to the Engineer.
- The Contractor shall give all notices, pay all fees and comply with all laws, rules and regulations applicable to the Work at no additional cost.

## 8.4 USE OF PUBLIC STREETS (SP-page 13 -14, 3.07)

The use of Public Street and Alleys shall be such as providing a minimum inconvenience to the public and to other traffic. The Contractor shall so conduct his operations that he shall not close any thoroughfare nor interfere in any way with traffic on railway, highways, or on water, without the written consent of the proper authorities.

The Contractor shall immediately remove any earth or other excavated material spilled from trucks and clean the streets to the satisfaction of the governing authority.

General requirements are that the transport vehicles must be the type(s) approved for this application by the political jurisdiction involved. The vehicles have watertight bodies that they are properly equipped and fitted with seals and covers to prohibit material spillage or draining on roadways, and that they are cleaned as often as is necessary to prevent deposit of material on roadways.

The County does not provide staging areas.

#### **8.5 RIGTH OF WAY VERIFICATION (SP-page 14, 3.09)**

All works and improvements shall be performed, constructed and installed within the limits of the existing Right-of Way pursuant to the contract. The Contractor is responsible for obtaining all necessary documentation for verifying right-of way and property lines. The contractor shall retain a Florida Registered Surveyor and Mapper to obtain right-of way and property lines. The Contractor's surveyor will layout the required alignments, grades and is responsible for their accuracy.

#### **8.6 PRESERVATION OF PROPERTY (SP-page 14-15, 3.09)**

Property, public or private, if damage during construction or removed for convenience of work, shall be repaired or replaced at Contractor's expense in a manner acceptable to the Engineer, prior to final acceptance of the work. This includes, but is not limited to signalization equipment and miscellaneous hardware removed from the construction site, signs, driveways landscaping, walkways, walls, fences, footing or underground utilities.

All street signs shall remain in place during time of construction except those required to be relocated due to interference with actual construction. All signs relocated or damaged by the Contractor during the course of the work shall be re-installed or replaced at the proper location, as soon as possible at the Contractor's expense.

Prior to removal of any traffic control sign that interfere with the construction, the Contractor shall provide temporary signing or other provisions to assure a continuous flow of traffic under at least the same conditions of previously existed.

#### **8.7 UTILITIES. (SP-page 15, 3.10)**

The Contractor shall make all necessary arrangements with the utility companies concerned for maintenance of their lines during the construction period.

The County will not be liable for any delay or added expense the Contractor experiences due to the activities of the utility companies, nor shall the County be held responsible for damage to any utilities due to any actions by the Contractor.

Contractor shall contact **Sunshine State One Call of Florida, Inc. 1-800-432-4770 no less than forty-eight (48) hours prior to commencing any trenching or excavation on this project.**

#### **8.8 PROJECT TIME SCHEDULE (SP-page 18-19, 3.14)**

##### **Work Progress Schedule.**

The Schedule had to be submitting before this conference where show the various activities of the work, demonstrating a reasonable and workable plan to complete the Project within the Contract Duration.

**Progress of the Work.** The Contractor shall commence the Work within 5 calendar days from the date of "Notice to Proceed" and continue all work in an expeditious manner to a conclusion acceptable to the Engineer prior to the expiration Contract Duration.

The Contractor shall supply sufficient work force, materials and equipment to perform the work listed under "Scope of Work" in accordance with the schedule approved by the Engineer and the requirements stipulated in the Contract.

Progress of the work shall be judged based on a proportion of the amount of the work completed and accepted, to the number of calendar days that remain on the Contract Duration.

Contract work completed shall not fall behind by more than ten (10) percentage points, according to the total number of days past on the Contract since the issuance of the "Notice to Proceed"

#### **8.9 PERFORMANCE OF WORK. (SP-page 20, 3.17)**

The Contractor shall submit for approval by the Engineer a description of the type of materials and equipment to be used; and the method of procedure to be in the performance of the work.

##### **Dust Control and Saw Cutting:**

Dust control measurements are required as necessary to prevent the surface and air transport of dust from any construction activity performed under the Contract. This may include but is not limited to: pre-watering deeply before excavation, scheduling thorough and consistent watering that does not run off the site; applying best management practices in the loading, offloading, and transport of soils and miscellaneous materials; covering or otherwise stabilizing piles when necessary ;and schedule so control measures are available throughout the project.

##### **Open Excavations:**

At the close of each workday, the Contractor shall refill all open excavations, or cover open excavation with steel plates capable of supporting vehicular traffic.

##### **Florida Trench Safety Act:**

The propose and intention of the State of Florida "Trench Safety Act" is to provide for increased worker safety by requiring compliance with sufficient standards for trench safety and proving additional specific requirements when the excavation is in excess of 5 feet deep.

#### **8.10 RESTORATION OF PROPERTY. (SP-page 22, 3.18)**

The Contractor is advice to take preconstruction videos/picture of the entire work zone and adjacent areas and to take reasonable care in the protection of the property, vegetation and utilities.

Contractor shall restore the right-of-way as well as any affected adjacent private property within 45 days of completion of construction or damage to the affected property or area, whichever occurs first.

#### **8.11 AS-BUILT DRAWINGS (SP-PAGE 23, 3.19)**

Three (3) sets of complete "As Built" drawings signed and sealed by either a Florida Register Surveyor and Mapper or a Florida Registered Professional Engineer, shall be accurately recorded by the Contractor and submitted to the Engineer prior to final acceptance of the work. All locations and elevations shall be taken by a Florida Registered Surveyor and Mapper and be shown on the As-Built drawings. No separate payment will be made for the As-Built drawings.

**8.12 LIQUIDATED DAMAGES. (SP-PAGE 24, 3.21)**

The Contractor, or in case of his default the surety, shall pay to the County, not as a penalty but as liquidated damages, the amount of \$ 715.00 daily per calendar day should the Contractor fail to complete all works specified within the time stipulated in the contract including extra time granted in writing by the County.

**8.13 MAINTENANCE OF TRAFFIC, SECTION 102. (SP-page 26 4.03)**

A State of Florida MOT-Advanced Certified Technician is required for layout and maintenance of approved MOT plans. Traffic may be detoured only upon approval of the Director of Public Works Department. Contractor must submit an MOT plan to closure of roads for review and approval by Public Work Department. No work shall commence on this project or any portion thereof without implementation of an approved MOT plan.

**8.15 PREVENTION, CONTROL, AND ABATEMENT OF EROSION AND WATER POLLUTION. SECTION 104. (SP-page 28, 4.04)**

The Contractor's Erosion Control Plan (ECP) must be approved by the Engineer in writing before any construction activities. At the Preconstruction Conference (Today), submit to the Engineer for review and approval an ECP according with our Contract.

**8.16 CLEARING AND GRUBING (SP-page 35 & 36, 4.05)**

The contract unit price awarded shall be full compensation for all work required for clearing and grubbing; including, but not limited to, removal asphalt pavement, concrete curb and gutters, concrete sidewalk, vegetation, trees, trash, debris, tree trimming, mailboxes and other work related to clearing and grubbing including removal and disposal of stumps roots any others protruding object which are necessary for the proper construction project. Also included in this section shall be grading and final dressing required to provide the necessary terrain configuration to facilitate an effective drainage run-off.

**8.17 ROCK BASE (SP-page 36 4.07)**

The **rock base** shall be constructed on a sub grade prepared in accordance with FDOT Section 120-9.4.

Within the entire limits of the proposed **subgrade**, the minimum density acceptable at any location shall be ninety five (95) percent for Non-roadway areas and ninety eight (98) percent for Primary and Secondary Roads, of maximum density.

It shall be the Contractor's responsibility to maintain the required density until the base is placed on the subgrade.

**Base or Limerock Base** shall have an overall compacted thickness as specified and noted in the plans. Minimum density shall be nine eight (98) percent of such maximum density. Minimum percent of calcium and magnesium in the limerock material will be fifty (50). Upon Engineer's approval, the lime rock base shall be primed. The prime coat should have a minimum curing period of 48 hours.

## **8.18 BITUMINOUS TREATMENTS SURFACE COURSES AND CONCRETE PAVEMENT.**

### **(SP-page 38, 5)**

A prime coat is required for all limerock base construction and the cost will be included in the price utilizing the limerock base per square yard.

A tack coat shall be applied to previously primed and newly constructed bases, existing wearing surfaces, milled surfaces and previously applied leveling courses.

Payment for all bituminous material, including tack coat, shall be included in the payment for Asphaltic Concrete.

## **8.19 INLETS, MANHOLES AND JUNCTION BOXES. (SP-page 41, 6.01)**

Select material shall be used for backfill adjacent to catch basin and riser inlets, as detailed in the plans.

Upon completion of the work, and prior to acceptance and final payment, all such structures will be inspected by the Engineer to ensure that they are free of all debris and thoroughly cleaned.

## **8.20 PIPE CULVERTS. (SP-page 43, 6.03)**

Obtain pipe culvert from a producer currently on the FDOT's list of Producers with Accepted Quality Control Programs.

If Aluminum pipe is utilized, the Contractor shall exercise sufficient care in handling and backfilling to avoid damage to the pipe.

Corrugated Polyethylene Pipe Class I, and Polyvinyl Chloride (PVC) Pipe materials not be used on arterial roads. Corrugated Polyethylene Pipe Class II may be used on arterial roads pursuant to the requirements of this section.

## **8.21 FRENCH DRAIN. (SP-page 36, 6.04)**

Payments shall be made under: French Drain of 18" diam.perforated pipe, trench depth 15 ft BLS (Below Land Surface) in LF.

## **8.22 CONCRETE GUTTER, CURB ELEMENTS, AND TRAFFIC SEPARATOR. (SP-page 38, 7.02) AND CONCRETE SIDEWALK. (SP-page 39, 7.03)**

**Class I Concrete** shall have a minimum compressive strength of **3,000 P.S.I at 28 days.**

## **9. NOTICE TO PROCEED.**

Upon receipt of a **Notice to Proceed**, the Contractor shall notify the Department two working days in advance of his intent to commence work. The Contractor shall commence the work in accordance with the Contract Documents including the Schedule, schedule of values, shop drawings submittals and process, etc

## **10. Discuss Miscellaneous Issues/Questions and Answers.**

- Schedule.
- Propose starting day.



## MEETING SIGN IN SHEET

PROJECT NAME: BRICKELL AREAS.  
PROJECT NO. : #2010406

NAME	SIGNATURE	COMPANY	PHONE No.	FAX No.
YULY HERNANDEZ		PWD	3/375 4284	3/375 4000
Elva R. Reyes		POD	305 375 1879	305 375 2731
Robert Delgado		Rock Power	305 752-7742	305 752-7728
DUANE KOPP		PWD	305 575 1306	---
Estela Nogueira		HDUNID	786-268-5250	786-268-1340
Marien Fleitas		PWD	(305)375-3786	(305)375-5909
ALBERTO MAMÍ		PWD	(305)375-3786	305 375 5909
ALEX ROCHE		TECO	954-453-0811	954-453-0804
Francisco Alonso		T.Y. Lin (city of Miami consultant)	(305)567-1988	(305)567-1771
URBEN ANGLICIA		PWD	(305)375-2111	(305)375-2547
Otto Rojas		PWD	305 375 2111	305 375 2547
Urbano Baz		PWD	305 375 2111	305 375 2547

DATE: 9/1/10  
LOCATION: 14TH FLOOR CONFERENCE ROOM

## Meeting Memorandum

**PROJECT:** Mary Brickell Village Drainage and Street Improvements B-30637

**TO: Jorge Garcia** Phone: 305.416.1219  
 444 S.W. 2nd Avenue  
 Miami, FL 33130

**FROM:** Francisco J. Alonso, P.E.

**DATE:** Wednesday, September 16, 2010, 1:15 PM

A meeting was held on this date at City of Miami Department of Capital Improvements office to discuss the subject Project. The following were in attendance:

Individual	Title	Company
Alice N. Bravo, P.E.	CIP Director	City of Miami, CIP
Albert Sosa, P.E.	CIP Assistant Director	City of Miami, CIP
Jose Lago, P.E.	CIP	City of Miami, CIP
Jorge Garcia	Project Manager, CIP	City of Miami, CIP
Francisco J. Alonso, P.E.	Project Manager	TY Lin International

The purpose of this meeting was to discuss concerns T.Y. Lin had over the current scope of the project, the following bullet points address the specific topics discussed:

- The meeting began with a brief history of the project and an explanation of the drainage problems currently experience throughout the various depressions in the site. A brief history of how the current scope was arrived at was also detailed.
- Mr. Alonso explained that the current scope calls for a small pump station within the pavement just east of the intersection of S.W. 10<sup>th</sup> Street and 1<sup>st</sup> Avenue. The concerns expressed with current location included the following:
  - The project area is very difficult to construct due to existing utilizes along the street. In addition there is no apparent location for the placement of a control panel and emergency generator.
  - It will also be problematic for maintenance crews to access the pump station once it is operational and will require road closures to do so.
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- Mr. Sosa suggested a third alternative to construct a larger bypass pump station at the downstream end of the entire system near the outfall at NW 1<sup>st</sup> Avenue and the Miami River. Mr. Alonso concurred that this solution was really the “end all” solution to the flooding problems as it would address the entire area, but did involve a significantly larger station and cost. It was

mentioned that the costs of the larger station may be offset by not having to construction a new collection system and force main.

- It was also discussed that using CIPP (cured in place pipe) could be utilized to line the existing trunk lines further reducing restoration costs and construction time.
- It was finally agreed to model and study the three proposed scenarios: current scope, pump station at 10<sup>th</sup> Street Park, and pump station at outfall.
- T.Y. Lin would model and study the three scenarios as part of the ongoing technical memorandum to determine their effectiveness and feasibility as well as cost estimates for each in order to provide a basis for CIP to decide on a course of action for design.
- The remainder of the scope including milling and resurfacing, curb and gutter, and sidewalk improvements would remain the same. However T.Y. Lin would include estimates for bid options including milling and resurfacing of the remaining sections of roadway encompassed by the overall project area but not currently in the scope.
- T.Y. Lin requested and was granted 2 additional weeks to complete the study. T.Y. Lin agreed to provide an update in 2 weeks and deliver the technical memorandum on October 18, 2010.
- Mr. Garcia was to follow-up with the parks department to determine the feasibility of constructing the 10<sup>th</sup> Street park option and provide a response from PD.
- It was discussed that a meeting should be arranged with Lyn Helmers to determine the status of the agreements between the City and the private owners regarding decorative sidewalk treatments within the project limits.

## Meeting Memorandum

**PROJECT:** Mary Brickell Village Drainage and Street Improvements B-30637

**TO: Jorge Garcia**  
 444 S.W. 2nd Avenue  
 Miami, FL 33130

Phone: 305.416.1219

**FROM:** Francisco J. Alonso, P.E.

**DATE:** Friday, December 10, 2010

A meeting was held on this date at the project site to discuss the subject Project. The following were in attendance:

Individual	Title	Company
Albert Sosa, P.E.	CIP Assistant Director	City of Miami, CIP
Jose Lago, P.E.	CIP	City of Miami, CIP
Jorge Garcia	Project Manager, CIP	City of Miami, CIP
Francisco J. Alonso, P.E.	Project Manager	TY Lin International (TYLI)

The purpose of this meeting was to walk the project site along SW 1<sup>st</sup> Avenue west of the MDT corridor in order to identify possible locations for the proposed pump station, for discussion in an upcoming meeting with MDT. Originally TYLI was attempting to position the pump station within the MDT right-of-way under or near the guide-way. In a preliminary discussion with MDT and Orlando Misas (CIP), TYLI determined that the approval process for such a proposal would be long and possibly not successful. Upon reviewing the site with Utility Records in hand, it was determined that installing the pump station within the City right-of-way, possibly in a parking lane, would be possible. Specifically, a site just north of SW 9<sup>th</sup> Street along the parking lane was identified to have sufficient utility clearance to accommodate the pump station wet well/valve box. From current records, it seems only a small water main relocation would be required. TYLI was to investigate the site and clear it of utility conflicts to proceed with the Phase II design (pump station site plan). TYLI was to get a quote from its surveyor to perform a GPR analysis of the area and identify all underground facilities.

## Meeting Memorandum

**PROJECT:** Mary Brickell Village Drainage and Street Improvements B-30637

**TO: Jorge Garcia**  
 444 S.W. 2nd Avenue  
 Miami, FL 33130

Phone: 305.416.1219

**FROM:** Francisco J. Alonso, P.E.

**DATE:** Monday, December 20, 2010

A meeting was held on this date at the MDT offices to discuss the subject Project, specifically the location of the pump station with relation to the MDT right-of-way. The following were in attendance:

Individual	Title	Company
Eric J. Muntan	MDT Chief, Office of Safety and Security	Miami-Dade County MDT
Steven Chayt	Chief of Facilities Maintenance	Miami-Dade County MDT
Albert Sosa, P.E.	CIP Assistant Director	City of Miami, CIP
Jose Lago, P.E.	CIP	City of Miami, CIP
Jorge Garcia	Project Manager, CIP	City of Miami, CIP
Francisco J. Alonso, P.E.	Project Manager	TY Lin International (TYLI)

Note: There were two other representatives present from MDT but we do not have their contact information.

The purpose of this meeting was to determine the possibility and process by which the Mary Brickell Village pump stations or portions of it could be constructed within the MDT right-of-way. The main concerns posed by the MDT staff were as follows:

- Work could not be performed near the footings of the guide-way columns as they are typically spread footings which cover a significant area.
- If any work was agreed to be performed within the right-of-way there would need to be significant coordination with the MDT safety and security staff due to OSHA regulations, personal safety issues, as well as homeland security issues.

Mr. Sosa expressed that using the MDT right-of-way as the pump station site would be the last resort if no other location could be found within the City's right-of-way, and that we were currently evaluating different locations for utility clearance. MDT expressed that the process for approving any work within the MDT right-of-way was long and tedious and as an example mentioned the current City project just north of our site (B-30130 Greenway Project).

The last topic of discussion in the meeting was regarding the Overtown Greenway project (B30624). It was agreed to set up a field meeting with MDT staff to walk the site and identify possible issues.

## Meeting Memorandum

**PROJECT:** Mary Brickell Village Drainage and Street Improvements B-30637

**TO: Jorge Garcia**  
 444 S.W. 2nd Avenue  
 Miami, FL 33130

Phone: 305.416.1219

**FROM:** Francisco J. Alonso, P.E.

**DATE:** Friday, January 14, 2011 @ 11AM

A meeting was held on this date at the DERM Water Control offices to discuss the subject Project, specifically the permitting requirements with regard to drainage. The following were in attendance:

Individual	Title	Company
Camilo Ignacio	Engineer III	Miami Dade DERM
Marie Hall	Engineer II	Miami Dade DERM
Jorge Garcia	Project Manager, CIP	City of Miami, CIP
Francisco J. Alonso, P.E.	Project Manager	TY Lin International (TYLI)
Claudia Diaz	Project Engineer	TY Lin International (TYLI)

The purpose of this meeting was to determine the permitting requirements for Phase I and Phase II of the Mary Brickell Village Project.

Mr. Alonso began the meeting by describing the project location, existing conditions, and existing drainage concerns. The existing system was also thoroughly described as a large gravity outfall serving the entire neighborhood. The scope of the proposed improvements was also described including the conveyance improvements under Phase I and the pump station under Phase II. Proposed water quality features were also described.

Mr. Ignacio expressed that in general the project will require a Class II permit from them. He was not certain if an ERP would be required because we were not physically modifying the outfall pipe just installing a bypass pump station. He did express concern that because of the possible increase in discharge, we should present the project to the SFWMD to determine if an ERP will be required, as they are the agency with jurisdiction in this case. In addition he mentioned if drainage wells will be used (Mr. Alonso confirmed that) they would also require an environmental review by their office prior to submitting to FDEP for the well permits. Ms. Hall was designated as the contact for issues pertaining to drainage wells.

Mr. Alonso went on to describe that due to the recent changes in the project scope it was decided to bid it out in two phases, and the question was posed whether or not we need to submit two separate permit applications to allow for construction of Phase I. Mr. Ignacio confirmed that we would need to submit a separate Class II permit for Phase I, and that the conditions of the permit would state that water quality would be addressed as part of the pump station project in Phase II. An ERP would not required during Phase I as no improvements to the outfall are being made and the system would function as existing with only Phase I constructed.



Finally, it was decided to submit the 60% plans and technical memorandum along with a class II permit application to begin review next week. Mr. Ignacio mentioned that the review process would take approximately 3 weeks and that we could have an approved application in approximately 6-9 weeks.

**Meeting adjourned at 11:35AM**

## Meeting Memorandum

**PROJECT:** Mary Brickell Village Drainage and Street Improvements B-30637

**TO: Jorge Garcia** Phone: 305.416.1219  
 444 S.W. 2nd Avenue  
 Miami, FL 33130

**FROM:** Francisco J. Alonso, P.E.

**DATE:** Thursday, February 10, 2011 @ 10:00AM

A meeting was held on this date at Leonard Helmers office to discuss the subject Project, specifically the existing local covenants. The following were in attendance:

Individual	Title	Company
Leonard Helmers	Asst. Director	City of Miami Public Works
Jorge Garcia	Project Manager, CIP	City of Miami, CIP
Francisco J. Alonso, P.E.	Project Manager	TY Lin International (TYLI)

The purpose of this meeting was to determine the actions required when encountering work within areas where there are existing covenants for non-standard improvements by private developers (i.e. Pavers)

Mr. Helmers explained that in the area of this project there were currently a few covenants executed between the City and neighboring land owners (copies of covenants had been provided to all parties). Mr. Helmers went on to explain that the purpose of the covenants were to allow for the installation of non-standards upgrades such as pavers or specialty landscaping by the private land developers within the City Right-of-Way. As part of the covenants the City would have no responsibility to maintain or repair these non-standard improvements. The practical meaning of these covenants for this project is that if any construction is performed within the areas that disturb the non-standard features described in the covenants, the property owner is responsible for their repair. The City's responsibility would be to notify the property owners about the proposed work that will impact their properties with sufficient time that they can make arrangements to make the repairs following construction. If the property owners are non-responsive or do not wish to make the repairs, the City will simply replace the damages areas with standard right-of-way features such as concrete sidewalks or standard asphalt pavement.

Mr. Alonso asked about a specific location shown on the plans to be repaired about 50' west of South Miami Avenue along SW 10<sup>th</sup> Street. This area has large concrete paver tiles and is currently in need of repair. Mr. Helmers confirmed that Public Works is aware of this area and they have already notified the property owner to repair the area per the covenant.

**Action Items:**

- T.Y. Lin to remove from the plans the area along SW 10<sup>th</sup> Street that was proposed to be repaired, as PW has already notified the owner that the repairs must be made.
- T.Y. Lin will identify the property owners that will have covenant areas impacted by construction and CIP will notify them as we approach the letting date of the project.

**Meeting adjourned at 10:30AM**

**Department of Environmental Resources Management**

Natural Resources Regulation and Restoration Division

701 NW 1st Court, 6th Floor

Miami, Florida 33136-3912

T 305-372-6567 F 305-372-6407

Carlos Alvarez, Mayor

miamidade.gov

March 16, 2011

Francisco J Alonso  
T.Y. Lin International  
201 Alhambra Circle Suite 900  
Coral Gables, FL 33134

RE: Request for Additional information for Mary Brickell Village Drainage - Phase I, Class II Permit Application 20110006 for the proposed referenced project located at MIAMI, FL 33130-

Dear Alonso:

Departmental staff has reviewed the items submitted on February 17, 2011 for the application referenced above. The Department is providing comments and requesting the following items to process the application:

1. Submit a substantiating letter from the City of MIAMI Zoning Department stating that the proposed usage of the property upon which the proposed work would occur does not violate any zoning law applicable to the area of the proposed work.
2. Provide a stormwater pollution prevention plan to address the short term water quality impacts from the proposed construction of the proposed development. The plan should identify the appropriate erosion and sedimentation controls and stormwater best management practices to reduce erosion, sedimentation, and stormwater pollution.
3. In order to minimize danger of entrapment to manatees, outfalls which are greater than 7 inches and less than 60 inches in diameter shall be covered with grates or screens with spaces less than 7 inches wide; these shall be maintained to prevent upland flooding.
4. Submit signed and sealed percolation tests performed within the project site. Also, the exfiltration trench must be installed to the same depth that the percolation test was performed.

Please note that based on new information or future submittals, this Department may require additional information or items prior to the issuance of the Class II Permit. Once all the indicated items have been returned, this office shall process the permit application. Please submit the required information within 30 days to prevent your application from becoming dormant.

Be advised that a review of second resubmittal items originally disapproved may be subject to an additional 50% of the original permit fee.

Permits from the Florida Department of Environmental Protection (561-681-6600), and the South Florida Water Management District (1-800-432-2045) may be required for this project. It is the responsibility of you, as the applicant, to contact these agencies.

If you have any questions, please contact me at 305-372-6681.

Sincerely,

*Delivering Excellence Every Day*

A handwritten signature in blue ink, appearing to be "C. Alvarez".



# City of Miami



TONY E. CRAPP, JR.  
City Manager

April 19, 2011

Ms. Yaimara Perez  
Engineer 3  
Miami Dade County  
Department of Environmental Resources Management (DERM)  
Water Control Section  
701 NW 1<sup>st</sup> Court, 6<sup>th</sup> Floor  
Miami, Florida 33136-3912

Re: Mary Brickell Village Drainage Improvements, Phase 1, B-30637

Dear Ms. Perez:

This letter serves to inform you that the Office of Zoning has reviewed your request for the project entitled "Mary Brickell Village Improvement, Phase I, B-30637" with a DERM Class II Permit Application No. 20110006. The area of the proposed work is located within public right of way and bounded by SW/SE 9<sup>th</sup> Street (to the north) SW/SE 12<sup>th</sup> Street (to the south), SW 1<sup>st</sup> Avenue (to the west) and SE 1<sup>st</sup> Avenue (to the east). The Office of Zoning has no objection to the proposed work to be performed since it does not violate any applicable portions of the City of Miami Zoning Code and is in compliance with same.

Should you have any questions, please feel free to contact me at 305-416-1491 or via email at [bmin@miamigov.com](mailto:bmin@miamigov.com).

Sincerely,

  
Barnaby L. Min  
Zoning Administrator

BM/mt  
c: Zoning File